

ASCENSION ISLAND, SOUTH ATLANTIC

RANGE REFERENCE ATMOSPHERE  
0-66 KM ALTITUDE

JANUARY 1984

METEOROLOGY GROUP  
RANGE COMMANDERS COUNCIL

WHITE SANDS MISSILE RANGE  
KWAJALEIN MISSILE RANGE  
YUMA PROVING GROUND

PACIFIC MISSILE TEST CENTER  
NAVAL WEAPONS CENTER  
ATLANTIC FLEET WEAPONS TRAINING FACILITY  
NAVAL AIR TEST CENTER

EASTERN SPACE AND MISSILE CENTER  
ARMAMENT DIVISION  
WESTERN SPACE AND MISSILE CENTER  
AIR FORCE SATELLITE CONTROL FACILITY  
AIR FORCE FLIGHT TEST CENTER  
AIR FORCE TACTICAL FIGHTER WEAPONS CENTER

DTIC  
ELECTED  
FEB 28 1984  
A

84 02 17 007

This document has been approved  
for public release and sale; its  
distribution is unlimited.

DTIC FILE COPY

ADA138470

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER Document 371-84	2. GOVT ACCESSION NO. AD-A138428	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Ascension Island, South Atlantic Range Reference Atmosphere, 0-66 Km Altitude		5. TYPE OF REPORT & PERIOD COVERED Final
7. AUTHOR(s) Meteorology Group Range Commanders Council White Sands Missile Range, NM 88002		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Same as Block 7.		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS Range Commanders Council ATTN: STEWS-SA-R White Sands Missile Range, NM 88002		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Same as Block 11.		12. REPORT DATE January 1984
		13. NUMBER OF PAGES 206
		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for Public Release; Distribution Unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES Supersedes Document 104-63, "Eastern Test Range - Ascension Island, South Atlantic, Part 1," AD645591.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Range reference atmosphere, data quality control, coordinate system, computation of statistical parameters, statistical models, orthogonal axes, thermodynamic quantities, data samples, altitude levels, derived monthly mean, annual mean model atmospheres.		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) FOREWORD - see attached.		

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

## FOREWORD

Atmospheric parameters are essential to the research and development of missiles and aerospace vehicles. In the early 1960's, the need was recognized for realistic atmospheric models derived in a consistent manner for each of the several major test ranges. An atmospheric model derived from statistical data for a particular geographical location is referred to as a reference atmosphere.

The first Range Reference Atmosphere (RRA) was issued in 1963 by the Inter-Range Instrumentation Group (IRIG) for Cape Kennedy, Florida, and was followed by additional publications for several ranges up to 1974. Since that time, improved upper air data bases have become available from which to develop the RRA. These resulted from the extended period of records and from improvement in the upper air measuring program by rocketsondes for altitudes above the rawinsonde ceiling of 30 km. Revised and improved RRAs are justified for the following reasons:

- 1) Needs for more definitive statistical atmospheric models have arisen because of changes and advances in aerospace technology. The Space Transportation System (Space Shuttle) is one example.
- 2) Most ranges now have an extended and improved upper air data base from which to develop a more definitive RRA.
- 3) There are requirements for RRAs for new ranges and range sites.
- 4) There have been scientific advances in understanding the upper atmospheric structure and physical relationships.
- 5) Advances in statistical modeling techniques have been made because of the general availability of high-speed electronic computers. These have led to the adoption of advanced concepts in atmospheric modeling.

For these reasons, the Range Reference Atmosphere Committee (RRAC) was tasked by the Range Commanders Council Meteorology Group (RCC MG) to establish new and improved RRAs. The purpose, scope, and objectives of this task are outlined in the following paragraphs.

**Purpose:** This committee, Task MG-1, establishes RRAs for the several ranges as provided by the RCC. An RRA is a model of the Earth's atmosphere over a geographical location of interest, for use by DOD and other U.S. Government range users. The RRA is used to provide planning data for evaluating environmental constraints for the particular configurations of environment-sensitive systems and components being developed or undergoing tests.

**Scope:** Using the best available upper atmosphere data base to include rawinsonde, rocketsonde and possibly other high-altitude data sources for the range location, the task is to establish a model of certain statistics for wind and thermodynamic quantities derived in a uniform manner and published in a standardized format.

**Objectives:** The wind statistics shall be, insofar as practical, modeled to be consistent with rigorous mathematical probability properties of the multivariate normal probability theory. The thermodynamic quantities statistics shall be, insofar as practical, modeled to be consistent with the hydrostatic equation, the equation of state, and the probability principles that are related through these physical equations. The document shall serve as an authoritative source of information and as an atmospheric model for a particular range. The first in the series of revised RRAs to be published is for Kwajalein Missile Range (KMR) (publication date December 1982). The altitude range required for KMR is 0 to 70 km. The order of priority for the subsequent publications is:

<u>Range</u>	<u>Altitude Range Required</u>
1. AFFTC/Edwards AFB, CA	0 - 70 km <sup>a</sup>
2. ESMC/Cape Canaveral AFS, FL	0 - 70 km
3. WSMC/Vandenberg AFB, CA	0 - 70 km <sup>a</sup>
4. WSMR/White Sands, NM	0 - 70 km
5. PMTC/Point Mugu, CA	0 - 70 km
6. UTTR/Dugway (Michael AAF), UT	0 - 30 km <sup>b</sup>
7. AD/Eglin AFB, FL	0 - 30 km
8. ESMC/Ascension Island	0 - 70 km (Terminates at 66 km because of insufficient data)
9. NASA/Wallops Flight Center, VA	0 - 70 km
10. Taquac (Guam)	0 - 30 km
11. PMTC/Barking Sands, HI	0 - 70 km

In keeping with the RCC's objective of standardization, the modeling techniques, basic text, and tabulation format are to be the same for all RRAs. These new and revised RRAs present not only the mean values of the thermodynamic quantities (pressure, temperature, virtual temperature, and density), but also include statistical measures for the dispersion (i.e., standard deviations and skewness coefficients). New quantities presented are water vapor pressure and dewpoint temperature. The statistical modeling for the wind is entirely new. The new approach uses the properties of the bivariate normal probability distribution function.

- a. Use rocketsonde data from PMTC/Point Mugu for altitudes above 30 km.
- b. Consider augmenting data base from Ely or Salt Lake City.

All final computations were performed by the United States Air Force Environmental Technical Applications Center (USAFETAC) in response to a task from Eastern Space and Missile Center (ESMC).

The text was prepared jointly by USAFETAC and the NASA/George C. Marshall Space Flight Center's Space Sciences Laboratory, Atmospheric Sciences Division. The editing and preparation of the draft manuscript were performed by the NASA/MSFC organization.

The cochairmen express their gratitude to all RRAC members and their respective colleagues who have made significant technical contributions to the establishment of these RRAs.

Special thanks are tendered to Lt. B. Novograd for his diligence in forming the many computations and the development of the primary tables, I through IV. Special thanks goes to Lt. F. Wirsing for editing and formulating the equations for the derivable thermodynamic equations. These gentlemen performed this outstanding work under the direction of Major B. Lilius, USAFETAC.

Grateful acknowledgment goes to Mrs. Annette Tingle, NASA/MSFC, for editing the draft manuscript.

The RRAC consists of representatives from the U.S. Air Force, U.S. Army, National Aeronautics and Space Administration, U.S. Navy, and National Oceanic and Atmospheric Administration. The committee members for the RRA for the first publication are:

G. G. Boire, WSMC  
O. H. Daniel, ESMC  
R. de Violini, PMTC  
F. G. Finger, NOAA/NWS  
E. E. Fisher, HQ AFSC  
B. R. Hixon, PMTC  
J. M. Hobbie, KMR  
E. J. Keppel, AD  
S. F. Kubinski, WSMR  
F. J. Schmidlin, NASA/WFC

O. E. Smith  
Cochairman, NASA/MSFC

Maj. B. W. Galusha  
Cochairman, USAF/ETAC

## INSTRUCTIONS FOR PREPARATION OF REPORT DOCUMENTATION PAGE

**RESPONSIBILITY.** The controlling DoD office will be responsible for completion of the Report Documentation Page, DD Form 1473, in all technical reports prepared by or for DoD organizations.

**CLASSIFICATION.** Since this Report Documentation Page, DD Form 1473, is used in preparing announcements, bibliographies, and data banks, it should be unclassified if possible. If a classification is required, identify the classified items on the page by the appropriate symbol.

### COMPLETION GUIDE

**General.** Make Blocks 1, 4, 5, 6, 7, 11, 13, 15, and 16 agree with the corresponding information on the report cover. Leave Blocks 2 and 3 blank.

**Block 1.** Report Number. Enter the unique alphanumeric report number shown on the cover.

**Block 2.** Government Accession No. Leave Blank. This space is for use by the Defense Documentation Center.

**Block 3.** Recipient's Catalog Number. Leave blank. This space is for the use of the report recipient to assist in future retrieval of the document.

**Block 4.** Title and Subtitle. Enter the title in all capital letters exactly as it appears on the publication. Titles should be unclassified whenever possible. Write out the English equivalent for Greek letters and mathematical symbols in the title (see "Abstracting Scientific and Technical Reports of Defense-sponsored RDT/E," AD-667 000). If the report has a subtitle, this subtitle should follow the main title, be separated by a comma or semicolon if appropriate, and be initially capitalized. If a publication has a title in a foreign language, translate the title into English and follow the English translation with the title in the original language. Make every effort to simplify the title before publication.

**Block 5.** Type of Report and Period Covered. Indicate here whether report is interim, final, etc., and, if applicable, inclusive dates of period covered, such as the life of a contract covered in a final contractor report.

**Block 6.** Performing Organization Report Number. Only numbers other than the official report number shown in Block 1, such as series numbers for in-house reports or a contractor/grantee number assigned by him, will be placed in this space. If no such numbers are used, leave this space blank.

**Block 7.** Author(s). Include corresponding information from the report cover. Give the name(s) of the author(s) in conventional order (for example, John R. Doe or, if author prefers, J. Robert Doe). In addition, list the affiliation of an author if it differs from that of the performing organization.

**Block 8.** Contract or Grant Number(s). For a contractor or grantee report, enter the complete contract or grant number(s) under which the work reported was accomplished. Leave blank in in-house reports.

**Block 9.** Performing Organization Name and Address. For in-house reports enter the name and address, including office symbol, of the performing activity. For contractor or grantee reports enter the name and address of the contractor or grantee who prepared the report and identify the appropriate corporate division, school, laboratory, etc., of the author. List city, state, and ZIP Code.

**Block 10.** Program Element, Project, Task Area, and Work Unit Numbers. Enter here the number code from the applicable Department of Defense form, such as the DD Form 1498, "Research and Technology Work Unit Summary" or the DD Form 1634, "Research and Development Planning Summary," which identifies the program element, project, task area, and work unit or equivalent under which the work was authorized.

**Block 11.** Controlling Office Name and Address. Enter the full, official name and address, including office symbol, of the controlling office. (Equates to funding/sponsoring agency. For definition see DoD Directive 5200.20, "Distribution Statements on Technical Documents.")

**Block 12.** Report Date. Enter here the day, month, and year or month and year as shown on the cover.

**Block 13.** Number of Pages. Enter the total number of pages.

**Block 14.** Monitoring Agency Name and Address (if different from Controlling Office). For use when the controlling or funding office does not directly administer a project, contract, or grant, but delegates the administrative responsibility to another organization.

**Blocks 15 & 15a.** Security Classification of the Report: Declassification/Downgrading Schedule of the Report. Enter in 15 the highest classification of the report. If appropriate, enter in 15a the declassification/downgrading schedule of the report, using the abbreviations for declassification/downgrading schedules listed in paragraph 4-207 of DoD 5200.1-R.

**Block 16.** Distribution Statement of the Report. Insert here the applicable distribution statement of the report from DoD Directive 5200.20, "Distribution Statements on Technical Documents."

**Block 17.** Distribution Statement (of the abstract entered in Block 20, if different from the distribution statement of the report). Insert here the applicable distribution statement of the abstract from DoD Directive 5200.20, "Distribution Statements on Technical Documents."

**Block 18.** Supplementary Notes. Enter information not included elsewhere but useful, such as: Prepared in cooperation with . . . Translation of (or by) . . . Presented at conference of . . . To be published in . . .

**Block 19.** Key Words. Select terms or short phrases that identify the principal subjects covered in the report, and are sufficiently specific and precise to be used as index entries for cataloging, conforming to standard terminology. The DoD "Thesaurus of Engineering and Scientific Terms" (TEST), AD-672 000, can be helpful.

**Block 20.** Abstract. The abstract should be a brief (not to exceed 200 words) factual summary of the most significant information contained in the report. If possible, the abstract of a classified report should be unclassified and the abstract to an unclassified report should consist of publicly-releasable information. If the report contains a significant bibliography or literature survey, mention it here. For information on preparing abstracts see "Abstracting Scientific and Technical Reports of Defense-Sponsored RDT&E," AD-667 000.

DOCUMENT 371-84

ASCENSION ISLAND, SOUTH ATLANTIC

RANGE REFERENCE ATMOSPHERE  
0-66 KM ALTITUDE

January 1984

Prepared by

Range Reference Atmosphere Committee  
Meteorology Group  
Range Commanders Council

Published by

Secretariat  
Range Commanders Council  
White Sands Missile Range, New Mexico 88002

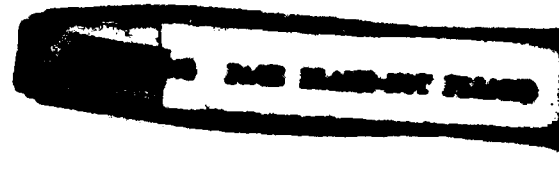


APPROVED FOR PUBLIC RELEASE: DISTRIBUTION UNLIMITED



# TABLE OF CONTENTS

	<u>PAGE</u>
LIST OF ORGANIZATION ACRONYMS. . . . .	v
FOREWORD . . . . .	vii
CHAPTER I. INTRODUCTION . . . . .	1
A. Definition and Purpose of the Range Reference Atmosphere . . . . .	1
B. Scope of the Range Reference Atmosphere and Arrangement of Tables. . . . .	1
C. Data Quality Control Procedures. . . . .	2
D. Organization of the Chapters . . . . .	3
CHAPTER II. WIND STATISTICS AND MODELS. . . . .	5
A. General Considerations . . . . .	5
B. Coordinate System and Computation of Statistical Parameters . . . . .	8
C. Statistical Wind Models. . . . .	10
D. Statistical Parameters With Respect to Any Orthogonal Axes . . . . .	25
CHAPTER III. STATISTICS OF THERMODYNAMIC QUANTITIES AND MODELS . . . . .	29
A. General Considerations . . . . .	29
B. Establishing Data Samples at the Required Altitude Levels. . . . .	32
C. Computation of Statistical Parameters for Tables II and III. . . . .	36
D. Derived Monthly Mean and Annual Mean Model Atmospheres. . . . .	39
E. Thermodynamic Quantities Derivable from the Basic Tables. . . . .	40
CHAPTER IV. CONCLUSIONS AND RECOMMENDATIONS . . . . .	47
REFERENCES . . . . .	49
CONVERSION UNITS . . . . .	53
APPENDIX A . . . . .	109
APPENDIX B . . . . .	175



# LIST OF ORGANIZATION ACRONYMS

AD	Armament Division
AFFTC	Air Force Flight Test Center
AFSC	Air Force Systems Command
AFSC/AFGL	AFSC/Air Force Geophysics Laboratory
AFSC/SD	AFSC/Space Division
AFSCF	Air Force Satellite Control Facility
AFTFWC	Air Force Tactical Fighter Weapons Center
AWS	Air Weather Service
BMD	Ballistic Missile Division
DOD	Department of Defense
DOE	Department of Energy
DOE/NTS	DOE/Nevada Test Site
DPG	Dugway Proving Ground
ESMC	Eastern Space and Missile Center
ETR	Eastern Test Range
KMR	Kwajalein Missile Range
NASA	National Aeronautics and Space Administration
NASA/MSFC	NASA/Marshall Space Flight Center
NASA/WFC	NASA/Wallops Flight Center
NOAA	National Oceanic and Atmospheric Administration
NWC	Naval Weapons Center
PMTC	Pacific Missile Test Center
USA/DTC	U.S. Army/Deseret Test Center
USAECOM	U.S. Army Electronics Command
USAFETAC	United States Air Force Environmental Technical Applications Center

UTTR	Utah Test and Training Range
WSMC	Western Space and Missile Center
WSMR	White Sands Missile Range
WTR	Western Test Range
YPG	Yuma Proving Ground
6585TG	6585th Test Group
TSCF	Targeting Systems Characterization Facility

## FOREWORD

Atmospheric parameters are essential to the research and development of missiles and aerospace vehicles. In the early 1960's, the need was recognized for realistic atmospheric models derived in a consistent manner for each of the several major test ranges. An atmospheric model derived from statistical data for a particular geographical location is referred to as a reference atmosphere.

The first Range Reference Atmosphere (RRA) was issued in 1963 by the Inter-Range Instrumentation Group (IRIG) for Cape Kennedy, Florida, and was followed by additional publications for several ranges up to 1974. Since that time, improved upper air data bases have become available from which to develop the RRA. These resulted from the extended period of records and from improvement in the upper air measuring program by rocketsondes for altitudes above the rawinsonde ceiling of 30 km. Revised and improved RRAs are justified for the following reasons:

- 1) Needs for more definitive statistical atmospheric models have arisen because of changes and advances in aerospace technology. The Space Transportation System (Space Shuttle) is one example.
- 2) Most ranges now have an extended and improved upper air data base from which to develop a more definitive RRA.
- 3) There are requirements for RRAs for new ranges and range sites.
- 4) There have been scientific advances in understanding the upper atmospheric structure and physical relationships.
- 5) Advances in statistical modeling techniques have been made because of the general availability of high-speed electronic computers. These have led to the adoption of advanced concepts in atmospheric modeling.

For these reasons, the Range Reference Atmosphere Committee (RRAC) was tasked by the Range Commanders Council Meteorology Group (RCC MG) to establish new and improved RRAs. The purpose, scope, and objectives of this task are outlined in the following paragraphs.

Purpose: This committee, Task MG-1, establishes RRAs for the several ranges as provided by the RCC. An RRA is a model of the Earth's atmosphere over a geographical location of interest, for use by DOD and other U.S. Government range users. The RRA is used to provide planning data for evaluating environmental constraints for the particular configurations of environment-sensitive systems and components being developed or undergoing tests.

Scope: Using the best available upper atmosphere data base to include rawinsonde, rocketsonde and possibly other high-altitude data sources for the range location, the task is to establish a model of certain statistics for wind and thermodynamic quantities derived in a uniform manner and published in a standardized format.

**Objectives:** The wind statistics shall be, insofar as practical, modeled to be consistent with rigorous mathematical probability properties of the multivariate normal probability theory. The thermodynamic quantities statistics shall be, insofar as practical, modeled to be consistent with the hydrostatic equation, the equation of state, and the probability principles that are related through these physical equations. The document shall serve as an authoritative source of information and as an atmospheric model for a particular range. The first in the series of revised RRAs to be published is for Kwajalein Missile Range (KMR) (publication date December 1982). The altitude range required for KMR is 0 to 70 km. The order of priority for the subsequent publications is:

<u>Range</u>	<u>Altitude Range Required</u>
1. AFFTC/Edwards AFB, CA	0 - 70 km <sup>a</sup>
2. ESMC/Cape Canaveral AFS, FL	0 - 70 km
3. WSMC/Vandenberg AFB, CA	0 - 70 km <sup>a</sup>
4. WSMR/White Sands, NM	0 - 70 km
5. PMTC/Point Mugu, CA	0 - 70 km
6. UTTR/Dugway (Michael AAF), UT	0 - 30 km <sup>b</sup>
7. AD/Eglin AFB, FL	0 - 30 km
8. ESMC/Ascension Island	0 - 70 km (Terminates at 66 km because of insufficient data)
9. NASA/Wallops Flight Center, VA	0 - 70 km
10. Taquac (Guam)	0 - 30 km
11. PMTC/Barking Sands, HI	0 - 70 km

In keeping with the RCC's objective of standardization, the modeling techniques, basic text, and tabulation format are to be the same for all RRAs. These new and revised RRAs present not only the mean values of the thermodynamic quantities (pressure, temperature, virtual temperature, and density), but also include statistical measures for the dispersion (i.e., standard deviations and skewness coefficients). New quantities presented are water vapor pressure and dewpoint temperature. The statistical modeling for the wind is entirely new. The new approach uses the properties of the bivariate normal probability distribution function.

- a. Use rocketsonde data from PMTC/Point Mugu for altitudes above 30 km.*  
*b. Consider augmenting data base from Ely or Salt Lake City.*

All final computations were performed by the United States Air Force Environmental Technical Applications Center (USAFETAC) in response to a task from Eastern Space and Missile Center (ESMC).

The text was prepared jointly by USAFETAC and the NASA/George C. Marshall Space Flight Center's Space Sciences Laboratory, Atmospheric Sciences Division. The editing and preparation of the draft manuscript were performed by the NASA/MSFC organization.

The cochairmen express their gratitude to all RRAC members and their respective colleagues who have made significant technical contributions to the establishment of these RRAs.

Special thanks are tendered to Lt. B. Novograd for his diligence in forming the many computations and the development of the primary tables, I through IV. Special thanks goes to Lt. F. Wirsing for editing and formulating the equations for the derivable thermodynamic equations. These gentlemen performed this outstanding work under the direction of Major B. Lilius, USAFETAC.

Grateful acknowledgment goes to Mrs. Annette Tingle, NASA/MSFC, for editing the draft manuscript.

The RRAC consists of representatives from the U.S. Air Force, U.S. Army, National Aeronautics and Space Administration, U.S. Navy, and National Oceanic and Atmospheric Administration. The committee members for the RRA for the first publication are:

G. G. Boire, WSMC  
O. H. Daniel, ESMC  
R. de Violini, PMTC  
F. G. Finger, NOAA/NWS  
E. E. Fisher, HQ AFSC  
B. R. Hixon, PMTC  
J. M. Hobbie, KMR  
E. J. Keppel, AD  
S. F. Kubinski, WSMR  
F. J. Schmidlin, NASA/WFC

O. E. Smith  
Cochairman, NASA/MSFC

Maj. B. W. Galusha  
Cochairman, USAF/ETAC

## CHAPTER I. INTRODUCTION

### A. Definition and Purpose of the Range Reference Atmosphere

#### A.1 Definition

A reference atmosphere is a statistical model of the Earth's atmosphere derived from upper air measurements over a particular geographical location. Hence, these Range Reference Atmospheres (RRAs) are atmospheric models developed by the Range Reference Atmosphere Committee (RRAC) in response to a task by the Range Commanders Council Meteorology Group (RCC MG) and published by the RCC Secretariat. The RCC MG, formerly called the Inter-Range Instrumentation Group/Meteorology Working Group (IRIG/MWG), published a series of RRAs during the period 1963 through 1974.

#### A.2 Purpose

A series of revised and expanded RRAs are to be published for locations of interest to the RCC. These publications are to serve as authoritative reference sources on certain upper air statistics and as atmospheric models for particular range sites. The technical usefulness of these documents for the ranges, range users, U.S. aerospace industries, and the scientific community is recognized because of the standardization of the development techniques and the presentation of the tabulations.

### B. Scope of the Range Reference Atmosphere and Arrangement of Tables

#### B.1 Scope

The RRA contains tabulations for monthly and annual means, standard deviations, and skewness coefficients for windspeed, pressure, temperature, density, water vapor pressure, virtual temperature, and dewpoint temperature; the means and standard deviations for the zonal (U) and meridional (V) wind components; and the linear (product moment) correlation coefficient between the wind components. These statistical parameters are tabulated at the station elevation, at 1-km intervals from sea level to 30 km, and at 2-km intervals from 30 to 90 km. The wind statistics are given at approximately 10 m above the station elevations and at altitudes with respect to mean sea level thereafter. For those range sites without rocketsonde measurements, the RRAs terminate at 30 km altitude, or they are extended, if required, when rocketsonde data from a nearby launch site are available. There are four sets of tables for each of the 12 monthly reference periods and the annual reference period.

#### B.2 Arrangement of Tables

The statistical parameters for the RRA models are presented in four tables, as outlined in the following paragraphs.

Table I contains all the wind statistical parameters. This table gives the monthly and annual means and standard deviations of the U and V wind components and the linear (product moment) correlation coefficient between these

two components; the mean, standard deviation and skewness coefficient of the windspeed, and the number of wind observations (sample size).

Table II contains the monthly and annual means, standard deviations, and skewness values of pressure, temperature, and density, and the number of observations used for each of these thermodynamic quantities.

Table III contains the monthly and annual means, standard deviations and skewness values of the water vapor pressure, virtual temperature and dewpoint, and the number of observations for each of these moisture-related quantities. The statistical parameters for water vapor pressure and dewpoint terminate at 15 km altitude. Above 15 km the statistical parameters for virtual temperature are considered to be the same as those for temperature.

Table IV contains the monthly and annual mean atmospheric models for the thermodynamic variables: pressure, virtual temperature, and density. This table is derived from the monthly and annual mean virtual temperature versus altitude (geometric) using the hydrostatic equation and the equation of state. Also presented is the geopotential height corresponding to the tabulated geometric altitudes.

The physical unit for all wind parameters is meters per second. The physical unit for pressure is millibars; for temperature and virtual temperature, degrees Kelvin; for density, grams per cubic meter; and for water vapor pressure, millibars. In all cases the skewness coefficient and the correlation coefficient between wind components are unitless. All reference to altitude is geometric altitude and is expressed in kilometers. All reference to height is geopotential height and has the unit geopotential meters or kilometers. All geometric altitudes and geopotential heights are with respect to mean sea level.

#### C. Data Quality Control Procedures

A small portion (less than 10 percent) of the soundings in the data base used to calculate the RRA tables contained erroneous data values. The soundings which contained these erroneous values were eliminated from the data base using the following procedures:

- 1) Soundings containing gaps in their height data greater than 200 mb were rejected. This step was taken because some soundings only contained height values at their "mandatory" pressure levels, which were occasionally missing, resulting in soundings with no height information at all.

- 2) An initial set of RRA statistics was computed using all the remaining soundings. This initial set of statistics was used to determine data limits for the temperature, pressure, U and V components of the wind, and the dewpoint (for the 0- to 30-km portion of the RRA) or the density (for the 30- to 90-km portion of the RRA). The lower (upper) data limits were set at the mean value for a specific parameter, minus (plus) six standard deviations of that quantity. One pair of data limits was computed for each of these parameters: month of the year and data level.



3) This initial set of data limits was then used to screen the data base. All the soundings that contained values outside these data limits were rejected. A new RRA was then computed using the screened data base. This second RRA was used to generate a second set of data limits.

4) The second set of data limits was then used to screen the data base further. A new RRA was again generated. The skewness values in this RRA were then evaluated, according to empirical criteria specified in section II.A.3 of this document for the winds, and according to criteria in section III.A.3 for the thermodynamic quantities. If these criteria were satisfied, the new RRA was then used to generate a final set of data limits, which were used to control the quality of the data base for the final version of the RRA.

5) Occasionally, the third RRA that was generated did not satisfy all of the skewness criteria. This indicated that some incorrect values were still present in the data base. To complete quality control, steps 3 and 4 were repeated for additional iterations (usually one or two) until the resulting RRA satisfied the skewness criteria. At that point, a final set of data limits was generated. This final set of data limits was then used to control the quality of the data base and generate the final RRA.

#### D. Organization of the Chapters

Because there are plans to publish a series of RRAs, comments on the special organization of the document are in order. The RRA document is arranged in four chapters. Chapter I is the introduction. Chapter II, Wind Statistics and Models, contains the techniques used to arrive at the wind statistical parameters, table I, and the probability functions that are to be used as wind models to derive several wind statistics. Chapter III, Statistics of Thermodynamic Quantities and Models, contains the techniques used to arrive at the thermodynamic and moisture-related statistical parameters given in tables II and III and the atmospheric thermodynamic model presented in table IV. This chapter also contains sets of equations to calculate several atmospheric properties. Chapter IV contains the general conclusions and recommendations. These four chapters are reprinted without change for each documented RRA to assure consistency and for expediency in preparing the documentation. To account for variations particular to a specific RRA, two appendixes have been included. Appendix A, Examples of Wind Statistics, is designed to give a few illustrative examples of wind statistics for the specific RRA and cursory observations, comparisons, or comments on wind statistics. Appendix B, Range Specific Information, is designed to present specific information particular to the range, such as geographical location, data base, etc., and any cursory observations or comments on the thermodynamic quantities.

Read these appendixes! They are located as the last two units in the document because they may vary in length depending on the circumstances. Appendixes A and B and tables I, II, III, and IV are the only differences among the RRA documents published in this new RRA series.

## CHAPTER II. WIND STATISTICS AND MODELS

### A. General Considerations

#### A.1. Objectives

An objective of the RRA is to furnish minimum tabulation for the wind statistics. To meet this objective, the bivariate normal probability distribution was adopted as a statistical model for the wind treated as a vector quantity at the RRA data levels. Only five statistical parameters are required to completely describe this probability function. In Cartesian coordinates these parameters are the means and standard deviations of the two orthogonal components and the correlation coefficient between the two components. These five statistical parameters for the U and V (meteorological coordinates) components are given in table I. The statistical properties of the bivariate normal probability distribution are used to derive many wind statistics that are of interest to the ranges and range users. This procedure produces consistent wind statistics that are connected through rigorous mathematical probability functions. By using these functions, extensive tabulations of wind statistics are avoided.

The statistical properties of the bivariate normal probability distribution presented for the vector wind statistical model are:

- 1) The wind components are univariate normally distributed.
- 2) The conditional distribution of one component given a value of the other component is univariate normally distributed.
- 3) The windspeed is of the form of a generalized Rayleigh distribution.
- 4) The frequency distribution of wind direction can be derived.
- 5) The conditional distribution of windspeed given a value of wind direction (wind rose) can be derived.
- 6) The five tabulated wind statistical parameters with respect to the meteorological U and V coordinate system can be derived for any arbitrary rotation of the orthogonal axes.

The probability distribution functions and sets of equations to derive wind statistics for the previously stated properties of the vector wind model are presented in this chapter. Symbols used are summarized in table A. Illustrative examples are presented in appendix A. No attempt is made to give the derivation of the probability functions. The reader is referred to Smith (1976) for some derivations and several applications of the probability distribution properties for wind statistics.

#### A.2. Data Quality Control

The U and V components of the wind were used to generate data limits set at plus and minus six standard deviations from the mean for each of the

TABLE A. LIST OF SYMBOLS USED IN CHAPTER II

N	- The number of wind measurements in table I
r	- A general variable for the bivariate normal probability distribution in polar coordinates
R	- A generalized Rayleigh variable used for derived windspeed probability distribution
R (U, V)	- The linear (product moment) correlation coefficient between the zonal and meridional wind components in table I
SK (W)	- Skewness parameter for windspeed in table I
S (U)	- The standard deviation of the zonal wind component in table I
S (V)	- The standard deviation of the meridional wind component in table I
S (W)	- The standard deviation of windspeed in table I
t	- A standardized normal variate used in text table B
U	- The zonal wind component
UBAR	- The mean value of the zonal wind component in table I
V	- The meridional wind component
VBAR	- The mean value of the meridional wind component in table I
W	- Windspeed or modulus of wind vector, a scalar quantity
WBAR	- The mean value of windspeed in table I
X	- A general component variable or coordinate axis
Y	- A general component variable or coordinate axis
$\bar{X}$	- A general component mean value in the [x,y] coordinate system
$\bar{Y}$	- A general component mean value in the [x,y] coordinate system
$\alpha$ (alpha)	- Rotation angle for the [x,y] coordinate system

TABLE A. (concluded)

$\theta$  (theta) - Wind direction in the polar coordinate system

$\lambda_{( )}$  (Lambda) - A parameter in the bivariate normal probability distribution in text table C

$\xi$  (Xi) - The mean value in the standardized normal probability distribution used in text table B

$\pi$  (Pi) - Constant = 3.14159 ...

$\rho$  (Rho) - The general linear correlation coefficient between the two component variables in the [x,y] coordinate system

$\sigma_x, \sigma_y$  - The general standard deviations of the x and y component variables in the [x,y] coordinate system.

quantities. These data limits were used to screen the wind data base, as described in section I.C. The data base was considered to be free from errors under the following conditions:

- 1) The skewness of the windspeed was below 4.0 at data levels where the mean windspeed was less than 15 m/s, and
- 2) The skewness of the windspeed was below 2.5 at data levels where the mean windspeed was greater than 15 m/s.

### A.3 Limitations

For the wind statistics, the correlation coefficients for like wind components and unlike wind components between altitude levels were not computed. Therefore, wind statistics with respect to altitude (profile) cannot be derived from the RRA statistics. For wind profile modeling techniques the user is referred to Smith (1976). However, the wind statistics at discrete altitudes are valid; all of the probability distribution functions given in chapter II can be derived from the five wind component statistical parameters contained in table I, and the derived distributions can be considered as wind models at discrete altitudes.

By convention, in the statistical literature Greek letters are used for population or theoretically known parameters, and sample estimates are denoted by English alphabetical letters or with a "hat" (^) over the Greek letters. In chapter II Greek letters are used for the variances and the linear correlation coefficient, and the means are denoted by  $\bar{X}$  and  $\bar{Y}$  when dealing with the bivariate normal distribution. It will always be understood that table I contains sample estimates of the statistical parameters and they are with respect to the meteorological U and V coordinate system.

## B. Coordinate System and Computation of Statistical Parameters

### B.1. Coordinate System

Wind measurements are recorded in terms of magnitude and direction. The wind direction is measured in degrees clockwise from true north and is the direction from which the wind is blowing. The wind magnitude (the modulus of the vector) is the scalar quantity and is referred to as windspeed or scalar wind. A statistical description that accounts for the wind as a vector quantity is appropriate and requires a coordinate system.

For the RRA the standard meteorological coordinate system has been chosen for the wind statistics, all tables of statistical parameters, and related discussions because the coordinate system used in aerospace and related applied fields has not always been consistent.

Using figure 1, the polar and Cartesian forms for the meteorological coordinate system are defined:

$W$  = windspeed, scalar wind, or magnitude of the wind vector in meters per second.

$\theta$  = wind direction.  $\theta$  is measured in degrees clockwise from true north and is the direction from which the wind is blowing.

$U$  = zonal wind component, positive west to east, in meters per second.

$V$  = meridional wind component, positive south to north, in meters per second.

The components  $\theta$  and  $W$  define the polar form, and the  $U$ - $V$  components define the Cartesian forms:

$$U = -W \sin \theta \quad , \quad 0 \leq \theta \leq 360^\circ \quad (1)$$

$$V = -W \cos \theta \quad . \quad (2)$$

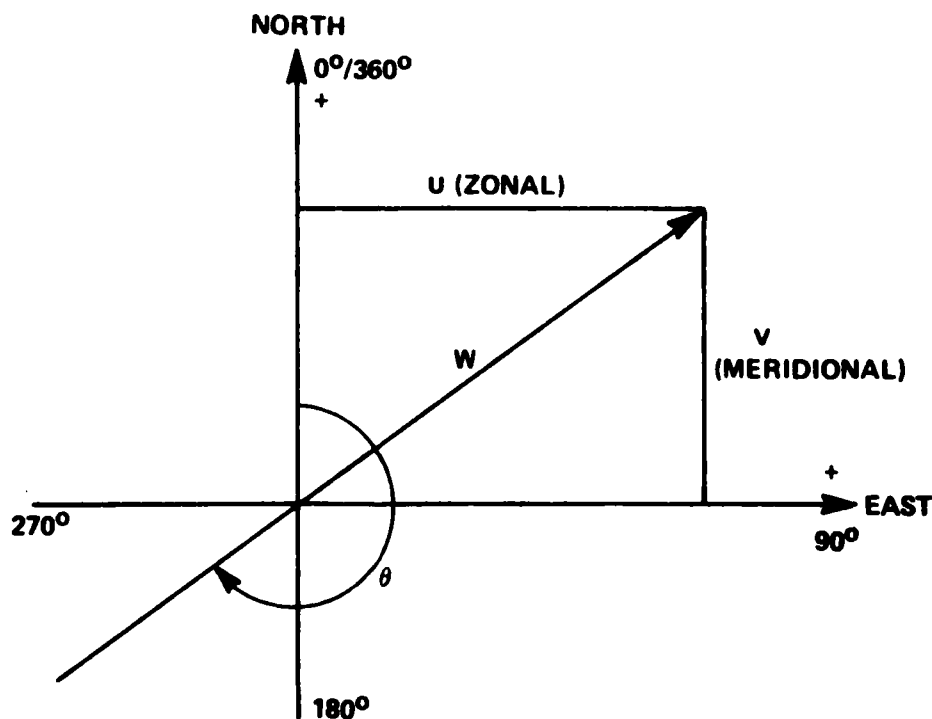


Figure 1. The meteorological coordinate system.

It is helpful to note the difference between the mathematical convention for a vector direction and the meteorological convention for wind direction:

$$\theta_{\text{met}} = 270 - \theta_{\text{math}} \quad (3)$$

when  $0 \leq \theta_{\text{math}} \leq 270^\circ$

$$\theta_{\text{met}} = 360 + (270 - \theta_{\text{math}})$$

when  $270 \leq \theta_{\text{math}} \leq 360^\circ$

## B.2 Computation of Statistical Parameters

The wind statistical parameters in table I for the means and standard deviations of the U and V wind components and windspeed and the skewness parameter of windspeed were computed using the sums technique presented in chapter III.C.3. In addition, the linear (product moment) correlation coefficient between the U and V wind components,  $r(u,v)$  in table I, was computed. This correlation coefficient is defined as

$$r(u,v) = \frac{\sum_{i=1}^n (U_i - \bar{U})(V_i - \bar{V})}{N s(u) \cdot s(v)} \quad (4)$$

These statistical parameters are with respect to the Standard Meteorological Coordinate System.

## C. Statistical Wind Models

### C.1. Wind Component Statistics

The univariate normal (Gaussian) probability distribution function is used to obtain wind component statistics. In generalized notations, this probability density function (pdf) is

$$f(t) = \frac{e^{-\frac{t^2}{2}}}{\sqrt{2\pi}} \quad (5)$$

where  $t = X - \xi / \sigma_x$  is the standardized variate, with  $\xi$  defining the mean and  $\sigma_x$  the standard deviation. The probability distribution function (PDF) is

$$F(X) = \int_{-\infty}^X f(t) dt \quad (6)$$

Because this integral cannot be obtained in closed form, it is widely tabulated for zero mean and unit standard deviation. For a convenient reference for the RRA, selected values of  $F(X)$  are given in table B. To emphasize the connotation of probability,  $F(X)$  is shown in table B as  $P\{X\}$ .

The  $t$  values in table B are used as multiplier factors to the standard deviation to express the probability that a normally distributed variable,  $X$ , is less than or equal to a given value as

$$P\{X \leq \text{mean} + t \sigma_X\} = \text{probability, } p \quad (7)$$

For example, when  $t = 1.6449$ , the probability that  $X$  is less than or equal to the mean plus 1.6449 standard deviations is 0.95. That value of  $X$  that is less than or equal to the mean plus 1.6449 standard deviations is called the 95th percentile value of  $X$ . Also given in table B are the numerical values to express the probability that  $X$  falls in the interval  $X_1$  and  $X_2$ ; i.e.,

$$P\{X_1 \leq X \leq X_2\} = \text{Interpercentile Range} \quad (8)$$

where

$$X_1 = \bar{X} - t \sigma_X$$

$$X_2 = \bar{X} + t \sigma_X$$

For  $t = 1.9602$  the probability that  $X$  lies in the interval  $X_1$  and  $X_2$  is 0.95. The values of  $X_1$  and  $X_2$  in this example comprise the 95th interpercentile range.

For a normally distributed variable, the mode (most frequent value) and the median (50th percentile value) are the same as the mean value. The means and standard deviations of the  $U$  and  $V$  wind components from table 1 are used in equations (7) and (8) to compute the percentile values and interpercentile ranges of the  $U$  and  $V$  wind components. When equation (7) is illustrated on a normal probability graph, a straight line is formed.

## C.2. The Vector Wind Model

Because wind is a vector quantity having direction and magnitude that can be expressed as two components in an orthogonal coordinate system, a probability model that describes the joint relationship is the bivariate normal probability distribution. In general component notation, the bivariate normal probability density function (BNpdf) is



TABLE B. VALUES OF  $t$  FOR STANDARDIZED NORMAL  
(UNIVARIATE) DISTRIBUTION FOR PERCENTILES  
AND INTERPERCENTILE RANGES

$t$	$P(X)$	$X$	$P\{X_1 \leq X \leq X_2\} (\%)$
-3.0000	0.00135	$\xi - 3.0000 \sigma$	
-2.5758	0.00500	$\xi - 2.5758 \sigma$	
-2.3263	0.01000	$\xi - 2.3263 \sigma$	
-2.2365	0.01266	$\xi - 2.2365 \sigma$	
-2.0000	0.02275	$\xi - 2.0000 \sigma$	
-1.9602	0.02500	$\xi - 1.9602 \sigma$	
-1.6449	0.05000	$\xi - 1.6449 \sigma$	
-1.2816	0.10000	$\xi - 1.2816 \sigma$	
-1.0000	0.15866	$\xi - 1.0000 \sigma$	
-0.8416	0.20000	$\xi - 0.8416 \sigma$	
-0.6745	0.25000	$\xi - 0.6745 \sigma$	
-0.2533	0.40000	$\xi - 0.2533 \sigma$	
0.0000	0.50000	$\xi$	
0.2533	0.60000	$\xi + 0.2533 \sigma$	
0.6745	0.75000	$\xi + 0.6745 \sigma$	
0.8416	0.80000	$\xi + 0.8614 \sigma$	
1.0000	0.84134	$\xi + 1.0000 \sigma$	
1.2816	0.90000	$\xi + 1.2816 \sigma$	
1.6449	0.95000	$\xi + 1.6449 \sigma$	
1.9602	0.97502	$\xi + 1.9602 \sigma$	
2.0000	0.97725	$\xi + 2.0000 \sigma$	
2.2365	0.98734	$\xi + 2.2365 \sigma$	
2.3263	0.99000	$\xi + 2.3263 \sigma$	
2.5758	0.99500	$\xi + 2.5758 \sigma$	
3.0000	0.99865	$\xi + 3.0000 \sigma$	

where  $X_1 = \xi - t\sigma$   
and  $X_2 = \xi + t\sigma$

$$f(X,Y) = \frac{1}{2\pi\sigma_x\sigma_y\sqrt{1-\rho^2}} \left[ \exp \frac{-1}{2(1-\rho^2)} \left\{ \frac{(X-\bar{X})^2}{\sigma_x^2} - \frac{2\rho(X-\bar{X})(Y-\bar{Y})}{\sigma_x\sigma_y} + \frac{(Y-\bar{Y})^2}{\sigma_y^2} \right\} \right] \quad -\infty \leq X \leq \infty \text{ and } -\infty \leq Y \leq \infty \quad (9)$$

where the five parameters are  $\bar{x}, \bar{y}$ , the component means;  $\sigma_x, \sigma_y$ , the component standard deviations; and  $\rho$ , the correlation coefficient between the two component variables,  $X$  and  $Y$ .

For many applications the interest is in determining the probability that a point  $\{X, Y\}$  will fall within a contour of equal probability density. The exponential terms of equation (9), when set equal to a constant,  $\lambda^2$ , give a family of ellipses depending on the value of the constant. The ellipses have a common center at the point  $\{\bar{X}, \bar{Y}\}$ . Integration of equation (9) over the region bounded by the contours of equal probability density gives

$$P(\lambda) = 1 - e^{-\frac{\lambda^2}{2(1-\rho^2)}} \quad (10)$$

Solving for  $\lambda^2$  and replacing  $P(\lambda)$  by  $p$  gives

$$\lambda^2 = -2(1-\rho^2) \ln(1-p) \quad (11)$$

Now define

$$\lambda_e = \sqrt{2} \sqrt{-\ln(1-p)} \quad (12)$$

For ready reference and comparisons,  $\lambda_e$  is shown in table C for selected values of  $p$ .

TABLE C. VALUES OF  $\lambda$  FOR BIVARIATE NORMAL  
DISTRIBUTION ELLIPSES AND CIRCLES

P(%)	$\lambda_c$ (ellipse)	$\lambda_c$ (circle)	P(%)	$\lambda_c$ (ellipse)	$\lambda_c$ (circle)
0.000	0.0000	0.0000	65.000	1.4490	1.0246
5.000	0.3203	0.2265	68.268	1.5151	1.0713
10.000	0.4590	0.3246	70.000	1.5518	1.0973
15.000	0.5701	0.4031	75.000	1.6651	1.1774
20.000	0.6680	0.4723	80.000	1.7941	1.2686
25.000	0.7585	0.5363	85.000	1.9479	1.3774
30.000	0.8446	0.5972	86.466	2.0000	1.4142
35.000	0.9282	0.6563	90.000	2.1460	1.5175
39.347	1.0000	0.7071	95.000	2.4477	1.7308
40.000	1.0108	0.7147	95.450	2.4860	1.7579
45.000	1.0935	0.7732	98.000	2.7971	1.9778
50.000	1.1774	0.8325	98.168	2.8284	2.0000
54.406	1.2533	0.8862	98.889	3.0000	2.1213
55.000	1.2637	0.8936	99.000	3.0348	2.1460
60.000	1.3537	0.9572	99.730	3.4393	2.4320
63.212	1.4142	1.0000	99.9877	4.2426	3.0000
$\lambda_c = \sqrt{2} \sqrt{-\ln(1-P)}$ $\lambda_c = \sqrt{-\ln(1-P)}$					

The probability ellipse that contains p-percent of the wind vectors expressed in the most general form is the conic defined by

$$AX^2 + BXY + CY^2 + DX + EY + F = 0 \quad , \quad (13)$$

where

$$A = \sigma_y^2$$

$$B = -2\rho\sigma_x\sigma_y$$

$$C = \sigma_x^2$$

$$D = 2\sigma_x\sigma_y \rho \bar{Y} - 2\sigma_y^2 \bar{X} = - (B\bar{Y} + 2A\bar{X})$$

$$E = 2\sigma_x\sigma_y \rho \bar{X} - 2\sigma_x^2 \bar{Y} = - (B\bar{X} + 2C\bar{Y})$$

$$F = A\bar{X}^2 + C\bar{Y}^2 + B\bar{X}\bar{Y} - AC (1 - \rho^2) \lambda_e^2 \quad ,$$

and

$$\lambda_e = \sqrt{2} \sqrt{-\ln (1 - \rho)} \quad .$$

For graphical presentations, the range of the variable is important in order to arrange the scale. The largest and smallest values of X and Y for a given probability ellipse, p, are given by

$$X_{L,S} = \bar{X} \pm \sigma_x \lambda_e \quad (14)$$

$$Y_{L,S} = \bar{Y} \pm \sigma_y \lambda_e \quad , \quad (15)$$

where, as before,  $\lambda_e = \sqrt{2} \sqrt{-\ln (1 - p)}$  .

Although there are several approaches to graphing the probability ellipses, the following procedure is advantageous for electronic computer plotting. In establishing the computer plotting program, the sample estimates for  $\bar{X}, \bar{Y}, \sigma_x, \sigma_y$ , and  $\rho$  are constants in equation (13). The user makes the choice of probability ellipses desired. Thus,  $p$  in equation (12) is programmed as a parameter. The largest and smallest values for  $X$  and  $Y$  are computed by equations (14) and (15) for the largest probability ellipse selected. This sets the graphical scale. Values of  $X$  within the range of "X smallest" to "X largest" are obtained by incrementing  $X$  between these limits. Using the quadratic equation, a solution for  $Y$  of equation (13) is made and plotted for each value of  $X$ . The centroid  $(\bar{X}, \bar{Y})$  for the family of probability ellipses is plotted as a point. Labeling and other identification complete the plotting program.

For a given probability, equation (13) defines an ellipse that contains  $p$ -percent of the points  $X, Y$ . Since the entire area under the bivariate normal density function [equation (9)] is unity, upon integration for a given probability ellipse, that given ellipse contains  $p$ -percent of the total area. In the wind statistics,  $p$ -percent of the wind vectors fall within the specified probability ellipse. From this point of view, a specified probability ellipse gives the joint probability that  $p$ -percent of the  $U-V$  components lie within the given ellipse.

When  $\sigma_x^2 = \sigma_y^2 = \sigma^2$  and  $\rho = 0$  in the bivariate normal distribution, the probability ellipses of equation (13) reduce to circles whose centers are at the means  $\bar{X}, \bar{Y}$ . The radii of the probability circles are  $\sigma_{V1} \lambda_c$ , where

$$\sigma_{V1} = \sqrt{2\sigma^2} \quad (16)$$

and

$$\lambda_c = \sqrt{-\ln (1 - p)} \quad (17)$$

Values for  $\lambda_c$  for selected probabilities,  $p$ , are given in table C.

Because this function is simple, it can easily be graphed manually. However, the generalized plotting technique for electronic computer plotters, as represented by equation (13), can be advantageously used.

### C.3. Derived Distributions for Wind Statistics

In this subsection the probability distribution functions and sets of equations are presented to derive certain probability distribution functions for wind statistics. These derived probability distributions are:

- 1) The conditional distribution of wind components
- 2) The generalized Rayleigh distribution for windspeed
- 3) The distribution for wind direction
- 4) The conditional distribution of windspeed given a wind direction (wind rose).

The required five statistical parameters for these derived distributions for wind statistics are given in table I.

#### C.3.1 The Conditional Distribution of Wind Components

Given that two random variables  $X$  and  $Y$  are bivariate normally distributed, the conditional distribution  $f(Y|X)$  is read as  $f(Y)$  given  $X$ , and likewise  $f(X|Y)$  is read as  $f(X)$  given  $Y$ . The conditional probability distribution function  $F(Y|X)$  has the mean  $E(Y|X)$  and variance  $\sigma^2_{(Y|X)}$ , where

$$E(Y|X^*) = \bar{Y} + \rho \left( \frac{\sigma_Y}{\sigma_X} \right) (X^* - \bar{X}) \quad (18)$$

and

$$\sigma^2_{(Y|X^*)} = \sigma_Y^2 (1 - \rho^2) \quad (19)$$

The conditional standard deviation is

$$\sigma_{(Y|X^*)} = \sigma_Y \sqrt{1 - \rho^2} \quad (20)$$

By interchanging the variables and parameters, the conditional distribution function for  $F(X|Y^*)$  has the conditional mean

$$E(X|Y^*) = \bar{X} + \rho \left( \frac{\sigma_X}{\sigma_Y} \right) (Y^* - \bar{Y}) \quad , \quad (21)$$

conditional variance

$$\sigma^2_{(X|Y^*)} = \sigma_X^2 (1 - \rho^2) \quad , \quad (22)$$

and conditional standard deviation

$$\sigma_{(X|Y^*)} = \sigma_X \sqrt{1 - \rho^2} \quad . \quad (23)$$

The preceding conditional probability distribution functions are univariate normal distributions for a (fixed) given value for one of the bivariate normal variables. Thus, the t-values given in table B are applicable for conditional probability statements. For example,

$$F(Y|X^*) = E(Y|X^*) + t\sigma_{(Y|X^*)} \quad . \quad (24)$$

For  $t = 1.6449$  there is a 95 percent chance that  $Y$  is less than or equal to  $\bar{Y} + 1.6449 \sigma_{(Y|X^*)}$  given that  $X = X^*$ . In symbols this statement reads

$$P \left\{ Y \leq E(Y|X^*) + 1.6449 \sigma_{(Y|X^*)} \mid X = X^* \right\} = 0.9500 \quad . \quad (25)$$

Interval probability statements can also be made; namely,

$$P \left\{ Y_1 = E(Y|X^*) - t\sigma_{(Y|X^*)} \leq Y \leq Y_2 = E(Y|X^*) + t\sigma_{(Y|X^*)} \mid X = X^* \right\}$$

where  $X^*$  can take on any fixed value of  $X$ , but a convenient arrangement is to let  $X^* = \bar{X} \pm t\sigma_X$ .

The close connection of the regression function of  $Y$  on  $X$  to the conditional mean for the bivariate normal distribution is noted; namely,

$$Y = \bar{Y} + \rho \left( \frac{\sigma_Y}{\sigma_X} \right) (X - \bar{X}) \quad (26)$$

Similarly, the regression function of X on Y is

$$X = \bar{X} + \rho \left( \frac{\sigma_X}{\sigma_Y} \right) (Y - \bar{Y}) \quad (27)$$

These are linear functions and express the same results as would be obtained from a least-squares regression line.

### C.3.2. The Generalized Rayleigh Distribution for Windspeed

If two random variables, X and Y, are bivariate normally distributed, then the probability distribution for the modulus, R, can be derived in terms of the five parameters that define the bivariate normal distribution.

$$R = \sqrt{X^2 + Y^2} \quad (28)$$

The distribution of R so derived is called a generalized Rayleigh distribution because there are no restrictions on the parameters. For applications to the RRA, the variable R is recognized as windspeed or the modulus of the wind vector.

The probability density function for R is expressed as

$$f(R) = a_0 \text{Re}^{-a_1 R^2} \left[ I_0(a_2 R^2) I_0(a_3 R) + 2 \sum_{k=1}^{\infty} I_k(a_2 R^2) I_{2k}(a_3 R) \cos 2k\psi \right] R \geq 0 \quad (29)$$

The functions  $I_0(\cdot)$ ,  $I_k(\cdot)$ , and  $I_{2k}(\cdot)$  are the modified Bessel functions of the first kind for zero order, kth order, and 2kth order. The coefficients are



$$a_0 = \exp \left[ -\frac{1}{2} \left\{ \frac{\bar{X}^2}{\sigma_a^2} + \frac{\bar{Y}^2}{\sigma_b^2} \right\} \right] / \sigma_a \sigma_b ,$$

where  $\sigma_a^2$  and  $\sigma_b^2$  are the rotated variances to produce zero correlation between X and Y.  $\sigma_a$  and  $\sigma_b$  are the positive and negative roots<sup>1</sup> of the expression

$$\sigma_{(+,-)}^2 = \frac{1}{2} \left\{ \sigma_x^2 + \sigma_y^2 \pm \left[ (\sigma_x^2 + \sigma_y^2)^2 - 4\sigma_x^2 \sigma_y^2 (1 - \rho^2) \right]^{1/2} \right\} ,$$

$$a_1 = (\sigma_x^2 + \sigma_y^2) / 4(1 - \rho^2) \sigma_x^2 \sigma_y^2 ,$$

$$a_2 = \frac{\left[ (\sigma_x^2 - \sigma_y^2)^2 + 4\rho^2 \sigma_x^2 \sigma_y^2 \right]^{1/2}}{4(1 - \rho^2) \sigma_x^2 \sigma_y^2} ,$$

$$a_3 = \left[ \left( \frac{\bar{X}}{\sigma_a} \right)^2 + \left( \frac{\bar{Y}}{\sigma_b} \right)^2 \right]^{1/2} ,$$

1. This computational form is obtained from the determinant

$$\begin{vmatrix} \sigma_x^2 - K & \sigma_x \sigma_y \rho \\ \sigma_x \sigma_y \rho & \sigma_y^2 - K \end{vmatrix} ,$$

where K is  $\sigma_{(+,-)}^2$ , and  $\sigma_a$  and  $\sigma_b$  are analogous to the standard deviation of the major and minor axes of the bivariate normal probability ellipse.

and

$$\tan \psi = \frac{\bar{Y}}{\bar{X}} \frac{\sigma_a^2}{\sigma_b^2} .$$

Since this density function cannot be integrated in closed form from zero to R, numerical integration is used to obtain practical results for the probability distribution function; i.e.,

$$F(R) = \int_0^{R*} f(R) dR . \quad (30)$$

A number of special cases can be obtained from the general Rayleigh distribution [equation (29)], the simplest of which is to let  $\sigma_x \equiv \sigma_y = \sigma$  and  $\bar{X} = \bar{Y} = 0$  with independent variables X and Y. This gives

$$f(R) = \frac{R}{\sigma^2} e^{-R^2/2\sigma^2} , \quad (31)$$

which is recognized as the classical Rayleigh probability density function. The density function, equation (31), can be integrated in closed form over any range of the variable R. Hence, the probability distribution function, F(R), for equation (31) is

$$F(R) = 1 - \exp \left\{ \frac{-R^2}{2\sigma^2} \right\} . \quad (32)$$

### C.3.3. The Derived Distribution of Wind Direction

Considering the wind as a vector quantity and bivariate normally distributed, the wind direction can be derived. This is done by first writing the bivariate normal probability density function in polar coordinates whose variables are

$$g(r, \theta) = r d_1 e^{-\frac{1}{2} (a^2 r^2 - 2br + c^2)} \quad (33)$$

(see footnote 2)

where

$$a^2 = \frac{1}{(1 - \rho^2)} \left[ \frac{\sin^2 \theta}{\sigma_x^2} - \frac{2\rho \cos \theta \sin \theta}{\sigma_x \sigma_y} + \frac{\cos^2 \theta}{\sigma_y^2} \right]$$

$$b = \frac{-1}{(1 - \rho^2)} \left[ \frac{\bar{x} \sin \theta}{\sigma_x^2} - \frac{\rho(\bar{x} \cos \theta + \bar{y} \sin \theta)}{\sigma_x \sigma_y} + \frac{\bar{y} \cos \theta}{\sigma_y^2} \right]$$

$$c^2 = \frac{1}{(1 - \rho^2)} \left[ \frac{\bar{x}^2}{\sigma_x^2} - \frac{2\rho \bar{x} \bar{y}}{\sigma_x \sigma_y} + \frac{\bar{y}^2}{\sigma_y^2} \right]$$

$$d_1 = \frac{1}{2\rho \sigma_x \sigma_y \sqrt{1 - \rho^2}}$$

$r = \sqrt{x^2 + y^2}$  is the modulus of the vector or speed, and  $\theta$  is the direction of the vector. After integrating  $g(r, \theta)$  over  $r = 0$  to  $\infty$ , the probability density function of  $\theta$  is

$$g(\theta) = \frac{d_1}{a^2} e^{-\frac{1}{2} c^2} \left[ 1 + \sqrt{2\pi} \left( \frac{b}{a} \right) e^{\frac{1}{2} \left( \frac{b}{a} \right)^2} \Phi \left( \frac{b}{a} \right) \right] \quad (34)$$

2. This expression, equation (33), in Smith 1976) is given with respect to the mathematical convention for a vector direction.

where  $a^2$ ,  $b$ ,  $c^2$ , and  $d_1$  are as previously defined in equation (33) and

$$\phi\left(\frac{b}{a}\right) = \phi(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^x e^{-\frac{1}{2}t^2} dt$$

is taken from tables of normal distribution functions or made available through a computer subroutine.

If desired, equation (34) can be integrated numerically over a chosen range of  $\theta$  to obtain the probability that the vector direction will lie within the chosen range; i.e.,

$$F(\theta) = \int_{\theta_2}^{\theta_1} g(\theta) d\theta \quad (35)$$

One application may be to obtain the probability that the wind will flow from a given quadrant or sector as, for example, onshore.

#### C.3.4. The Derived Conditional Distribution of Windspeed Given the Wind Direction (Wind Rose)

Continuing with the considerations in section C.3.3. of this chapter, the conditional probability density function (pdf) for windspeed,  $r$ , given a specified value for the wind direction,  $\theta$ , can be expressed as

$$f(r|\theta) = \frac{a^2 r e^{-\frac{1}{2}(a^2 r^2 - br)}}{1 + \sqrt{2\pi} \left(\frac{b}{a}\right) e^{\frac{1}{2}\left(\frac{b}{a}\right)^2} \phi\left\{\frac{b}{a}\right\}} \quad (36)$$

where the coefficients,  $a$  and  $b$  and the function  $\phi\left\{\frac{b}{a}\right\}$  are as previously defined in equation (33) and in equation (34).

From equation (36) the mode (most frequent value) of the conditional windspeed given a specified value of the wind direction is the positive solution of the quadratic equation,

$$a^2 r^2 - br - 1 = 0 \quad (37)$$

which is

$$(\ddot{r} | \theta) = \frac{1}{2a} \left[ \left( \frac{b}{a} \right) + \sqrt{4 + \left( \frac{b}{a} \right)^2} \right] \quad (38)$$

The locus of the conditional modal values of windspeed when plotted in polar form versus the given wind directions forms an ellipse.

The noncentral moment for equation (36) is expressed as

$$\mu'_n = \int_0^{\infty} r^n f(r|\theta) dr \quad (39)$$

Now the first noncentral moment is identical to the first central moment or the expected value,  $E(r|\theta)$ . The integration of equation (39) for the first moment is sufficiently simple to yield practical computations and can be expressed as

$$E(r|\theta) = \frac{\left( \frac{b}{a} \right) + \left[ 1 + \left( \frac{b}{a} \right)^2 \right] \sqrt{2\pi} e^{\frac{1}{2} \left( \frac{b}{a} \right)^2} \phi \left\{ \frac{b}{a} \right\}}{a \left[ 1 + \left( \frac{b}{a} \right) \sqrt{2\pi} e^{\frac{1}{2} \left( \frac{b}{a} \right)^2} \phi \left\{ \frac{b}{a} \right\} \right]} \quad (40)$$

Hence, equation (40) gives the conditional mean value of the windspeed given a specified value for the wind direction.

The integration of equation (36) for the limits  $r = 0$  to  $r = r^*$  gives the probability that the conditional windspeed is  $\leq r^*$  given a value for the wind direction,  $\theta$ . This conditional probability distribution (PDF) can be written as

$$\Pr \left\{ r \leq r^* \mid \theta = \theta_0 \right\} = 1 - \left[ \frac{e^{-\frac{1}{2} r_s^2 + \sqrt{2\pi} \left( \frac{b}{a} \right) \left\{ 1 - \phi(r_s) \right\}}}{e^{-\frac{1}{2} \left( \frac{b}{a} \right)^2 + \sqrt{2\pi} \left( \frac{b}{a} \right) \phi \left\{ \frac{b}{a} \right\}}} \right] \quad (41)$$

$$\text{where } r_s = \left[ a r^* - \left( \frac{b}{a} \right) \right]$$

By definition, equation (41) is an expression for a "wind rose." Empirical wind rose statistics are often tabulated or graphically illustrated giving the frequency that the windspeed is not exceeded for those windspeed values that lie within assigned class intervals of the wind direction. After evaluation of equation (41) for various values of windspeed,  $r^*$ , and the given wind directions,  $\theta$ , interpolations can be performed to obtain various percentile values of the conditional windspeed.

For the special case when  $b$  in equation (33) equals zero (i.e., for  $\bar{x} = \bar{y} = 0$ ), the conditional modal values of windspeeds [equation (38)], the conditional mean values of windspeeds [equation (40)], and the fixed conditional percentile values of windspeeds [interpolated from evaluations of equation (41)], when plotted in polar form versus the given wind directions, produce a family of ellipses.

For the special case when  $\bar{x} = \bar{y} = 0$ , equation (36) reduces to the following simple case:

$$\Pr \left\{ r \leq r^* \mid \theta = \theta_0 \right\} = 1 - e^{-\frac{a^2 r^{*2}}{2}} \quad (42)$$

There is a special significance of equation (42) when related to the bivariate normal probability distribution. If  $r^*$  and  $\theta$  are measured from the centroid of the probability ellipse, then the probability that  $r \leq r^*$  is the same as the given probability ellipse. Further, solving equation (42) for  $r^*$ , gives

$$r^* = \frac{1}{a} \sqrt{-2 \ln (1 - P)} \quad (43)$$

If a probability ellipse  $P$  is chosen, equation (42) gives the distance of  $r$  along any  $\theta$  from the centroid of the ellipse to the intercept of the specified probability ellipse. If there is an interest in conditional probability of winds for a given  $\theta$  relative to the monthly means, equation (43) is applicable. If it is desired to find the magnitude of the wind along any  $\theta$  relative to the monthly mean to the intercept of a given probability ellipse, equation (43) is applicable.

#### D. Statistical Parameters With Respect To Any Orthogonal Axes

The five wind statistical parameters presented in table I are given with respect to the standard meteorological coordinate system; i.e., these parameters are for the  $U$  and  $V$  components. For many aerospace vehicles and range applications, there is a need for wind statistics with respect to orthogonal axes other than west to east and south to north. For example, it may be required to present wind statistics with respect to a flight azimuth of an

aerospace vehicle whose flight azimuth is  $\alpha$  degrees from true north measured in a clockwise direction. The following sets of equations are presented to compute the five parameters for the new coordinate axes rotated  $\alpha$  degrees clockwise from true north.

a. Rotation of the means through  $\alpha$  degrees:

$$\bar{X}_{\alpha} = \bar{X} \cos (90 - \alpha) + \bar{Y} \sin (90 - \alpha) \quad (44)$$

$$\bar{Y}_{\alpha} = \bar{Y} \cos (90 - \alpha) - \bar{X} \sin (90 - \alpha) \quad (45)$$

b. Rotation of the variances through  $\alpha$  degrees:

$$\begin{aligned} \sigma_{x_{\alpha}}^2 &= \sigma_x^2 \cos^2 (90 - \alpha) + \sigma_y^2 \sin^2 (90 - \alpha) \\ &+ 2\rho\sigma_x\sigma_y \cos (90 - \alpha) \sin (90 - \alpha) \end{aligned} \quad (46)$$

$$\begin{aligned} \sigma_{y_{\alpha}}^2 &= \sigma_y^2 \cos^2 (90 - \alpha) + \sigma_x^2 \sin^2 (90 - \alpha) \\ &- 2\rho\sigma_x\sigma_y \cos (90 - \alpha) \sin (90 - \alpha) \end{aligned} \quad (47)$$

c. Rotation of the linear correlation coefficient through  $\alpha$  degrees:

$$\rho_{\alpha} = \frac{\text{cov} (X,Y)_{\alpha}}{\sigma_{x_{\alpha}} \sigma_{y_{\alpha}}} \quad (48)$$

where  $\text{cov} (X,Y)_{\alpha}$  is the rotated covariance,

$$\begin{aligned} \text{cov} (X,Y)_{\alpha} &= \text{cov} (X,Y) [\cos^2 (90 - \alpha) - \sin^2 (90 - \alpha)] \\ &+ \cos (90 - \alpha) \sin (90 - \alpha) (\sigma_y^2 - \sigma_x^2) \end{aligned}$$

and

$$\text{cov}(X,Y) = \rho \sigma_x \sigma_y$$

By using these rotational equations, the bivariate normal distribution with respect to any desired rotated coordinates can be obtained from sample estimates that have been computed with respect to a specific axis. The marginal distributions after rotation are also normally (univariate) distributed. Using the rotational equations greatly reduces computational efforts for applications requiring statistics with respect to several coordinate axes.

Appendix A presents some illustrative examples for the wind statistics of the specific RRA.



## CHAPTER III. STATISTICS OF THERMODYNAMICS QUANTITIES AND MODELS

### A. General Considerations

#### A.1. Objectives

The objective inherent in developing the thermodynamic section of the RRA was to describe the thermodynamic characteristics of the atmosphere using a minimum of data tabulations. A set of parameters was selected which, together, thermodynamically describe the climatological state of the atmosphere. These parameters are the pressure, temperature, density, dewpoint, virtual temperature, and water vapor pressure. Used together, these parameters permit the calculation of a large number of derived quantities. (Symbols used in the calculations in this chapter are summarized in table D.) Some of these quantities, such as the speed of sound, are dealt with in section III.E.

The probability distribution of each of the six thermodynamic RRA parameters is described by its mean value, its standard deviation, and its skewness. Several of these parameters (temperature, pressure, dewpoint and density) have probability distributions that are close to a univariate normal distribution; the others do not. The skewness parameter gives an estimate of the asymmetrical departures of a probability distribution.

Hydrostatically modeled mean values of pressure and density were calculated (table IV), so that users may determine the departure of the actual climatological values of these parameters from hydrostatic conditions. This was done by hydrostatically integrating the pressure from the lowest RRA data level to the termination altitude of the particular RRA.

#### A.2. Data Quality Control

Data limits derived from the following parameters were used to screen the thermodynamic portion of the RRA data base: temperature, pressure, dewpoint (for the 0- to 30-km portion only), and density (for the 30- to 70-km portion only). These limits were set to plus and minus six standard deviations from the mean values of each of these quantities. These limits were used to screen the thermodynamic portion of the RRA data base, according to the procedures described in section I.C. The data base used to generate the thermodynamic portion of the RRA (tables I, II, and IV) was considered to be free from errors under the following conditions:

- a) The skewness values of the pressure and temperature were between -2.5 and 2.5 at all data levels.
- b) The skewness values of the density were between -3.5 and 3.5 at data levels between 0 and 30 km.
- c) The skewness values of the density were between -3.0 and 3.0 at data levels between 30 and 70 km.
- d) The skewness values of the dewpoint were between -2.5 and 2.5 at all data levels with more than 10 data values.

TABLE D. LIST OF SYMBOLS USED IN CHAPTER III

$C_s$	- Speed of sound
$C_d$	- Collision diameter
$E$	- Vapor pressure
$g_\phi$	- Gravity at latitude $\phi$
$H$	- Geopotential height
$H_m$	- Geopotential height at a mandatory radiosonde data level
$H_s$	- Geopotential height at a significant radiosonde data level
$K_t$	- Coefficient of thermal conductivity
$L$	- Mean free path length
$M$	- Mean molecular weight of air at sea level
$M3Q$	- Annual or monthly third moment of quantity $Q$
$n$	- Refractive modulus
$N$	- Refractive index
$NA$	- Avogadro's constant
$N_Q$	- Number of values of quantity $Q$
$P$	- Pressure
$P_m$	- Pressure at a mandatory radiosonde data level
$P_s$	- Pressure at a significant radiosonde data level
$P_h$	- Hydrostatically integrated mean monthly or annual pressure
$Q$	- Any tabulated RRA quantity
$R^*$	- Universal gas constant
$R'$	- Specific gas constant of dry air
$r', r^*$	- Parameters used in converting $z$ to $h$ and vice versa

TABLE D. (concluded)

S	- Sutherland's constant, used in the calculation of dynamic viscosity
T	- Temperature
$T_d$	- Dew point
$T_v$	- Virtual temperature
$T_{vm}$	- Virtual temperature at a mandatory radiosonde data level
$T_{vs}$	- Virtual temperature at a significant radiosonde data level
V	- Mean air particle speed
$V_c$	- Mean collision frequency
w	- Parameter used in the hydrostatic interpolation of pressure and density
Z	- Geometric altitude
$\lambda$	- Wavelength
$\alpha_Q$	- Skewness of quantity Q
$\beta$	- Constant used in the equation for viscosity
$\gamma$	- Ratio of specific heat at constant pressure to specific heat at constant volume
$\eta$	- Kinematic coefficient of viscosity
$\mu$	- Dynamic coefficient of viscosity
$\rho$	- Density
$\rho_h$	- Mean monthly or annual density derived from pressure height
$\sigma$	- Standard deviation of the quantity Q

### A.3. Limitation of Thermodynamic Statistics

The correlation coefficients between the thermodynamic quantities and the moisture-related quantities were not calculated at discrete altitudes, nor were any of the correlations between altitudes. Therefore, valid statistical dispersion models that require the relationship between two or more of these quantities at the same altitude or between altitudes cannot be derived. Approximations for the correlation coefficients between pressure, virtual temperature, and density at discrete altitudes may be obtained from the coefficients of variation as developed by Buell (1970). The coefficient of variation is the standard deviation divided by the mean. The mean values and the standard deviations are taken from table II. A model for the profile of monthly and annual mean pressure, virtual temperature, and density that is in excellent agreement with the respective statistical mean values is given by table IV. This agreement results because the physical relationships, given by the hydrostatic equation and the equation of state, were used to derive table IV. When only the monthly or annual mean values for pressure, virtual temperature, and density are required, it is recommended that table IV be used.

### B. Establishing Data Samples at the Required Altitude Levels

This section describes the computational procedures used to establish data samples of the thermodynamic RRA parameters at the RRA data levels. References are cited only when an equation given is one of many available in the literature or when an equation is stated in an unusual form.

#### B.1. Conversion of Data Recorded in Geopotential Heights to Geometric Altitude

The upper air rocketsonde observations used to obtain the table values above 30 km were recorded in terms of geometric altitude and can be interpolated directly to the altitude intervals shown in the tables. However, the radiosonde observations used to obtain the tabular values below 30 km were recorded in terms of geopotential heights. The change of coordinates from geopotential heights to geometric altitudes ( $h$  to  $z$ ) is accomplished by calculating a table of geopotential heights that correspond exactly to the geometric altitudes at which the atmospheric parameters are tabulated. The radiosonde observations are then interpolated to these geopotential heights. The relationship used to calculate geometric altitude from geopotential height is

$$H = (r'z)/(r^*z) \quad , \quad (49)$$

where

$$r' = gr^*/9.80665$$

and

$$r^* = -2g_\phi / (\partial g_\phi / \partial z_0) \quad .$$

$g_\phi$  is the sea-level gravity at the latitude  $\phi$  corresponding to the proper location. This value is given by (List, 1968)

$$g_\phi = 9.780356 (1 + 5.2885 \times 10^{-3} \sin^2 \phi - 5.9 \times 10^{-6} \sin^2 (2\phi)). \quad (50)$$

$\frac{\partial g_\phi}{\partial z_0}$  is the rate of change of gravity at the sea level. This quantity is given

by the equation

$$\frac{\partial g_\phi}{\partial z_0} = -3.085462 \times 10^{-6} + 2.27 \times 10^{-9} \cos (2\phi) - 2 \times 10^{-12} \cos (4\phi). \quad (51)$$

The units used for gravity are meters per square second, while the units for

$\frac{\partial g_\phi}{\partial z_0}$  are per square second.

The resulting table of values of  $H$  obtained by using even increments of 2 in equation (49) is shown in table IV of the RRA. The values of  $H$  above 30 km are not used in the interpolation of original data, but are included for the convenience of the user.

## B.2. Calculations on the Original Rawinsonde Data Records

It was necessary to interpolate the information from the original rawinsonde data records to the geometric altitudes specified as the RRA data levels. The parameters for which this interpolation was required were the temperature, dewpoint, and pressure. The other parameters were calculated from the interpolated values at each RRA data level. These "derived" parameters were the water vapor pressure, density, and virtual temperature.

### B.2.1. Calculation of the Geopotential Height at Significant Levels

Two somewhat different interpolation procedures were used to obtain data from radiosonde and rocketsonde observations at the levels shown in the tables. The procedure used to interpolate radiosonde observations began with the calculation of virtual temperature at each data level in a sounding. The virtual temperature was computed by

$$T_v = T / (1 - 0.379 (e/p)) \quad , \quad (52)$$

where  $T_v$  and  $T$  are in degrees Kelvin and  $e$  and  $p$  are in millibars.

The radiosonde soundings contain a mix of data taken at "mandatory" and "significant" levels. Pressure, temperature, and dewpoint information was given in these soundings at both types of levels. However, geopotential height information was only given at the mandatory levels. The heights at the significant levels were "filled in" (calculated) hydrostatically using pressure and temperature data from these levels. This procedure permitted the use of most of the significant level data in the calculation of the RRA tables. The equation used for this process was

$$H_s = H_m + 29.2712617 \frac{(T_{vs} - T_{vm})}{2} \ln(P_s/P_m) , \quad (53)$$

where the subscripts s and m denote quantities at significant and mandatory levels. This equation was not used if the difference between two adjacent mandatory levels was greater than 200 mb. All soundings with such data gaps were rejected for use in compiling the RRA.

#### B.2.2. Temperature

Radiosonde temperatures were interpolated logarithmically with respect to pressure using the equation

$$T = T_U + (T_L - T_U) \frac{\ln p - \ln p_L}{\ln p_U - \ln p_L} , \quad (54)$$

where the subscripts U and L indicate values at the nearest data levels in the actual sounding above and below the interpolated level.

#### B.2.3. Pressure

The pressure values in each radiosonde sounding were interpolated to the RRA data levels using the equation

$$p = p_L \exp \left( \frac{H_L - H_U}{29.2712617 (0.5) (T_{vU} + T_{vL})} \right) \quad (55)$$

where the subscript L indicates virtual temperature, geopotential height, and pressure values at the data level below and closest to the level at which data were required.

#### B.2.4. Dewpoint Temperature

Dewpoint values were interpolated logarithmically with respect to pressure using the equation

$$T_d = T_{dU} + (T_{dL} - T_{dU}) \left( \frac{\ln p - \ln p_L}{\ln p_U - \ln p_L} \right) . \quad (56)$$

The subscripts U and L indicate data at the nearest upper and lower data levels in a sounding.

#### B.2.5. Derived Water Vapor Pressure

The water vapor pressure was calculated from the interpolated dewpoint values at the RRA data levels using Teten's approximation:

$$e = 6.11 \text{ mb} \times 10^{7.5(T_d - 273.15)/(T_d - 35.86)} \quad (57)$$

#### B.2.6. Derived Density

The density values derived from radiosonde observations were calculated at the RRA data levels using the equation

$$\rho = 348.36787 p/T_v \quad (58)$$

#### B.2.7. Derived Virtual Temperature

The virtual temperature values were calculated at the RRA data levels for each sounding using the equation

$$T_v = T/(1 - 0.379(e/p)) \quad (59)$$

where  $T_v$  and  $T$  are in degrees Kelvin, and  $p$  and  $e$  are the pressure and vapor pressure, respectively, in millibars.

### B.3. Calculations on the Original Rocketsonde Data Records

The rocketsonde data records used to calculate the RRA table values above 30 km were given in terms of geometric altitude. For this reason, slightly different calculations were required to convert the recorded data values to values at the RRA data levels. The pressure, temperature, and density were all interpolated to the RRA data levels; moisture-related parameters (virtual temperature, water vapor pressure, and dewpoint) were not calculated, since atmospheric moisture at altitudes above 30 km was considered to be negligible.

No interpolation was done across gaps in the pressure or temperature data within a sounding larger than 7,000 m. Data values at the RRA levels within such a gap were set to missing.

#### B.3.1. Temperature

Rocketsonde temperatures were interpolated linearly with respect to geometric altitude using the equation

$$T = T_U + (T_L - T_U) \frac{Z - Z_L}{Z_U - Z_L} , \quad (60)$$

where the subscripts U and L indicate values at the nearest data level in the actual sounding above and below the interpolated level.

### B.3.2. Pressure

The pressure values in each rocketsonde sounding were interpolated to the RRA data levels using the equation

$$P = P_L \exp \left( - \frac{g_\phi}{R^*} \frac{M(Z - Z_L)}{\bar{T}_v} \cdot W^2 \right) , \quad (61)$$

where  $\bar{T}_v = \frac{T_{vU} + T_{vL}}{2}$  and  $W = \left( \frac{r^*}{r^* + Z + \frac{Z - Z_L}{2}} \right)$ .

### B.3.3. Density

Rocketsonde density values were interpolated using the equation

$$\rho = \rho_L \exp \left( - \frac{g_\phi M}{R^*} \frac{(Z - Z_L)}{\bar{T}_v} \cdot W^2 \right) , \quad (62)$$

where W is specified in section III.B.3.2.

## C. Computation of Statistical Parameters for Tables II and III

A three-step procedure was used for computing the monthly and annual means, standard deviations, and skewness values from the data values at the RRA data levels. Initially, certain statistical sums were calculated and stored as the soundings in the data base were processed. These sums were then used to calculate the monthly statistics given in the RRA tables. The annual statistics were then calculated from these stored sums and the monthly statistics.

### C.1. Stored Statistical Sums

The sums calculated were



$$\sum Q, \sum Q^2, \text{ and } \sum Q^3 ,$$

where  $Q$  is any one of the quantities given in the thermodynamic part of the RRA.

## C.2. Calculation of the Monthly Statistics

### C.2.1. Monthly Means

The mean monthly values of the thermodynamic RRA quantities were calculated using the equation

$$\bar{Q} = \sum Q / N_Q ,$$

where  $N_Q$  is the number of observed values of the quantity  $Q$  for a given month.

### C.2.2. Monthly Standard Deviations

The monthly standard deviations of the thermodynamic RRA quantities were calculated using the equation

$$\sigma_Q = \sqrt{\frac{(N_Q \sum Q^2) - (\sum Q)^2}{N_Q \cdot (N_Q - 1)}} . \quad (63)$$

### C.2.3. Monthly Skewness Values

The monthly skewness values of the windspeed and of the thermodynamic RRA quantities were calculated using the equation

$$\alpha_Q = \frac{M_{3Q}}{\sigma_Q^3} ,$$

where  $M_{3Q}$  is the third moment of the quantity  $Q$ ,  $\sigma_Q$  is its standard deviation, and

$$M_{3Q} = \left[ \frac{\sum Q^3}{N_Q} - \frac{3 \sum Q \sum Q^2}{N_Q^2} - \frac{2 \sum Q^3}{N_Q^3} \right] \cdot \frac{N_Q^2}{(N_Q - 1)(N_Q - 2)} . \quad (64)$$

### C.3. Calculation of the Annual Statistics

Equations (63) and (64), used to calculate the monthly values of the standard deviations and skewness values, involve taking the differences between two pairs of large sums containing  $Q^2$  and  $Q^3$ , where  $Q$  is any thermodynamic RRA quantity. Using these equations to compute the annual statistics would have resulted in a substantial loss of precision, as these sums become larger by several orders of magnitude in such a case. This problem was avoided by calculating the annual means, standard deviations, and skewness values from the monthly statistics.

#### C.3.1 Annual Mean Values

The annual mean values of the thermodynamic RRA quantities were calculated using the equation

$$Q_{ANN} = Q_A / N_Q$$

where  $Q_A$  is the total of all observed values of  $Q$  and  $N_Q$  is the total number of observations of  $Q$ .

#### C.3.2. Annual Standard Deviations

The annual standard deviations of the thermodynamic RRA quantities were calculated using the equation

$$\sigma_{Q_{ANN}} = \sqrt{\frac{1}{N_Q} \sum_{i=1}^{12} (N_{Qi} \sigma_{Qi}^2) + \frac{1}{N_Q} \sum_{i=1}^{12} (N_{Qi} \bar{Q}_i^2) - Q_{ANN}^2} \quad (65)$$

where  $N_{Qi}$  = the number of data values for  $Q$  in month  $i$  ( $i = 1$  to  $12$ ),  $Q_i$  = the monthly mean of  $Q$ , and  $\sigma_{Qi}$  = the standard deviation of quantity  $Q$  in month  $i$ .

#### C.3.3. Annual Skewness Values

The annual skewness values of the thermodynamic RRA quantities were calculated using the equation

$$\begin{aligned}
M3Q_{ANN} = & \frac{1}{N} \sum_{i=1}^{12} (N_{Qi} M_{3Qi}) + \frac{3}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} \bar{Q}_i Q_i^2) \\
& + \frac{1}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} Q_i^3) - \frac{3\bar{Q}_{ANN}}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} Q_i^2) \\
& - \frac{3\bar{Q}_{ANN}}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} Q_i^2) + 2\bar{Q}_{ANN}^3, \quad (66)
\end{aligned}$$

where  $M_{3Qi}$  = the third moment about the mean of quantity  $Q$  in month  $i$  and  $M3Q_{ANN}$  = the annual third moment about the mean of the quantity  $Q$ .

#### D. Derived Monthly Mean and Annual Mean Model Atmospheres

A set of modeled monthly mean and annual mean hydrostatic values of pressure and density was calculated from the lowest RRA data level (0 km, mean sea level) upwards to 30 km, and from 30 km upwards to 70 km. The integration from 0 to 30 km was computed independently of the integration from 30 to 70 km because of the difference in data sources. The two different values for 30 km are provided for comparison. When 30-km data are required, the values given in the 0- to 30-km table should be used. These hydrostatically modeled mean values, which are given in table IV, are useful as a check on the validity of the pressure and density values given in table II. In most cases, the values in tables II and IV for any given data level are within 1 percent of each other. The hydrostatic pressure values in table IV were calculated using the equation

$$p_1 = p_0 \exp \left( - \frac{0.034162 (H_1 - H_0)}{0.5 (T_{v1} + T_{v0})} \right), \quad (67)$$

where  $H_1 - H_0$  is in meters and a "0" subscript refers to values at the RRA data level immediately below the level being checked.  $p_0$  at the lowest data level is set equal to the RRA mean pressure;  $p_1$ , calculated for the next highest data level, is taken as  $p_0$  for the level above that. This process is repeated for all the other RRA data levels. The hydrostatic density corresponding to the hydrostatic pressures is calculated from these pressures and the RRA virtual temperature values using the formula

$$\rho_H = 348.36786 P_H / T_v, \quad (68)$$

where  $\rho_H$  and  $P_H$  are the hydrostatic density and pressure shown in table IV of the RRA.

#### E. Thermodynamic Quantities Derivable from the Basic Tables

Several other quantities can be calculated from the statistics listed in tables I and II. Primary physical constants used in these calculations are listed in table E. The equations given in this section can be used to calculate the approximate mean values of these quantities at each RRA data level. It is not possible to infer or derive any information concerning the standard deviation or skewness values of these quantities from the data in tables II and III of the RRA.

##### E.1. Mean Air Particle Speed

The mean air particle speed,  $V$ , is the arithmetic average of the speeds of all air particles in the volume element being considered. For a valid average to occur, there must be a sufficient number of particles involved to represent mean conditions. The equation for  $V$  for dry air is

$$V = \sqrt{\frac{8}{\pi} \cdot \frac{R \cdot T}{M}} \quad (69)$$

A computational form for dry air, using tabulated values, is

$$V = \sqrt{7.3094 \times 10^2 \times T} \text{ (meters per second)} \quad (70)$$

where  $T$  is the temperature in degrees Kelvin from table II. Equation (69), when corrected for moist air, becomes

$$V = \sqrt{\frac{8}{\pi} \cdot R' \cdot T_v} \quad (71)$$

The computational form for moist air is

$$V = \sqrt{7.3094 \cdot 10^2 \cdot T_v} \text{ (meters per second)} \quad (72)$$

where  $T_v$  is the virtual temperature in degrees Kelvin from table III.

TABLE E. LIST OF PRIMARY PHYSICAL CONSTANTS

$P_o$	= standard atmospheric pressure at sea level = $1.013250 \times 10^5$ Newton/m <sup>2</sup> = 2116.22 lb/ft <sup>2</sup>
$\rho_o$	= standard atmospheric density at sea level = 1.2250 kg/m <sup>3</sup> = 0.076474 lb/ft <sup>3</sup>
$T_o$	= standard temperature at sea level = 288.15 K = 15.0°C = 59.0°F
$g_o$	= standard gravity at sea level at latitude 45°32'33" = 9.80665 m/s <sup>2</sup>
$S$	= Sutherland's constant used in calculation of dynamic viscosity = 110.4 K
$T_i$	= ice-point temperature at $P_o$ = 273.15 K
$\mu$	= constant used in calculation of dynamic viscosity = $1.458 \times 10^{-6}$ kg/s m K <sup>1/2</sup> = $7.3025 \times 10^{-7}$ lb/s ft R <sup>1/2</sup>
$\gamma$	= ratio of specific heat of air at constant pressure to specific heat of air at constant volume = 1.4
$C_D$	= mean effective collision diameter of air molecules = $3.65 \times 10^{-10}$ m = $1.1975 \times 10^{-9}$ ft
$N_a$	= Avogadro's constant = $6.022169 \times 10^{26}$ /kg mol = $2.73179 \times 10^{26}$ /lb mol
$R^*$	= gas constant = 8.31432 J/mol K
$R'$	= gas constant for dry air = $2.8704 \times 10^2$ J/kg K
$M$	= molecular weight of dry air = 28.966 g/mol

### E.2. Mean Free Path

The mean free path,  $L$ , is the mean value of the distance traveled by each neutral air particle in a selected air parcel, between successive collisions with other particles in that parcel. A meaningful average requires that the selected parcel be large enough to contain a substantial number of particles. The equation for  $L$  is given by

$$L = \left( \frac{\sqrt{2}}{2\pi} \right) \left( \frac{R^*T}{N_a C_d^2 P} \right) \quad , \quad (73)$$

where  $C_d$  is the effective collision diameter of the mean air molecules. The 1976 standard atmosphere value of  $3.65 \times 10^{-10}$  is valid for the range of altitudes in the RRA.

A computational form for moist air, using tabulated values, is

$$L = 2.335 \times 10^{-7} \frac{T}{P} \text{ (meters)} \quad , \quad (74)$$

where  $T$  is the temperature in degrees Kelvin from table II and  $P$  is the pressure in millibars from table II.

A form of (73) to correct  $L$  for moist air is

$$L = \left( \frac{\sqrt{2}}{2\pi} \right) \frac{R^*MT_v}{N_a C_d^2} \quad . \quad (75)$$

The computational form for moist air is

$$L = 2.3325 \times 10^{-7} \frac{T_v}{P} \text{ (meters)} \quad , \quad (76)$$

where  $T_v$  is the virtual temperature in degrees Kelvin from table III and  $P$  is the pressure in millibars from table II.

### E.3. Mean Collision Frequency

The mean collision frequency,  $V_c$ , is considered to be the average speed of air particles contained in an air parcel, divided by the mean free path of the particles inside that parcel. Computationally this is equivalent to

$$V_c = \frac{V}{L} \text{ (sec}^{-1}\text{)} \quad (77)$$

To determine  $V_c$  for dry air, use  $V$  and  $L$  from equations (70) and (74). To determine  $V_c$  for moist air, use  $V$  and  $L$  from equations (72) and (76).

#### E.4. Speed of Sound

The expression for the speed of sound,  $C_s$ , in meters per second in dry air, is

$$C_s = \sqrt{\frac{R \cdot T}{M}} \quad (78)$$

To compute  $C_s$  for dry air from tabulated values, use

$$C_s = \sqrt{4.0185 \cdot 10^2 \cdot T} \text{ (meters per second)} \quad (79)$$

where  $T$  is the temperature in degrees Kelvin from table II. One form for the speed of sound in moist air is

$$C_s = \sqrt{R \cdot T_v} \quad (80)$$

where  $T_v$  is the virtual temperature from table III. A computational form for moist air is

$$C_s = \sqrt{4.0185 \times 10^2 T_v} \text{ (meters per second)} \quad (81)$$

#### E.5. Dynamic Coefficient of Viscosity

The coefficient of dynamic viscosity,  $\mu$ , is defined as a coefficient of internal friction developed where gas regions move adjacent to each other at different velocities. The following expression is taken from the U.S. Standard Atmosphere (1976):

$$\mu = \frac{B \cdot T^{3/2}}{T + S} \quad (82)$$

The computational form is

$$\mu = \frac{(1.458 \cdot 10^{-6}) T^{3/2}}{T + 110.4} \quad \left( \begin{array}{l} \text{kilograms per second} \\ \text{per meter} \end{array} \right), \quad (83)$$

where T is the temperature in degrees Kelvin from table II.

#### E.6. Kinematic Coefficient of Viscosity

The kinematic coefficient of viscosity, designated as  $\eta$ , is defined to be the ratio of the dynamic coefficient of viscosity of a gas to its density, or

$$\eta = \mu / \rho \quad (84)$$

The computational form is

$$\eta = 1.0 \cdot 10^3 \mu / \rho \quad \left( \begin{array}{l} \text{square meters} \\ \text{per second} \end{array} \right), \quad (85)$$

where  $\mu$  is the dynamic coefficient of viscosity from equation (83) and  $\rho$  is the density in grams per cubic meter from table II.

#### E.7. Coefficient of Thermal Conductivity

The empirical expression used for the coefficient of thermal conductivity, designated as  $K_t$ , is given in the 1976 Standard Atmosphere as

$$K_t = \frac{2.65019 \times 10^{-3} \cdot T^{3/2}}{T + 245.4 \times 10^{-(12/T)}} \quad \left( \begin{array}{l} \text{watts per meter} \\ \text{per degree Kelvin} \end{array} \right), \quad (86)$$

where T is in degrees Kelvin.

#### E.8. Refractive Modulus and Refractive Index

The refractive modulus or refractivity (Selby and McClatchey, 1975; Smith and Weintraub, 1953) is defined as N, where

$$N = (n - 1) \cdot 10^6 \quad (87)$$

and n is the refractive index.



For microwave frequencies below approximately 30 GHz (equivalent to wavelengths above 1 cm),  $N$ , the refractive modulus, is given by the empirical equation

$$N = 77.6 \frac{P}{T_d} + 3.73 \times 10^5 \frac{e}{T^2} \quad (\text{dimensionless}), \quad (88)$$

where  $E$  and  $P$  are in millibars and  $T$  and  $T_d$  are in degrees Kelvin.

The following expression is valid for the visible and infrared wavelengths shorter than approximately 30  $\mu\text{m}$  (0.03 mm).

$$N = 77.6 \frac{P}{T} + 0.584 \frac{P}{T\lambda} \quad (\text{dimensionless}), \quad (89)$$

where  $\lambda$  is the wavelength in microns and  $T$  is in degrees Kelvin.

The expression for  $N$  for the wavelength from 0.03 mm to 1 cm is an extremely complex function of wavelength.

## CHAPTER IV. CONCLUSIONS AND RECOMMENDATIONS

### Conclusions

This document satisfies the technical objectives established for the RRAC by the RCC MG. Upper air statistics and models for wind and thermodynamic quantities for the specific site have been derived in a consistent and uniform manner, which will be used in publications for all other assigned site locations. These RRAs represent an improvement over the previously published RRAs because of the availability of more extensive upper air data bases and the adaptation of more advanced statistical techniques. A statistical measure of central tendency (mean values) and a measure of dispersion (standard deviation with respect to the mean values) for monthly and annual reference periods have been tabulated for all variables in a consistent manner from data bases that have been edited and quality-controlled in the same manner. Further, a statistical measure for symmetry (skewness coefficient that involves the third statistical moment) has been tabulated for all variables except the U and V wind components. Even with these improvements, the user of these RRAs must recognize certain limitations of the statistical tabulations:

1) The wind profile structure with respect to altitude cannot be modeled from the RRA statistics because the interlevel and crosslevel correlations were not computed.

2) The profile structure with respect to altitude for any of the thermodynamic variables or any quantities derivable from these variables cannot be modeled because the prerequisite correlations were not computed. However, the profiles of monthly and annual means for pressure, virtual temperature, and density are in agreement (table IV) with the hydrostatic equation and the equation of state.

The preceding limitations are cited to prevent a misuse of the RRAs. More extensive statistical tabulations were beyond the scope of this committee's task. As greater insight is gained through usage of these RRAs, many adaptations of the statistical tabulations for specific engineering and scientific applications are envisioned.

### Recommendations

It is recommended that the wind and thermodynamic statistical tabulations and attendant models contained in the RRAs be used as a standard reference source, as may be appropriate, by the ranges and range users. It is further recommended that the respective Range Staff Meteorologist or responsible agency staff member be consulted for the applicability of the RRAs for specific engineering applications.

## REFERENCES

- Buell, Eugene C.: "Statistical Relations in a Perfect Gas." Journal of Applied Meteorology, 9, 1970, pp. 729-731.
- List, R. J., Editor: Acceleration of Gravity, Smithsonian Meteorological Tables, Sixth Ed. Smithsonian Institution, Washington, D.C., 1968, pp. 488.
- Selby, J.E.A.; and McClatchey, R.A.: AFCRL-TR-75-0255, Atmospheric Transmittance from 0.25 to 28.5  $\mu$ m - Computer Code Lowtran 3, Air Force Cambridge Research Laboratories. Available through the National Technical Information Service, Washington, D.C., 1975.
- Smith, E.K.; and Weintraub, S.: "The Constants in the Equation for Atmospheric Refractive Index at Radio Frequencies," Proceedings of the Institute of Radio Engineers, 41, 8, August 1953, pp. 1035-1037.
- Smith, O.E.: NASA TM X-73319, Vector Wind and Vector Wind Shear Models at 0-27 km Altitude for Cape Kennedy, Florida, and Vandenberg AFB, California. Prepared under sponsorship of the National Aeronautics and Space Administration. Available through the National Technical Information Service, Washington, D.C., July 1976.
- U.S. Standard Atmosphere, 1976. Prepared under the sponsorship of the National Aeronautics and Space Administration, United States Air Force, and United States Weather Bureau. Available through U.S. Government Printing Office, Washington, D.C., October 1976.

## PREVIOUS RANGE REFERENCE ATMOSPHERES PUBLISHED BY IRIG

- Atlantic Missile Range Reference Atmosphere for Cape Kennedy, Florida (Part I), Document 104-63, April 16, 1963. (AD451780)
- White Sands Missile Range Reference Atmosphere (Part I), Document 104-63, June 28, 1964. (AD451781)
- Fort Churchill Missile Range Reference Atmosphere for Fort Churchill, Manitoba, Canada (Part I), Document 104-63, August 7, 1964. (AD634727)
- Pacific Missile Range Reference Atmosphere for Eniwetok, Marshall Islands (Part I), Document 104-63, September 1, 1964. (AD479264)
- Fort Greely Missile Range Reference Atmosphere (Part I), Document 104-63, October 6, 1964. (AD634726)
- Eglin Gulf Test Range Atmosphere for Eglin AFB, Florida (Part I), Document 104-63, January 25, 1965. (AD472601)
- Pacific Missile Range Atmosphere for Point Arguello, California (Part I), Document 104-63, April 1965. (AD472602)

Wallops Island Test Range Reference Atmosphere (Part I), Document 104-63, July 10, 1965. (AD474071)

Eastern Test Range Reference Atmosphere for Ascension Island, South Atlantic (Part I), Document 104-63, July 1966. (AD645591)

Johnston Island Test Site Reference Atmosphere (Part I), Document 104-63, January 1970. (AD782652)

Lihue, Kauai, Hawaii Reference Atmosphere (Part I), Document 104-63, January 1970. (AD782653)

Cape Kennedy, Florida Reference Atmosphere (Part II), Document 104-63, September 1971. (AD751581)

White Sands Missile Range Reference Atmosphere (Part II), Document 104-63, September 1971. (AD782654)

Wallops Island Test Range Reference Atmosphere (Part II), Document 104-63, September 1971. (ADA040280)

Fort Greely Missile Range Reference Atmosphere (Part II), Document 104-63, September 1971. (ADA040281)

Edwards Air Force Base Reference Atmosphere (Part I), Document 104-63, September 1972. (AD782651)

Kwajalein Missile Range Reference Atmosphere for Kwajalein, Marshall Islands (Part I), Document 104-63, October 1974. (ADA002664)

Pacific Missile Test Center Reference Atmosphere for Point Arguello, California (Part II), Document 104-63, November 1975. (ADA040279)

#### REVISED RANGE REFERENCE ATMOSPHERES PUBLISHED BY THE RCC

Kwajalein Missile Range, Kwajalein, Marshall Islands, Range Reference Atmosphere, 0-70 Km Altitude, Document 360-82, December 1982. (AD123424)

Cape Canaveral, Florida, Range Reference Atmosphere, 0-70 Km Altitude, Document 361-83, February 1983. (ADA125553)

Vandenberg Air Force Base, California, Range Reference Atmosphere, 0-70 Km Altitude, Document 362-83, April 1983.

Dugway, Utah, Range Reference Atmosphere, 0-30 Km Altitude, Document 363-83, June 1983.

Wallops Island, Virginia, Range Reference Atmosphere, 0-70 Km Altitude, Document 364-83, July 1983.

White Sands Missile Range, New Mexico, Range Reference Atmosphere, 0-70 Km Altitude, Document 365-83, August 1983.

Edwards AFB, California, Range Reference Atmosphere, 0-70 Km Altitude, Document 366-83, August 1983.

Eglin AFB, Florida, Range Reference Atmosphere, 0-30 Km Altitude, Document 367-83, September 1983.

Taquac, Guam Island, Range Reference Atmosphere, 0-30 Km Altitude, Document 368-83, September 1983.

Point Mugu, California, Range Reference Atmosphere, 0-70 Km Altitude, Document 369-83, September 1983.

Barking Sands, Hawaii, Range Reference Atmosphere, 0-70 Km Altitude, Document 370-83, December 1983.

Ascension Island, South Atlantic, Range Reference Atmosphere, 0-66 Km Altitude, Document 371-84, January 1984.

## CONVERSION UNITS

### Physical Constants and Conversion Factors

Numerical values in this document are given in the International System of Units (SI, *Système International d'Unités*). The values in parentheses are equivalent U.S. Customary Units, which are English units adapted for use by the United States of America. The SI and U.S. Customary Units provided in table F are those normally used for measuring and reporting atmospheric data.

By definition, the following fundamental conversion factors are exact:

<u>Type</u>	<u>U.S. Customary Units</u>	<u>Metric</u>
Length	1 U.S. yard (yd)	0.9144 meter (m)
Mass	1 avoirdupois pound (lb)	453.59237 gram (g)
Time	1 second (s)	1 second (s)
Temperature	1 degree Rankine (°R)	9/5 degree Kelvin (K)

To aid in the conversion of units, conversion factors based on the above fundamental conversion factors are given in table F.

TABLE F. FACTORS FOR CONVERSION UNITS

Type of Data	M. I. F. R. I. C.		U. S. C. U. S. T. O. M. A. R. Y.				C. O. N. V. E. R. S. I. O. N.	
	Unit	Abbreviation	Unit	Abbreviation	Multiply	By	To Get	
TEMPERATURE Ambient Temperature	degree Celsius	°C	degree Fahrenheit	°F	°F - 32	0.5556	°C	
	degree Kelvin	K	degree Rankine	°R	°C	1.8°	°F - 32	
					°R - 459.67	1.00°	°F + 459.67	
					K	1.00°	°F	
					K - 273.15	1.00°	°C + 273.15	
Temperature Change	degree Celsius	°C	degree Fahrenheit	°F	°C or K	1.8°	temp. change °F or °R	
	degree Kelvin	K	degree Rankine	°R	°F or °R	0.5556	temp. change °C or K	
DENSITY Water Vapor Vapor Concentration (Absolute Humidity) and Ambient Density	gram per cubic meter	g m <sup>-3</sup>	gram per cubic foot	gr ft <sup>-3</sup>	g m <sup>-3</sup>	0.43700	gr ft <sup>-3</sup>	
	gram per cubic centimeter	g cm <sup>-3</sup>			gr ft <sup>-3</sup>	2.2883	g m <sup>-3</sup>	
					g cm <sup>-3</sup>	10 <sup>-6</sup>	g cm <sup>-3</sup>	
					g cm <sup>-3</sup>	4.370 x 10 <sup>-5</sup>	gr ft <sup>-3</sup>	
					gr ft <sup>-3</sup>	2.288 x 10 <sup>-6</sup>	g cm <sup>-3</sup>	
WIND Wind Speed	meter per second	m s <sup>-1</sup>	mile per hour	mph	m s <sup>-1</sup>	2.2369	mph	
			knots	knots	mph	0.44704°	m s <sup>-1</sup>	
			feet per second	ft s <sup>-1</sup>	m s <sup>-1</sup>	1.9438	knots	
					knots	0.51444	m s <sup>-1</sup>	
					mph	0.868976	knots	
					knots	1.15078	mph	
					m s <sup>-1</sup>	3.2808	ft s <sup>-1</sup>	
DISTANCE Length	meter	m	feet	ft	ft s <sup>-1</sup>	0.3048°	m s <sup>-1</sup>	
	micron	μ	inch	in.	m	3.2808	ft	
	Angstrom unit	Å			in.	0.3048°	m	
					in.	2.54 x 10 <sup>-4</sup>	Å	
					m	2.54 x 10 <sup>-8</sup>	Å	
					m	10 <sup>-6</sup>	Å	
					m	10 <sup>-10</sup>	Å	

° Defined exact conversion factor

TABLE F. (continued)

Type of Data	METRIC		U. S. CUSTOMARY			CONVERSION	
	Unit	Abbreviation	Unit	Abbreviation	Multiply	By	To Get
DISTANCE (Continued)					$\mu$	$10^{-6}$	m
					$\mu$	$3.937 \times 10^{-5}$	in.
					$\text{\AA}$	$10^{-10}$	m
					$\text{\AA}$	$3.937 \times 10^{-9}$	in.
MASS Weight	gram	g	gram	gr	lb	0.45359237*	kg
	kilogram	kg	pound	lb	lb	453.59237*	g
					kg	2.20462	lb
					F	15.4324	gf
					gr	0.06480	g
PRESSURE Atmospheric	newton per square meter	newton $\text{m}^{-2}$	pound force per square inch	lb $\text{in}^{-2}$	mb	$10^{-3}$	bar
	millimeter of Mercury	mmHg	inch of Mercury	in Hg	bar	$10^{-3}$	mb
	bar	bar			newton $\text{m}^{-2}$	$10^{-2}$	mb
	millibar	mb			newton $\text{m}^{-2}$	$1.4504 \times 10^{-4}$	lb $\text{in}^{-2}$
	dyne per square centimeter (microbar)	dyne $\text{cm}^{-2}$			lb $\text{in}^{-2}$	$6.8948 \times 10^{-3}$	newton $\text{m}^{-2}$
	kilogram force per square meter	kg $\text{m}^{-2}$			mb	$1.4504 \times 10^{-2}$	lb $\text{in}^{-2}$
					lb $\text{in}^{-2}$	68.948	mb
					mb	$10^{-3}$	dyne $\text{cm}^{-2}$
					dyne $\text{cm}^{-2}$	$10^{-3}$	mb
					lb $\text{in}^{-2}$	$6.8948 \times 10^{-4}$	dyne $\text{cm}^{-2}$
					dyne $\text{cm}^{-2}$	$1.4504 \times 10^{-5}$	lb $\text{in}^{-2}$
					mb	10.1972	kg $\text{m}^{-2}$
					kg $\text{m}^{-2}$	0.0980665	mb
					lb $\text{in}^{-2}$	703.0696	kg $\text{m}^{-2}$
					kg $\text{m}^{-2}$	0.0014223	lb $\text{in}^{-2}$
					mb	$2.9530 \times 10^{-2}$	in. Hg (32°F)
					mb	0.75006	mmHg (0°C)
					in. Hg (32°F)	25.40*	mmHg (0°C)
					mmHg (0°C)	1.33322	mb
					in. Hg (32°F)	33.8639	mb
		pascal	Pa			Pa	1.00*

\* Defined exact conversion factor



TABLE I-1. WIND STATISTICAL PARAMETERS

## JANUARY

STATION = 619020									
ASCENSION (WIDE AWAKE)									
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS	NOBS
KM	M/S	M/S		M/S	M/S	M/S	M/S		
.020	-6.30	1.80	.0000	3.97	1.03	7.67	1.64	.15	508.
1.000	-3.59	2.09	-.3459	1.55	2.08	4.69	2.50	.40	503.
2.000	-3.17	3.72	-.2001	.12	2.68	4.03	2.00	.93	509.
3.000	-4.31	3.51	-.1906	-.08	2.38	5.05	2.93	.49	505.
4.000	-4.63	3.39	-.1453	-.05	2.89	6.07	2.97	.49	510.
5.000	-5.14	3.65	-.1209	-.70	3.05	6.34	3.05	.31	503.
6.000	-5.80	3.27	-.0833	-.64	3.31	7.10	3.21	.16	509.
7.000	-5.62	4.75	-.0441	-.05	3.53	7.54	3.31	.11	503.
8.000	-4.06	6.52	.0000	-1.11	3.80	7.78	3.75	.71	509.
9.000	-1.81	2.03	.0173	-1.57	4.31	6.23	4.09	1.00	510.
10.000	.40	9.02	.0155	-2.28	4.90	6.66	5.70	1.26	503.
11.000	2.54	9.99	.0606	-2.94	5.42	9.95	6.71	1.27	507.
12.000	5.08	10.01	.0535	-3.70	5.33	11.05	7.65	1.14	507.
13.000	7.60	12.07	.0270	-3.72	5.65	13.11	8.95	1.07	507.
14.000	9.69	13.39	.0445	-2.52	5.78	14.29	9.64	.33	507.
15.000	6.49	12.17	.1773	-1.51	5.53	12.40	8.31	1.00	505.
16.000	1.18	8.33	.0032	-1.41	4.43	9.74	5.12	.99	506.
17.000	-3.57	5.77	-.1301	-1.21	3.70	6.97	3.55	.47	503.
18.000	-6.15	4.34	-.0473	-.44	3.31	7.54	4.03	.60	459.
19.000	-3.33	5.04	.0010	-.32	2.63	7.04	4.00	.74	454.
20.000	-7.03	8.19	-.1074	.02	2.48	9.30	6.97	.60	493.
21.000	-10.45	10.77	-.1477	.75	2.71	11.90	9.56	.59	483.
22.000	-13.81	12.03	-.1080	1.61	3.23	15.07	11.01	.47	481.
23.000	-15.00	10.05	-.0040	1.30	2.70	16.30	10.48	.35	473.
24.000	-17.21	10.00	.0701	.02	3.22	17.05	10.03	.30	460.
25.000	-17.04	10.09	.0431	-.09	3.13	18.25	9.70	.41	454.
26.000	-18.35	10.03	-.0074	-1.01	2.30	18.87	10.11	.44	441.
27.000	-19.97	12.16	-.0313	-1.73	3.03	20.31	11.42	.31	414.
28.000	-21.27	13.10	-.0515	-1.30	3.21	21.97	12.38	.20	402.
29.000	-23.52	13.89	.0192	-1.06	3.11	24.13	13.21	-.04	326.
30.000	-25.08	13.84	.1181	-.84	3.27	25.62	13.76	-.16	303.
32.000	-22.15	13.14	.0806	-.37	3.86	20.77	12.64	.01	81.
34.000	-26.55	12.93	-.2145	.09	3.06	26.65	12.74	-.02	81.
35.000	-30.24	11.10	-.1430	1.50	4.40	30.63	11.03	.12	81.
38.000	-34.53	10.44	.0349	1.07	4.59	34.63	10.43	.20	51.
40.000	-42.88	9.83	.0401	.68	4.93	42.15	9.90	.58	81.
42.000	-52.23	8.55	.0455	-1.18	5.83	52.60	6.48	.01	81.
44.000	-61.49	9.05	-.0411	-3.23	7.60	62.05	8.95	-.18	81.
46.000	-67.94	13.29	-.0465	-5.30	8.15	68.63	13.31	-.18	80.
48.000	-71.46	17.99	-.0510	-6.27	7.28	72.14	17.62	-.32	79.
50.000	-63.61	22.97	-.0070	-6.68	9.11	64.73	22.01	-.33	77.
52.000	-45.86	24.16	.0218	-7.25	10.12	40.23	22.55	.12	76.
54.000	-20.20	20.95	-.0300	-4.33	14.06	33.02	17.32	.77	74.
56.000	-14.85	17.15	.1379	-1.13	15.17	24.41	12.04	.75	70.
58.000	-1.54	16.54	-.1300	1.43	15.57	20.14	10.40	.38	59.
60.000	4.24	17.46	-.2739	3.03	14.29	20.46	10.49	1.00	50.
62.000	6.44	17.37	-.0195	2.29	17.37	22.49	11.56	1.22	43.
64.000	11.77	16.85	-.0045	4.73	18.56	25.41	11.16	.28	27.
65.000	20.23	19.51	-.0590	9.01	22.72	29.43	19.84	.47	7.

TABLE I-2. WIND STATISTICAL PARAMETERS

## FEBRUARY

STATION - 619020		ASCENSION (WIDE AWAKE)								NOBS
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKCH WS		
M/S	M/S	M/S		M/S	M/S	M/S	M/S			
0.000	-6.37	1.66	.0559	3.78	1.75	7.62	1.81	-.13	461.	
1.000	-4.33	2.59	-.3709	2.53	2.16	5.49	2.54	.23	461.	
2.000	-2.73	3.31	-.2459	.26	2.81	4.61	2.26	.60	459.	
3.000	-3.55	3.51	-.2328	-.92	2.67	5.26	2.52	.30	459.	
4.000	-3.48	3.57	-.1671	-1.15	3.03	5.43	2.42	.33	459.	
5.000	-4.29	3.58	-.1251	-.60	2.86	5.70	2.69	.27	459.	
6.000	-5.42	3.82	-.1763	-.38	3.20	6.77	2.93	.37	459.	
7.000	-5.93	4.52	-.1227	-.69	3.53	7.63	3.10	.22	459.	
8.000	-5.27	5.47	-.1003	-1.32	3.70	7.88	3.32	.36	459.	
9.000	-4.05	5.49	-.2190	-1.89	4.20	8.01	3.94	.59	459.	
10.000	-2.47	7.31	-.1470	-2.52	4.87	8.39	4.37	.62	459.	
11.000	-.68	8.67	-.0500	-3.36	5.61	9.55	5.18	1.19	459.	
12.000	1.39	9.50	-.0129	-3.42	5.53	9.94	5.95	1.08	454.	
13.000	3.00	10.57	-.0112	-3.29	5.78	10.71	7.08	1.33	454.	
14.000	2.90	11.18	-.0534	-2.01	5.88	11.01	7.39	1.31	456.	
15.000	.31	10.03	-.1378	-2.30	5.13	9.75	6.10	1.39	455.	
16.000	-2.50	7.30	-.1001	-1.75	4.13	7.76	4.40	.87	457.	
17.000	-4.70	5.23	-.1521	-.74	3.53	7.11	3.52	.57	456.	
18.000	-6.17	5.11	-.0297	.02	3.31	7.52	4.13	.61	456.	
19.000	-6.84	5.06	-.0257	-.17	2.61	8.05	4.04	.67	444.	
20.000	-8.57	8.09	-.1676	.09	2.78	9.02	7.08	.64	433.	
21.000	-10.73	10.62	-.1504	.21	3.07	12.10	9.59	.61	475.	
22.000	-13.55	11.06	.0152	1.49	3.21	14.63	10.00	.55	424.	
23.000	-15.23	10.16	.2205	1.33	2.77	15.79	9.06	.53	411.	
24.000	-16.64	9.92	.1202	1.08	3.47	17.42	9.59	.52	401.	
25.000	-17.00	10.18	-.0331	-.44	3.18	18.28	9.83	.77	393.	
26.000	-19.04	11.28	-.0537	-1.23	2.94	19.49	10.03	.59	373.	
27.000	-20.22	12.71	-.0679	-1.04	3.07	20.90	12.09	.29	352.	
28.000	-22.02	13.74	-.0088	-1.89	3.01	22.70	13.08	.13	332.	
29.000	-23.66	14.44	-.0312	-1.79	3.33	24.54	13.76	-.02	299.	
30.000	-25.72	14.37	-.0318	-1.72	3.06	26.20	13.92	-.09	241.	
32.000	-22.08	13.70	.2329	-1.20	3.76	22.67	13.29	.16	73.	
34.000	-20.69	13.29	-.0989	-.63	3.93	27.03	13.20	.14	73.	
35.000	-31.33	12.49	-.2311	-.33	3.93	31.64	12.30	.37	73.	
36.000	-35.25	11.57	-.0309	-.16	4.86	33.50	11.48	.46	73.	
40.000	-40.42	10.19	-.1525	.78	4.86	40.74	10.10	.73	73.	
42.000	-45.43	14.21	.1820	.79	6.00	46.03	13.52	.32	73.	
44.000	-45.89	19.69	.2407	-1.66	8.01	47.04	18.60	-.21	73.	
46.000	-40.10	23.53	.2119	-2.93	8.87	41.82	22.33	.05	76.	
48.000	-30.13	24.64	.1806	-4.09	6.89	33.45	21.03	.81	77.	
50.000	-17.04	22.44	.1000	-6.78	8.21	24.44	18.10	1.34	77.	
52.000	-4.87	17.92	-.0712	-7.22	8.79	19.45	11.37	1.46	77.	
54.000	3.71	15.22	.0031	-6.07	10.01	18.17	8.94	.55	72.	
56.000	8.93	15.67	.0235	-3.64	10.44	19.33	10.43	1.04	62.	
58.000	11.89	11.72	.3424	-1.13	10.19	17.90	7.78	.22	53.	
60.000	15.81	12.35	.1816	-1.30	11.99	21.63	8.71	-.07	51.	
62.000	15.64	16.38	-.3610	1.09	12.55	23.25	11.09	.67	36.	
64.000	15.91	16.44	-.4237	.22	13.99	24.24	10.73	.61	21.	
66.000	12.53	20.57	.7527	-2.39	14.23	23.13	14.15	.42	8.	

TABLE I-3. WIND STATISTICAL PARAMETERS

## MARCH

STATION - 619020		ASCENSION (WIDE AWAKE)								
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS		
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-6.47	1.98	-.0870	3.75	1.78	7.74	1.76	-.14	506.	
1.000	-4.76	2.55	-.3311	2.69	2.13	5.84	2.62	.23	507.	
2.000	-2.66	3.79	-.3078	.44	2.57	4.63	2.50	.69	506.	
3.000	-2.61	3.85	-.1949	-.79	2.77	4.67	2.50	.58	505.	
4.000	-3.05	3.43	-.0725	-.75	2.66	4.30	2.43	.53	505.	
5.000	-4.17	3.25	-.1070	-.64	2.67	6.61	2.49	.30	506.	
6.000	-6.20	3.81	-.2044	-.31	3.10	6.43	2.03	.25	507.	
7.000	-5.55	3.87	-.2370	-.41	3.31	6.97	3.10	.33	507.	
8.000	-4.58	4.68	-.1631	-.68	3.81	6.82	3.36	.31	506.	
9.000	-2.97	5.61	-.0825	-.90	4.41	6.93	3.54	.78	505.	
10.000	-1.02	6.54	-.0407	-1.33	4.91	7.33	3.97	.92	505.	
11.000	.80	7.53	.0209	-1.99	5.59	8.36	4.74	1.16	505.	
12.000	2.22	8.13	.0362	-3.01	5.50	9.07	5.29	1.14	505.	
13.000	3.35	9.35	.0674	-3.55	5.70	10.36	6.03	.97	506.	
14.000	4.26	10.55	.0303	-3.10	5.51	11.24	6.56	.56	506.	
15.000	3.09	9.50	-.0031	-1.95	5.04	9.99	6.06	.96	505.	
16.000	-.29	7.25	-.0573	-1.32	4.18	7.37	4.17	1.15	500.	
17.000	-3.72	4.79	-.0021	-.66	3.32	6.12	3.27	.72	492.	
18.000	-5.51	5.59	.0530	.17	3.01	7.34	4.09	.52	491.	
19.000	-5.65	6.64	-.0155	.38	2.69	7.70	5.18	.82	430.	
20.000	-7.17	8.54	-.0030	.81	2.66	9.26	6.91	.02	483.	
21.000	-9.45	9.83	-.0445	1.20	2.79	11.03	8.57	.52	474.	
22.000	-12.00	10.51	.0205	1.63	3.02	13.31	9.46	.67	471.	
23.000	-13.54	9.27	.1379	1.73	2.55	14.25	8.69	.58	467.	
24.000	-14.67	9.54	.0257	1.51	3.25	15.47	8.94	.64	457.	
25.000	-16.13	10.43	-.0225	.09	3.09	16.69	9.99	.85	454.	
26.000	-17.42	11.81	-.0576	-1.01	2.83	18.01	11.30	.50	436.	
27.000	-18.93	13.13	-.0335	-1.78	2.79	19.77	12.24	.20	389.	
28.000	-20.68	13.85	-.0375	-2.37	2.90	21.69	12.76	.01	377.	
29.000	-22.87	14.46	.0316	-7.39	2.83	23.60	13.39	-.14	260.	
30.000	-24.03	14.16	-.0730	-2.10	2.69	24.77	13.26	-.29	268.	
32.000	-19.57	15.65	.0606	-.76	3.27	21.14	13.84	-.03	99.	
34.000	-23.02	14.32	-.0152	1.04	3.82	23.60	13.91	-.02	99.	
35.000	-27.68	13.01	-.1595	1.34	4.28	28.15	12.76	-.11	99.	
38.000	-29.76	11.34	.0653	.97	4.58	30.20	11.07	-.13	99.	
40.000	-27.05	12.83	.0837	-.83	5.07	27.79	12.25	.22	99.	
42.000	-19.41	19.31	.3700	.85	6.45	23.31	15.72	.49	68.	
44.000	-8.25	20.83	.3028	1.06	7.81	19.60	13.30	.89	101.	
46.000	-.10	17.78	.0375	-.20	7.01	16.21	10.00	.69	101.	
48.000	4.37	16.20	.0833	-1.56	7.63	16.17	9.27	.80	100.	
50.000	11.87	13.92	.0347	-4.11	7.16	18.25	8.08	.19	100.	
52.000	17.12	12.95	.2441	-3.80	8.66	21.23	9.62	-.06	99.	
54.000	21.08	11.48	.0792	-3.61	8.53	23.59	10.21	-.32	96.	
56.000	23.79	11.56	.0417	-3.08	8.42	25.78	10.69	.02	91.	
58.000	24.29	13.64	.1266	-.33	9.26	26.41	12.78	.30	79.	
60.000	25.73	16.95	.1673	.03	10.92	29.47	14.05	.51	66.	
62.000	23.89	20.27	.0510	.77	14.30	30.84	15.10	.44	50.	
64.000	23.00	19.58	-.3154	-.02	10.19	28.19	15.63	.59	27.	
65.000	30.99	24.18	.2276	-.92	15.87	37.11	19.18	.28	9.	

TABLE I-4. WIND STATISTICAL PARAMETERS

APRIL

STATION - 619020		ASCENSION (WIDE AWAKE)								
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS	NOBS	
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-6.84	1.93	.1010	3.80	1.72	8.04	1.77	-.36	485.	
1.000	-5.37	2.07	-.3240	2.93	2.19	6.40	2.91	.01	481.	
2.000	-3.04	4.32	-.1472	.29	2.49	5.12	2.82	.74	484.	
3.000	-2.30	4.15	-.2105	-.71	2.57	4.75	2.65	.58	484.	
4.000	-2.26	3.63	-.1810	-.05	2.57	4.42	2.44	.60	465.	
5.000	-2.89	3.54	-.1772	-.51	2.69	4.73	2.48	.53	483.	
6.000	-3.47	3.60	-.1012	-.20	3.05	5.37	2.75	.70	486.	
7.000	-3.53	4.42	-.0013	.10	3.34	5.79	3.11	.73	465.	
8.000	-2.70	5.26	-.1147	.49	3.78	6.12	3.46	1.02	487.	
9.000	-.65	5.94	-.1465	.33	4.27	6.33	3.78	.55	485.	
10.000	1.14	6.57	-.0617	-.54	5.09	7.15	4.41	1.23	483.	
11.000	2.51	7.21	.0348	-2.49	6.02	8.72	4.95	1.29	482.	
12.000	3.56	7.76	.0315	-3.20	6.09	9.57	5.40	1.31	481.	
13.000	4.40	8.72	.0171	-3.46	6.04	10.36	6.03	1.06	480.	
14.000	4.73	9.48	-.0361	-2.62	5.40	10.38	6.43	1.13	480.	
15.000	3.59	9.23	.0003	-1.93	4.54	9.36	5.90	1.33	479.	
16.000	.35	7.57	.0603	-1.33	3.77	7.17	4.67	1.40	479.	
17.000	-3.09	6.15	-.0377	-.61	3.32	6.61	3.90	1.05	471.	
18.000	-4.03	6.31	-.0409	.06	3.25	6.82	4.47	1.56	472.	
19.000	-3.44	7.16	-.0582	.43	2.62	6.83	4.84	1.20	463.	
20.000	-4.72	8.53	-.0947	.74	2.53	7.95	6.21	1.05	463.	
21.000	-6.66	9.25	-.0701	.97	2.80	9.25	7.16	.69	457.	
22.000	-8.20	9.26	-.0190	1.02	3.04	10.34	7.51	1.04	451.	
23.000	-10.01	6.90	.0321	1.05	2.33	11.19	7.76	.91	433.	
24.000	-11.96	10.58	.0102	.07	2.85	13.38	9.07	.72	435.	
25.000	-14.07	11.96	.0154	.71	3.00	15.54	10.44	.43	431.	
26.000	-15.79	13.09	-.0039	.06	2.75	17.31	11.33	.25	415.	
27.000	-16.84	14.24	-.0122	-.81	2.89	18.65	11.83	.07	367.	
28.000	-17.83	14.65	.0121	-1.74	2.99	20.26	11.64	-.03	355.	
29.000	-18.04	15.75	.0554	-2.30	3.26	21.03	12.11	-.04	260.	
30.000	-17.50	15.95	-.0423	-2.24	2.78	21.01	12.03	-.10	261.	
32.000	-10.79	17.53	.1697	-.40	3.42	17.40	11.44	.21	50.	
34.000	-11.64	16.71	.1740	1.49	3.08	17.23	11.55	.42	91.	
35.000	-12.42	14.65	.0794	1.00	3.68	15.90	11.53	.57	91.	
38.000	-0.44	14.13	.1905	1.17	4.14	14.59	9.64	1.01	92.	
40.000	-.45	14.65	.1576	1.22	8.02	13.66	8.02	.41	92.	
42.000	9.39	14.17	.2151	3.47	5.01	16.12	8.04	.30	92.	
44.000	18.01	10.55	.1072	2.91	5.34	20.00	8.48	.00	93.	
46.000	21.93	9.25	-.1523	1.25	5.08	22.72	8.79	.05	93.	
48.000	24.10	10.21	-.0155	-1.12	5.23	25.10	9.20	.10	53.	
50.000	25.05	11.31	.0748	-2.37	5.60	27.05	9.93	-.23	53.	
52.000	28.63	11.73	-.0071	-2.51	6.07	23.75	10.72	-.34	50.	
54.000	32.62	12.01	.0206	-1.43	6.63	33.59	11.21	-.26	90.	
56.000	35.45	11.16	.0425	.19	8.36	37.54	10.60	-.25	83.	
58.000	40.57	11.87	-.3547	1.38	9.08	41.73	11.36	-.31	73.	
60.000	40.09	13.32	-.3075	3.61	8.85	41.51	12.31	-.19	59.	
62.000	43.40	17.64	-.2203	4.33	11.35	45.85	15.51	-.52	46.	
64.000	35.77	19.75	-.1532	8.67	11.54	41.36	15.15	.21	28.	
66.000	29.88	25.34	-.0658	3.31	11.75	25.62	17.65	.72	13.	

TABLE I-5. WIND STATISTICAL PARAMETERS

MAY

STATION = 619320		ASCENSION (WIDE AWAKE)								NOBS
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS		
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-7.28	1.50	.0403	3.67	1.69	6.36	1.75	-.33	509.	
1.000	-5.42	2.61	-.3183	2.52	2.10	5.33	2.82	.03	509.	
2.000	-1.56	3.87	-.0000	.05	2.54	4.43	2.38	.77	510.	
3.000	-.56	3.81	-.1053	-.87	2.83	4.29	2.28	.65	510.	
4.000	-.86	3.72	-.1246	-.59	2.91	4.18	2.43	1.15	510.	
5.000	-1.69	4.04	-.2302	-.24	2.94	4.56	2.65	1.00	510.	
6.000	-2.43	4.92	-.2005	-.16	3.23	5.50	3.19	.74	510.	
7.000	-2.43	5.52	-.1506	.14	3.60	6.05	3.57	.79	509.	
8.000	-1.04	6.11	-.1427	.40	4.46	6.64	3.78	.93	504.	
9.000	1.20	6.71	-.1630	-.09	5.08	7.36	4.27	1.00	503.	
10.000	3.08	6.91	-.1031	-1.80	5.47	6.16	4.67	1.01	504.	
11.000	4.42	7.27	-.0246	-4.02	6.03	9.64	5.65	.79	504.	
12.000	5.50	7.88	.0013	-4.80	5.58	10.54	5.34	.72	505.	
13.000	6.43	8.30	.1328	-5.03	5.60	11.67	6.26	.61	504.	
14.000	7.53	9.40	.1089	-4.56	5.46	12.34	6.68	.60	503.	
15.000	7.52	9.12	.0815	-3.75	5.05	11.74	6.43	.58	504.	
16.000	4.10	7.35	.0347	-2.37	4.19	8.45	4.75	.70	503.	
17.000	-.03	5.60	-.0247	-.91	3.65	6.03	3.43	.64	456.	
18.000	-1.45	6.52	-.0700	.01	3.29	6.44	3.73	.60	450.	
19.000	.25	6.70	-.0400	.30	2.70	6.41	3.55	.54	491.	
20.000	-.25	7.51	-.0244	.70	2.73	6.75	4.32	.92	485.	
21.000	-2.60	8.32	.0976	.50	2.87	7.37	5.49	1.20	477.	
22.000	-5.60	9.31	.0373	.23	2.81	8.36	6.18	.93	475.	
23.000	-8.17	10.79	-.0323	.03	2.36	11.44	7.60	.55	466.	
24.000	-10.41	12.93	-.0000	-.14	2.82	14.31	8.97	.17	463.	
25.000	-12.00	14.62	-.1500	-.12	3.02	16.93	9.25	-.03	456.	
26.000	-13.12	15.64	-.0503	-.18	2.95	16.52	9.00	-.14	441.	
27.000	-13.68	16.47	.0217	-.52	3.22	19.55	9.28	-.16	399.	
28.000	-13.57	17.18	-.0044	-1.23	2.97	20.04	9.35	-.16	391.	
29.000	-14.46	17.72	-.0105	-1.53	3.28	21.12	9.45	-.35	319.	
30.000	-13.65	18.09	-.0539	-1.10	2.95	20.78	9.55	-.28	304.	
32.000	-3.43	18.53	-.0751	.40	3.42	17.64	3.28	-.13	73.	
34.000	-3.68	15.99	.2706	1.62	4.43	15.01	7.94	.27	73.	
36.000	-1.62	13.41	-.0572	2.04	4.20	12.53	6.71	.61	73.	
38.000	4.51	13.45	-.1225	2.44	4.20	13.00	7.33	.32	73.	
40.000	11.16	12.64	-.1403	3.15	4.03	15.81	7.69	.28	73.	
42.000	16.30	10.75	-.1765	2.67	4.29	17.05	9.17	.33	73.	
44.000	17.84	9.84	-.2551	2.38	5.19	19.28	8.67	.32	76.	
46.000	17.74	11.20	-.1604	2.07	5.97	19.59	9.77	.21	75.	
48.000	15.78	12.97	-.0931	-.57	7.35	19.20	10.07	.14	75.	
50.000	16.49	13.00	-.1429	-2.22	7.01	20.14	9.37	.15	74.	
52.000	18.89	14.30	-.0557	-2.56	7.46	22.62	10.47	.26	74.	
54.000	21.63	15.83	.0300	-1.01	6.30	24.63	12.14	-.08	71.	
56.000	25.25	17.80	-.0977	2.28	8.44	28.43	13.79	.04	67.	
58.000	26.57	20.63	-.0342	5.57	7.65	31.59	14.80	.04	59.	
60.000	26.33	26.55	.3207	5.40	8.95	34.59	17.34	-.20	37.	
62.000	32.53	31.14	.3252	5.81	9.98	42.36	18.25	-.81	22.	
64.000	28.57	36.70	.6788	5.77	18.74	46.23	17.40	.19	13.	
66.000	20.91	35.06	.6596	4.99	15.06	35.25	21.95	-.03	8.	

TABLE 1-6. WIND STATISTICAL PARAMETERS

JUNE

STATION - 810020		ASCENSION (WIDE AWAKE)							
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS	NCOS
KM	M/S	M/S		M/S	M/S	M/S	M/S		
.000	-7.21	1.56	.1400	3.51	1.80	8.28	1.78	.02	474.
1.000	-5.39	2.60	-.3114	2.85	2.19	6.45	2.06	.12	474.
2.000	-1.68	3.58	-.0047	.47	2.70	4.24	2.38	.73	475.
3.000	-.14	3.65	-.1641	-.70	3.25	4.33	2.29	.53	475.
4.000	-.52	4.14	-.1822	-.66	3.03	4.59	2.48	.62	475.
5.000	-1.89	4.78	-.1370	-.26	2.97	5.18	2.85	.82	475.
6.000	-2.93	5.91	-.0457	.19	3.52	6.48	3.73	.68	475.
7.000	-2.89	6.68	-.0337	.66	4.43	7.51	4.07	.83	475.
8.000	-1.50	6.95	-.1713	.48	5.02	7.51	4.22	.82	474.
9.000	.22	7.13	-.1525	-1.00	5.58	8.00	4.75	.78	474.
10.000	1.35	7.25	-.0493	-2.09	6.01	8.87	4.55	.58	472.
11.000	1.99	8.07	.1218	-5.24	6.51	10.61	5.12	.46	471.
12.000	3.57	9.17	.2534	-5.06	6.59	11.85	5.64	.57	471.
13.000	5.23	9.81	.1667	-5.21	6.22	12.38	5.99	.55	470.
14.000	6.57	9.10	.0083	-3.86	5.72	11.70	6.05	.47	470.
15.000	5.67	7.86	-.0537	-2.35	5.41	9.87	5.58	.61	465.
16.000	2.10	6.45	.0177	-1.31	4.34	7.07	4.05	.89	463.
17.000	-.63	5.76	.0332	-.65	3.41	5.68	3.33	.78	455.
18.000	-.32	6.17	-.0177	-.32	3.28	6.05	3.50	.93	454.
19.000	1.45	6.38	-.1531	-.15	2.85	6.24	3.54	.63	451.
20.000	1.18	7.24	-.1512	-.08	2.80	6.83	3.66	.67	449.
21.000	-.80	9.10	-.0613	.05	2.78	8.09	5.05	.78	432.
22.000	-4.34	11.79	.0420	.22	2.64	11.24	6.27	.42	430.
23.000	-7.30	13.32	-.0203	.10	2.56	13.43	7.54	.12	425.
24.000	-9.76	14.94	-.0843	-.33	3.14	16.12	8.26	-.07	422.
25.000	-10.87	15.55	-.1650	-.68	2.84	17.50	7.83	-.13	415.
26.000	-11.50	16.15	-.1675	-.62	2.84	18.56	8.03	-.16	394.
27.000	-11.77	16.99	-.1231	-.97	3.26	18.06	8.05	-.22	353.
28.000	-11.49	17.55	-.0659	-.94	2.78	19.05	8.22	-.24	345.
29.000	-12.23	17.87	-.0049	-.89	3.05	19.72	9.46	-.29	280.
30.000	-11.08	17.01	.0219	-.45	2.72	18.21	9.35	-.10	262.
32.000	-3.93	15.56	-.0433	.35	3.64	13.08	9.06	.96	61.
34.000	-1.80	14.43	-.1373	-.32	3.57	12.67	7.82	.56	61.
36.000	.25	17.02	.4073	.06	4.31	15.03	7.73	.44	61.
38.000	4.84	15.36	.3526	1.61	3.97	15.52	8.05	.33	61.
40.000	6.90	13.81	.0463	1.77	4.63	14.33	7.29	.38	61.
42.000	7.45	13.28	-.1927	2.00	5.06	14.41	7.36	.61	61.
44.000	5.32	14.62	-.1394	3.55	5.30	14.84	7.73	.64	61.
46.000	1.73	15.45	.0069	3.28	6.08	14.84	8.12	.34	61.
48.000	-1.31	17.53	.1402	.37	7.41	16.25	9.79	.58	61.
50.000	-1.48	20.34	.1990	-3.08	6.35	17.92	11.80	.68	60.
52.000	1.40	23.97	.3374	-2.75	7.72	21.51	13.17	.78	59.
54.000	7.52	23.27	.0221	-.59	8.37	22.64	12.17	.65	59.
56.000	12.29	21.09	.1326	1.47	9.41	23.17	13.47	.66	59.
58.000	18.31	19.57	-.1025	2.33	7.76	24.17	13.94	.43	47.
60.000	24.26	20.77	-.2193	3.60	10.20	30.30	14.51	-.05	33.
62.000	26.53	23.31	.0760	2.09	12.13	32.27	17.46	.21	23.
64.000	30.64	18.00	-.0463	1.66	13.69	35.57	12.76	-.03	14.
66.000	33.47	18.72	-.2482	-2.04	9.89	35.67	16.51	-.02	6.

TABLE E-7. WIND STATISTICAL PARAMETERS

JULY

STATION - 619020		ASCENSION (WIDE AWAKE)				S.D. V	MEAN WS	S.D. WS	SKEW WS	NOBS
Z	MEAN U	S.D. U	R(U,V)	MEAN V	M/S					
M/H	M/S	M/S		M/S	M/S		M/S	M/S		
.020	-7.38	1.91	-.0589	3.47	1.88	8.43	1.73	-.09	462.	
1.000	-5.02	2.69	-.1870	3.18	2.32	7.06	2.60	.10	467.	
2.000	-1.79	3.95	-.0053	.46	3.08	4.63	2.55	.74	467.	
3.000	.30	4.36	-.0074	-1.21	3.48	5.09	2.60	.46	467.	
4.000	-2.84	4.40	-.1827	-.00	3.00	4.72	2.64	.81	467.	
5.000	-2.39	4.62	-.1076	-.37	3.14	5.25	3.05	.85	467.	
6.000	-3.50	5.40	-.1823	-.18	3.64	6.37	3.76	1.01	463.	
7.000	-3.18	6.04	-.0050	.19	4.02	6.83	3.83	.75	467.	
8.000	-1.83	6.67	-.1312	.32	4.56	7.32	3.90	.79	463.	
9.000	-.36	7.40	-.0771	-.68	5.66	8.31	4.31	.78	465.	
10.000	.88	8.24	.0009	-2.72	6.45	9.71	4.82	.48	465.	
11.000	2.27	9.91	.2033	-3.89	7.21	11.66	5.80	.41	462.	
12.000	4.46	11.30	.2176	-4.05	6.71	12.82	6.65	.49	463.	
13.000	7.04	11.38	.1933	-3.32	6.59	13.91	7.32	.61	469.	
14.000	8.71	11.09	.0440	-1.71	5.96	13.30	7.76	.52	456.	
15.000	6.15	8.62	-.0350	-.80	4.84	9.99	6.02	.79	455.	
16.000	1.43	6.44	-.1025	-.83	3.85	6.67	3.82	.98	454.	
17.000	-.86	5.37	-.0953	-.33	3.30	5.46	3.27	.83	445.	
18.000	.42	5.51	-.0171	.52	3.34	5.54	3.35	.97	446.	
19.000	1.65	5.68	.0023	.66	2.84	5.69	3.32	.85	445.	
20.000	.92	7.60	.0325	.68	2.67	7.05	4.02	1.12	434.	
21.000	-1.84	11.11	.0749	.46	3.14	10.34	5.44	.71	426.	
22.000	-5.56	13.68	.1187	-.11	2.95	13.42	6.01	.25	423.	
23.000	-7.61	14.13	.0220	-.24	2.74	14.37	7.64	.09	412.	
24.000	-9.17	14.75	-.0721	-.22	3.35	15.73	8.08	.04	409.	
25.000	-10.57	14.80	-.1762	-.12	3.04	16.39	9.44	.11	395.	
26.000	-11.53	14.90	-.1713	-.28	2.82	16.75	9.05	-.01	381.	
27.000	-12.02	15.27	-.1129	-.64	3.23	17.11	9.77	-.04	356.	
28.000	-12.35	15.09	-.0023	-.60	2.83	16.79	10.31	.06	346.	
29.000	-13.47	15.18	.0753	-.28	3.21	17.81	10.21	-.03	278.	
30.000	-12.28	13.53	.1309	.14	2.82	15.22	9.67	.09	260.	
32.000	-5.50	12.27	.1561	.65	3.56	10.77	8.81	1.10	87.	
34.000	-5.38	10.72	.1160	.35	3.29	10.43	8.72	.92	87.	
36.000	-7.63	12.91	.0409	.04	4.01	13.38	7.79	.59	87.	
38.000	-9.69	15.42	.1294	.93	4.18	15.52	10.37	.80	87.	
40.000	-11.05	15.61	.0270	2.11	5.25	16.86	10.58	.67	87.	
42.000	-13.45	15.23	.0152	3.32	5.96	18.38	11.00	.32	87.	
44.000	-16.78	15.94	-.0554	4.05	6.56	20.64	12.05	.26	89.	
46.000	-21.20	16.50	-.0469	4.60	6.73	24.53	14.00	.27	89.	
48.000	-24.18	16.76	.0393	1.28	7.91	27.06	13.53	.30	88.	
50.000	-23.37	17.29	.2692	-1.79	8.19	26.57	14.41	.53	87.	
52.000	-17.39	15.98	.1089	-3.35	7.71	21.30	13.15	.73	65.	
54.000	-7.96	15.50	.0499	-2.37	8.81	17.52	8.57	.90	84.	
56.000	.98	14.91	-.1023	-2.67	9.44	16.17	7.39	.31	80.	
58.000	9.61	14.04	-.2011	-2.72	11.48	18.32	9.47	.56	69.	
60.000	13.88	16.38	.1206	1.88	10.72	21.00	11.52	.51	44.	
62.000	18.28	17.22	.4094	7.51	9.70	24.03	14.05	.28	35.	
64.000	22.28	17.71	-.3052	5.83	9.69	27.43	13.16	.53	23.	
66.000	22.19	23.68	.0392	10.49	12.69	33.00	13.65	-.12	11.	

TABLE I-8. WIND STATISTICAL PARAMETERS

AUGUST

STATION # 815020		ASCENSION (WIDE AWAKE)								
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS	NOBS	
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-7.34	1.77	.0039	3.45	1.59	8.29	1.67	-.15	483.	
1.000	-6.59	2.51	-.2012	3.60	2.14	7.00	2.51	-.30	481.	
2.000	-3.77	4.16	-.16.2	.79	2.60	5.52	2.69	.56	480.	
3.000	-1.94	4.54	-.0337	-1.00	3.16	5.31	2.59	.54	479.	
4.000	-1.04	4.14	-.1735	-.87	3.29	5.04	2.61	.83	479.	
5.000	-2.70	4.50	-.1274	-.18	3.22	5.47	2.69	.63	479.	
6.000	-3.28	5.13	-.0258	.09	3.71	6.32	3.27	.50	480.	
7.000	-2.24	5.79	-.0700	.51	4.09	6.63	3.46	.66	480.	
8.000	-.00	6.48	-.0213	.56	4.78	7.19	3.79	.63	478.	
9.000	.15	7.39	-.1732	-.77	5.67	8.24	4.41	.76	478.	
10.000	.05	8.39	.1315	-2.72	6.60	9.73	5.24	.64	477.	
11.000	2.18	10.19	.3114	-4.30	8.07	12.27	6.43	.46	476.	
12.000	5.25	10.67	.3773	-3.53	8.05	12.95	7.12	.60	476.	
13.000	8.41	10.41	.2270	-2.14	7.23	13.45	7.39	.43	475.	
14.000	9.62	8.62	.0772	-.77	6.23	12.62	6.91	.37	475.	
15.000	6.51	5.03	-.0771	-.83	5.31	9.54	5.21	.53	474.	
16.000	2.00	5.53	-.2703	-1.04	4.02	6.28	3.52	.73	473.	
17.000	-.45	4.79	-.2774	-.30	3.06	5.06	2.63	.70	470.	
18.000	.38	5.28	-.0091	.35	3.10	5.30	3.10	1.03	469.	
19.000	1.60	6.59	-.0740	.51	2.77	6.20	3.92	1.20	469.	
20.000	.40	8.79	-.0446	.61	2.67	8.03	4.50	.98	467.	
21.000	-2.51	11.90	-.0134	.54	2.98	11.26	5.43	.23	463.	
22.000	-5.53	13.98	.0674	.25	2.84	13.55	7.03	.20	459.	
23.000	-7.99	14.72	.1033	.23	2.69	14.02	8.21	.20	448.	
24.000	-9.41	14.06	.0627	.20	3.30	15.03	8.92	.15	443.	
25.000	-11.16	14.99	-.0346	.05	2.95	16.38	9.29	.05	433.	
26.000	-11.53	15.29	-.0924	-.56	2.94	17.06	9.71	.03	419.	
27.000	-11.82	16.13	-.0003	-1.02	3.08	17.38	10.38	.13	381.	
28.000	-12.13	16.19	-.0053	-.60	2.81	17.22	10.93	.09	374.	
29.000	-13.17	15.68	-.0037	-.46	3.06	17.74	10.65	-.03	304.	
30.000	-12.43	14.04	-.0091	-.03	2.73	16.11	9.95	.09	289.	
32.000	-5.40	12.05	.1020	.41	3.60	11.43	6.23	.00	89.	
34.000	-7.18	11.41	-.0149	.06	3.91	12.01	7.18	.71	89.	
36.000	-9.10	13.22	-.0150	-.70	4.55	14.02	8.54	.61	60.	
38.000	-12.77	18.04	-.0390	.72	8.54	17.57	11.80	.47	89.	
40.000	-16.14	15.92	.0008	2.73	6.00	19.02	12.77	.41	88.	
42.000	-15.90	13.12	.0172	4.28	6.18	19.29	10.41	.36	88.	
44.000	-16.05	11.75	-.0633	4.21	8.08	19.32	10.09	.33	88.	
46.000	-15.98	11.65	-.1944	2.21	7.07	18.97	10.09	.34	88.	
48.000	-12.14	12.18	-.0073	-.15	6.93	18.07	9.19	.68	89.	
50.000	-6.04	12.36	.0343	-2.03	7.10	13.03	8.47	.73	87.	
52.000	-1.25	13.83	-.0093	-2.44	7.60	13.47	8.63	.93	86.	
54.000	2.37	13.11	-.0750	-2.20	7.94	13.30	8.15	.63	84.	
56.000	8.15	13.73	-.1565	-1.17	8.32	15.71	8.74	.56	79.	
58.000	14.05	13.60	-.1306	2.92	8.77	19.57	9.06	.45	68.	
60.000	18.01	14.42	.0331	6.42	12.44	24.30	11.55	.22	53.	
62.000	22.68	16.56	-.0057	11.07	15.91	30.91	14.10	.07	33.	
64.000	27.30	17.33	-.1571	9.10	16.74	35.00	13.60	-.17	20.	
66.000	23.49	18.57	-.3741	22.13	11.88	36.70	12.11	.03	10.	



TABLE I-9. WIND STATISTICAL PARAMETERS

SEPTEMBER

STATION = 819020		ASCENSION (WIDE AWAKE)								NOBS
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS		
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-6.95	1.85	.1129	3.54	1.60	8.01	1.69	-.40	445.	
1.000	-6.05	2.55	-.2530	3.51	2.15	8.01	2.47	-.25	444.	
2.000	-6.51	4.28	-.1773	1.09	2.92	7.59	3.58	.41	444.	
3.000	-5.89	5.04	-.2247	-.79	2.81	7.46	3.59	.45	443.	
4.000	-4.24	4.93	-.0723	-1.14	2.86	6.23	3.60	.66	443.	
5.000	-3.27	4.46	-.2616	-.43	2.94	5.36	3.27	.93	443.	
6.000	-3.43	5.16	-.2097	.13	3.18	5.92	3.67	1.15	443.	
7.000	-3.03	5.97	-.0365	.33	3.73	6.57	3.94	.91	443.	
8.000	-1.47	6.55	-.0333	-.21	4.31	7.04	3.75	.64	443.	
9.000	.14	7.42	-.0058	-1.60	5.30	8.25	4.19	.60	443.	
10.000	1.85	8.60	.1373	-3.09	6.39	10.17	4.92	.80	442.	
11.000	4.09	9.65	.2015	-4.01	6.55	12.01	5.82	.49	441.	
12.000	7.81	10.46	.1591	-3.05	6.50	13.17	6.94	.56	441.	
13.000	10.55	10.43	.0404	-2.05	6.11	14.45	7.83	.31	441.	
14.000	12.11	9.30	-.0597	-1.15	5.59	14.43	7.57	.16	442.	
15.000	9.30	7.33	-.0305	-1.09	4.97	11.35	6.10	.41	442.	
16.000	3.47	5.35	-.1222	-1.40	3.85	6.67	3.59	.63	440.	
17.000	-.38	4.74	-.1735	-.04	2.91	4.96	2.67	.65	435.	
18.000	-.22	5.52	-.0550	.23	3.10	5.44	3.24	1.22	434.	
19.000	.28	6.67	-.0422	.31	2.69	6.16	3.00	1.00	431.	
20.000	-.86	9.09	-.1063	.45	2.86	8.52	4.37	.09	426.	
21.000	-2.65	12.10	-.0749	.32	2.97	11.40	5.78	.35	418.	
22.000	-5.44	14.30	-.0039	.53	2.95	13.68	7.61	.43	416.	
23.000	-7.36	15.14	-.0003	.65	2.83	14.56	8.91	.30	400.	
24.000	-9.57	15.77	-.0223	.54	3.71	16.06	8.81	.35	326.	
25.000	-11.10	14.84	-.0045	.00	3.22	15.97	9.92	.16	389.	
26.000	-12.00	14.40	-.1945	-.52	2.82	15.68	10.34	.15	301.	
27.000	-12.61	14.80	-.2130	-.86	3.37	16.49	10.87	.18	332.	
28.000	-12.91	14.51	-.2222	-.93	2.69	15.65	11.57	.25	320.	
29.000	-14.20	14.30	-.1871	-.80	3.14	17.10	11.13	.15	243.	
30.000	-13.87	13.54	.0000	-.65	2.63	16.25	10.90	.22	220.	
32.000	-6.48	12.51	.0757	-.61	3.53	12.43	7.42	.52	88.	
34.000	-6.00	14.33	-.0226	.40	3.30	13.99	7.42	.33	88.	
36.000	-6.97	15.65	.0956	.29	3.95	14.99	9.11	.47	88.	
38.000	-8.78	16.64	-.1077	.63	4.13	15.58	11.27	.43	68.	
40.000	-10.90	17.12	-.0094	1.23	5.75	17.17	12.23	.65	83.	
42.000	-10.28	16.39	.0479	1.12	5.15	16.78	10.90	1.17	89.	
44.000	-7.09	14.82	-.0387	2.83	5.02	14.44	9.63	1.48	91.	
46.000	-1.57	14.88	-.1470	3.06	6.28	14.11	8.45	.96	92.	
48.000	3.21	13.61	-.0243	.51	6.53	13.32	7.69	.84	91.	
50.000	6.45	13.67	-.1207	-3.31	7.29	14.65	8.73	.95	91.	
52.000	8.00	15.75	.0450	-5.40	6.65	17.39	8.93	.52	90.	
54.000	9.71	15.68	.1153	-5.12	6.24	17.75	9.38	.50	87.	
56.000	12.97	13.27	.0190	-1.81	8.07	17.78	9.59	.48	89.	
58.000	16.18	14.18	.0479	3.26	8.02	20.29	11.16	.59	80.	
60.000	20.26	15.00	-.1762	7.14	8.44	24.55	12.14	.91	66.	
62.000	25.69	17.52	.0154	7.84	10.00	30.00	14.98	.42	49.	
64.000	34.12	19.46	.3769	8.64	11.65	38.58	15.98	.33	26.	
66.000	48.06	16.73	.0504	6.32	11.69	43.60	16.48	-.25	10.	

TABLE I-10. WIND STATISTICAL PARAMETERS

OCTOBER

STATION - 619020		ASCENSION (WIDE AWAKE)								NOBS
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS		
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-7.15	1.61	.0975	3.20	1.60	8.00	1.55	-.10	461.	
1.000	-6.97	2.37	-.2032	2.78	2.13	7.79	2.47	-.14	461.	
2.000	-7.30	4.40	-.0783	.63	2.79	8.16	3.76	.39	460.	
3.000	-7.14	4.91	-.2005	-.41	2.61	8.21	3.62	.20	460.	
4.000	-5.67	4.96	-.0486	-1.10	2.55	7.05	3.84	.48	459.	
5.000	-4.18	4.28	-.0748	-.83	2.84	5.87	3.18	.82	460.	
6.000	-3.61	4.82	-.2983	-.61	3.35	6.09	3.27	1.03	461.	
7.000	-2.56	5.18	-.2724	-.19	4.03	6.22	3.32	.91	461.	
8.000	-.37	5.95	-.2059	.09	4.97	6.71	3.88	1.26	458.	
9.000	2.60	6.84	-.2418	-.32	6.08	8.24	4.75	.97	453.	
10.000	5.47	7.48	-.1627	-1.23	7.12	10.36	5.56	.59	460.	
11.000	8.21	8.35	-.0516	-2.55	8.19	13.04	6.37	.37	460.	
12.000	11.21	8.82	-.0533	-2.94	7.66	14.53	6.91	.17	460.	
13.000	13.56	8.68	-.1335	-2.63	7.31	16.35	7.47	.18	463.	
14.000	14.28	8.57	-.2546	-1.93	6.46	18.24	7.66	.21	462.	
15.000	11.54	7.81	-.1945	-1.49	5.28	13.37	6.74	.43	461.	
16.000	5.47	6.04	-.0355	-1.33	4.08	7.96	4.63	.85	460.	
17.000	.32	4.29	-.1114	-.85	3.16	5.21	2.91	.67	459.	
18.000	-.82	5.59	.0973	.33	3.02	5.40	3.45	1.30	447.	
19.000	-.80	6.31	.1287	.39	2.67	5.83	3.71	1.30	447.	
20.000	-1.99	8.78	.0005	.35	2.70	8.30	4.38	.40	443.	
21.000	-4.40	12.29	-.1073	.22	2.76	11.49	6.75	.48	409.	
22.000	-6.65	14.48	-.1034	.23	3.15	13.85	8.46	.30	427.	
23.000	-8.67	14.85	-.0620	.49	2.71	14.32	9.89	.33	412.	
24.000	-11.13	15.27	-.0025	.63	3.43	15.91	10.76	.28	406.	
25.000	-13.12	14.33	.0504	.71	2.87	16.48	10.70	.10	363.	
26.000	-14.09	13.72	.1250	.22	2.51	16.49	11.00	.10	376.	
27.000	-14.78	13.63	.0242	-.58	3.18	17.01	11.20	.03	344.	
28.000	-14.01	12.94	-.1023	-.66	2.67	16.00	10.85	.24	335.	
29.000	-13.92	13.21	-.2039	-2.01	3.13	16.59	10.34	.27	262.	
30.000	-12.69	13.34	-.1739	-2.03	2.81	15.72	10.17	.37	246.	
32.000	-7.59	14.50	.0334	-1.00	3.86	14.40	8.63	.27	83.	
34.000	-9.22	15.71	-.0559	-.03	3.44	16.07	9.13	.14	83.	
36.000	-8.74	17.79	-.0252	.80	3.69	17.36	10.15	.30	83.	
38.000	-7.62	17.41	-.0275	.20	4.12	16.34	10.43	.56	83.	
40.000	-3.25	14.35	.1445	.26	4.63	12.89	9.41	1.03	83.	
42.000	.45	11.29	.0144	1.62	5.14	10.00	6.28	.63	64.	
44.000	4.25	11.50	-.2857	2.13	6.32	12.01	7.04	.75	87.	
46.000	8.35	10.56	-.4203	-.97	7.18	12.69	8.01	1.08	85.	
48.000	11.38	10.91	-.5467	-2.31	6.45	14.62	8.99	.85	85.	
50.000	12.57	11.70	-.1209	-3.29	6.40	16.39	8.78	.39	85.	
52.000	14.13	13.29	.2135	-2.03	7.12	18.92	8.42	.41	83.	
54.000	17.89	11.54	.1052	-2.73	7.27	20.98	8.50	.10	81.	
56.000	19.76	8.28	.1603	-1.52	6.54	21.29	8.23	.29	72.	
58.000	20.07	9.23	-.0059	-1.78	7.31	21.35	8.13	.00	60.	
60.000	23.05	11.90	.1331	.62	7.81	25.13	10.02	-.03	46.	
62.000	24.69	11.31	.0262	3.79	8.53	26.66	10.56	.00	38.	
64.000	26.68	9.70	.0375	3.77	7.61	28.19	9.54	-.11	27.	
66.000	23.33	16.57	-.0991	6.67	13.28	29.44	12.44	.18	16.	

TABLE I-11. WIND STATISTICAL PARAMETERS

## NOVEMBER

STATION = 619020		ASCENSION (WIDE AWAKE)								
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS	NOBS	
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-6.92	1.63	.0916	3.26	1.50	7.81	1.55	-.18	463.	
1.000	-5.90	2.34	-.3269	2.35	2.33	6.63	2.36	-.18	462.	
2.000	-6.15	3.67	-.2579	-.19	2.74	7.02	3.09	.62	462.	
3.000	-5.89	4.20	-.2109	-.97	2.85	7.14	3.22	.31	462.	
4.000	-4.77	4.15	-.0739	-.80	2.87	6.22	3.18	.44	461.	
5.000	-4.07	3.98	-.1014	-.61	3.44	6.00	2.92	.45	461.	
6.000	-3.54	4.51	-.2053	-.64	3.69	6.11	3.09	.59	459.	
7.000	-2.31	5.42	-.1002	-.65	4.04	6.33	3.37	.64	459.	
8.000	-.02	6.25	-.2225	-.32	4.93	7.00	3.79	.82	458.	
9.000	3.03	7.33	-.1621	-.57	5.93	8.59	4.93	.72	457.	
10.000	6.24	8.30	-.1448	-1.75	6.83	11.04	6.01	.59	456.	
11.000	9.25	9.26	-.1233	-3.59	7.97	14.07	7.07	.34	452.	
12.000	11.94	9.47	-.1226	-4.55	8.07	15.69	7.83	.31	450.	
13.000	13.97	9.60	-.2172	-4.72	7.63	17.23	8.41	.23	450.	
14.000	14.55	9.47	-.2355	-4.07	6.75	17.09	8.45	.32	448.	
15.000	12.13	8.83	-.3200	-2.75	5.94	14.36	7.55	.57	448.	
16.000	6.17	7.35	-.0532	-2.20	4.91	9.65	5.27	1.01	446.	
17.000	.43	5.94	-.0039	-1.63	3.94	6.41	3.53	.81	439.	
18.000	-2.27	5.40	-.0941	-.69	3.09	5.83	3.22	.62	436.	
19.000	-1.96	6.18	.0110	-.16	2.71	6.08	3.53	.58	432.	
20.000	-3.42	9.14	-.0163	.26	2.65	8.65	5.24	.73	425.	
21.000	-6.45	11.82	-.0555	.57	3.08	11.44	7.75	.48	415.	
22.000	-9.47	13.08	-.0043	.60	2.91	13.34	9.58	.39	413.	
23.000	-12.04	13.20	.0137	.83	2.57	14.52	10.75	.32	407.	
24.000	-14.05	13.96	-.0403	.68	3.28	16.71	11.15	.24	403.	
25.000	-15.12	13.27	.0378	.31	3.07	17.13	10.90	.27	395.	
26.000	-15.03	12.87	.0736	-.37	2.53	16.76	10.90	.15	378.	
27.000	-14.35	13.51	.0013	-1.21	2.76	16.96	10.47	.11	336.	
28.000	-13.22	14.03	-.0141	-2.01	2.84	16.89	9.90	.27	320.	
29.000	-12.27	14.69	-.0044	-1.00	3.37	16.92	9.63	.30	250.	
30.000	-11.43	14.93	.0153	-1.56	3.01	16.55	9.34	.40	243.	
32.000	-9.44	16.02	.1102	.45	3.90	17.34	8.12	.15	77.	
34.000	-8.98	17.99	.1681	-.07	3.87	17.67	10.22	.23	76.	
36.000	-7.06	18.24	-.0343	-.03	3.30	16.68	10.59	.35	78.	
38.000	-3.59	14.90	.1506	.71	4.35	13.65	8.10	.83	78.	
40.000	.85	12.34	.3062	.48	4.49	10.73	7.66	1.83	78.	
42.000	1.14	12.45	.0627	.78	4.67	11.20	7.19	1.09	79.	
44.000	-.09	12.97	-.0635	-.45	5.91	12.04	7.53	.85	81.	
46.000	-2.30	13.93	-.0669	-1.47	4.83	12.80	7.67	1.00	82.	
48.000	-4.35	16.92	-.0537	-3.75	6.16	16.45	9.01	.70	83.	
50.000	-6.36	17.62	.1335	-4.32	7.11	17.58	10.52	.52	83.	
52.000	-7.22	18.50	.1163	-5.53	6.63	18.45	11.21	.72	82.	
54.000	-7.21	19.29	.0932	-6.61	6.70	18.95	12.25	.93	77.	
56.000	-6.39	19.92	.1618	-6.55	6.00	18.76	12.58	1.43	74.	
58.000	-4.18	19.62	.0858	-6.39	8.06	18.54	12.95	1.38	61.	
60.000	-3.09	21.08	-.3271	-5.23	8.31	19.03	13.38	2.14	35.	
62.000	1.53	25.73	.1046	-4.29	11.94	23.14	16.17	1.43	28.	
64.000	9.08	16.07	-.0429	-4.28	11.87	20.21	8.63	.19	19.	
66.000	11.68	13.69	.0923	3.32	13.75	20.33	9.29	.10	12.	

TABLE I-12. WIND STATISTICAL PARAMETERS

## DECEMBER

STATION = 619020		ASCENSION (WIDE AWAKE)								NOBS
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS		
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-6.64	1.81	.0740	3.63	1.50	7.73	1.53	-.26	453.	
1.000	-4.66	2.46	-.4217	1.93	2.29	5.55	2.43	.07	455.	
2.000	-4.87	3.43	-.3237	.17	2.91	5.94	2.93	.41	454.	
3.000	-5.72	3.78	-.3175	-.57	2.95	6.82	3.07	.30	454.	
4.000	-5.72	3.79	-.1042	-.77	3.10	6.85	3.20	.70	453.	
5.000	-5.45	3.70	-.1302	-.47	3.35	6.73	3.10	.65	453.	
6.000	-5.62	4.05	-.1417	-.68	3.25	7.02	3.12	.34	452.	
7.000	-4.52	4.70	-.0233	-1.28	3.46	6.96	3.39	.29	452.	
8.000	-2.97	5.93	-.0424	-1.59	4.12	7.03	3.71	.39	451.	
9.000	-.10	7.10	-.0762	-1.97	5.00	7.83	4.22	.60	450.	
10.000	2.71	7.98	-.0675	-2.66	5.78	9.30	5.00	.80	449.	
11.000	5.31	8.96	.0176	-3.64	6.33	11.19	6.17	.69	449.	
12.000	7.95	9.31	-.0103	-5.13	6.53	12.92	7.20	.49	449.	
13.000	10.39	10.07	-.0509	-5.40	6.73	14.83	7.99	.42	449.	
14.000	11.20	10.81	-.1704	-4.30	8.45	15.26	8.31	.34	448.	
15.000	8.29	10.20	-.0413	-3.19	5.95	12.93	7.13	.63	446.	
16.000	2.38	7.72	-.0763	-2.75	4.99	8.75	4.58	.72	445.	
17.000	-2.83	5.28	-.1716	-2.13	3.91	6.65	3.38	.55	430.	
18.000	-4.61	4.70	-.0476	-.69	3.11	6.43	3.49	.82	440.	
19.000	-4.06	6.15	-.0155	-.18	2.49	6.60	4.11	.74	439.	
20.000	-5.74	8.88	-.1084	.10	2.57	8.85	6.32	.64	434.	
21.000	-8.61	11.35	-.1627	.48	2.87	11.64	8.70	.46	425.	
22.000	-12.12	12.76	-.1325	1.10	3.10	14.39	10.67	.34	423.	
23.000	-14.92	12.62	-.0243	1.07	2.76	16.24	11.27	.27	419.	
24.000	-17.28	12.52	-.0235	.65	3.41	18.44	11.29	.13	416.	
25.000	-17.65	11.23	.0848	-.73	3.18	18.57	10.51	.27	409.	
26.000	-17.45	10.50	.0716	-1.45	2.57	17.95	10.05	.22	393.	
27.000	-17.07	11.37	.0453	-1.86	2.69	17.92	10.50	.24	363.	
28.000	-16.61	12.71	.0520	-1.62	2.64	18.02	11.03	.28	358.	
29.000	-17.09	14.21	.0434	-1.21	3.00	18.96	12.03	.23	277.	
30.000	-17.08	14.62	.0535	-.97	2.70	18.68	12.57	.29	208.	
32.000	-18.12	14.80	.0272	-.48	3.70	20.25	12.24	-.07	59.	
34.000	-19.16	14.37	.0333	.57	2.99	19.78	12.38	.19	59.	
36.000	-17.60	13.05	-.0822	.44	3.63	18.81	11.78	.25	59.	
38.000	-15.54	11.85	.1542	.16	4.19	16.64	11.03	.55	59.	
40.000	-16.74	12.67	.0379	.81	4.47	17.98	11.71	.38	59.	
42.000	-22.25	14.58	.1227	1.79	4.90	23.19	14.02	.70	59.	
44.000	-29.78	15.04	.1941	-.11	4.83	30.25	14.85	.58	59.	
46.000	-33.25	16.12	-.1025	-2.41	5.34	30.03	15.80	.29	59.	
48.000	-44.45	17.54	-.0569	-3.81	6.30	45.19	17.16	.74	59.	
50.000	-47.26	20.08	.0531	-5.48	6.47	40.66	18.44	.51	53.	
52.000	-43.48	20.67	.2186	-6.85	6.77	50.03	18.07	.34	53.	
54.000	-42.17	22.99	-.0213	-7.72	5.81	45.08	19.02	-.26	59.	
56.000	-32.90	25.55	.0322	-7.32	8.12	38.69	19.20	-.15	59.	
58.000	-20.45	25.45	-.0494	-7.12	8.04	26.94	18.34	.55	48.	
60.000	-12.93	24.17	-.0466	-4.83	10.15	22.97	18.46	1.39	33.	
62.000	-9.58	24.65	.1527	-4.44	12.48	23.65	17.47	1.14	23.	
64.000	-1.26	12.54	.3351	-6.45	9.47	15.26	7.15	.96	16.	
66.000	-8.23	15.04	.4519	.07	6.86	15.66	7.73	-.03	7.	

TABLE I-13. WIND STATISTICAL PARAMETERS

## ANNUAL

STATION = 619020		ASCENSION (WIDE AWAKE)								
Z	MEAN U	S.D. U	RID. V	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEN WS	N065	
KM	M/S	M/S		M/S	M/S	M/S	M/S			
.020	-6.90	1.86	.0699	3.53	1.71	8.00	1.71	-.14	5716.	
1.000	-5.45	2.77	-.3353	2.71	2.26	6.49	2.78	.03	5714.	
2.000	-3.75	4.30	-.2035	.38	2.78	5.54	3.11	.85	5710.	
3.000	-3.25	4.79	-.1774	-.75	2.65	5.75	3.12	.71	5707.	
4.000	-3.10	4.47	-.0115	-.64	2.80	5.44	3.03	.63	5706.	
5.000	-3.51	4.22	-.1301	-.49	3.03	5.55	2.95	.60	5707.	
6.000	-4.02	4.77	-.1567	-.29	3.33	6.29	3.33	.70	5710.	
7.000	-3.70	5.45	-.0603	-.18	3.81	6.75	3.52	.83	5707.	
8.000	-2.25	6.30	-.0621	-.23	4.43	7.09	3.76	.75	5693.	
9.000	-.26	7.24	-.0970	-.93	5.19	7.84	4.34	.87	5697.	
10.000	1.68	8.09	-.0215	-2.13	5.95	9.06	5.12	.88	5690.	
11.000	3.53	9.23	.0676	-3.51	6.75	10.07	6.11	.78	5665.	
12.000	5.76	9.97	.0701	-3.93	6.61	12.01	6.90	.75	5650.	
13.000	7.79	10.70	.0375	-3.72	6.49	13.19	7.59	.72	5650.	
14.000	8.71	10.81	-.0273	-2.81	6.05	13.28	7.81	.71	5653.	
15.000	6.65	9.69	-.0300	-2.00	5.30	11.21	6.69	.63	5644.	
16.000	2.13	7.40	-.0618	-1.53	4.27	7.72	4.53	1.03	5627.	
17.000	-1.65	5.69	-.0846	-.90	3.48	6.05	3.38	.81	5542.	
18.000	-2.60	6.11	-.0600	-.04	3.21	6.33	3.78	.97	5534.	
19.000	-2.03	7.09	.0051	.18	2.75	6.64	4.23	1.04	5502.	
20.000	-3.21	9.05	-.0503	.40	2.66	8.29	5.97	.62	5438.	
21.000	-5.65	11.27	-.0932	.59	2.91	10.59	7.45	.75	5314.	
22.000	-8.55	12.76	-.0517	.77	3.06	12.93	8.80	.65	5203.	
23.000	-10.73	12.65	-.0275	.73	2.69	14.24	9.26	.42	5120.	
24.000	-12.64	13.47	-.0274	.51	3.31	16.06	9.72	.35	5120.	
25.000	-13.99	13.43	-.0314	-.10	3.10	17.01	9.62	.30	5022.	
26.000	-14.02	13.73	-.0301	-.66	2.84	17.66	10.25	.22	4810.	
27.000	-15.37	14.60	-.0220	-1.16	3.09	18.49	10.90	.16	4373.	
28.000	-15.76	15.17	-.0000	-1.41	2.90	18.96	11.40	.18	4201.	
29.000	-16.67	15.80	.0000	-1.37	3.21	20.03	11.73	.14	3346.	
30.000	-18.58	15.79	.0312	-1.12	2.96	19.62	11.91	.22	3164.	
32.000	-11.22	10.29	.1003	-.23	3.65	16.69	11.27	.53	902.	
34.000	-12.45	16.09	.0102	.40	3.76	17.69	11.67	.63	902.	
36.000	-13.60	17.78	-.0045	.64	4.10	19.26	12.17	.65	902.	
38.000	-13.05	18.12	.0034	.78	4.47	20.09	13.04	.62	903.	
40.000	-12.03	21.25	.1081	1.24	5.18	21.01	14.37	.75	863.	
42.000	-12.05	24.20	.1020	1.87	5.64	22.33	16.37	1.00	864.	
44.000	-10.98	23.96	.2155	1.56	6.85	23.81	18.17	1.19	980.	
46.000	-10.37	23.02	.1915	.33	7.27	24.65	19.65	1.37	982.	
48.000	-9.24	30.39	.1403	-1.79	7.21	25.47	20.40	1.59	979.	
50.000	-5.89	23.77	.1484	-3.71	7.39	24.93	19.21	1.61	972.	
52.000	-1.36	28.01	.1033	-4.24	7.87	24.37	16.52	1.40	953.	
54.000	4.18	25.72	.1337	-3.60	8.51	23.70	14.27	.99	935.	
56.000	9.25	23.06	.1571	-2.07	9.34	23.53	13.57	.78	884.	
58.000	14.12	21.67	.1219	-.05	10.10	24.18	13.77	.70	753.	
60.000	17.91	21.49	.0903	2.09	11.02	26.25	14.37	.65	574.	
62.000	20.68	23.27	.1274	3.56	13.06	29.84	16.33	.49	428.	
64.000	22.50	20.91	.1516	3.55	13.53	30.39	15.31	.62	261.	
66.000	22.90	23.63	.1235	5.39	14.37	32.13	17.45	.48	117.	

TABLE II-1. THERMODYNAMIC STATISTICAL PARAMETERS

JANUARY

STATION - 610023 Z KM	ACCESSION (NINE ANXES)			S.D. T DEG K	SKEW T	MEAN D G/M3	S.D. D G/M3	SKEW D	NOBS P	NOBS T	NOBS D
	MEAN P MB	SKEW P	MEAN T DEG K								
0.000 1006.5000	1.2453	.03	292.75	1.27	-.22	1101.0000	8.0200	.19	460.	460.	460.
0.000 1007.0000	1.2437	.03	293.25	1.25	-.24	1159.0000	6.0620	.19	493.	493.	493.
1.000 607.5000	1.3435	.14	291.05	1.22	-.39	1074.0000	4.9730	-.28	493.	493.	493.
2.000 603.7000	1.2525	-.04	292.00	1.72	-.61	955.4000	5.6740	.53	493.	493.	493.
3.000 714.0000	1.2000	.11	293.99	1.19	-.51	873.9000	3.6070	-.32	493.	493.	493.
4.000 638.3000	1.2423	.04	277.45	1.20	-.10	753.7000	3.5270	-.02	492.	492.	492.
5.000 553.7000	1.1943	.03	273.00	1.34	-.55	714.8000	3.5320	.29	492.	492.	492.
6.000 472.7000	1.1174	.14	265.31	1.33	-.24	671.2000	3.3100	.02	492.	492.	492.
7.000 423.5000	1.1132	.12	260.04	1.33	-.70	593.3000	2.9510	.37	492.	492.	492.
8.000 379.2000	1.1107	.07	253.03	1.28	-.59	521.4000	2.9620	-.16	493.	493.	493.
9.000 330.6000	1.1026	-.03	245.47	1.33	-.34	465.1000	2.9230	-.69	493.	493.	493.
10.000 287.4000	1.1335	-.03	237.56	1.38	-.01	420.9000	2.6010	-.80	492.	492.	492.
11.000 249.6000	1.1191	-.03	229.65	1.43	.04	377.2000	1.7430	.26	492.	492.	492.
12.000 213.7700	1.0721	.01	221.55	1.29	.03	335.5000	1.5550	.02	492.	492.	492.
13.000 183.1100	1.0318	.14	214.50	1.33	.44	297.1000	1.7710	-.11	492.	492.	492.
14.000 153.9500	.9775	.33	203.05	1.50	.53	261.1000	2.0300	-.17	492.	492.	492.
15.000 132.1300	.8403	.43	202.15	1.89	.42	227.7000	2.1320	-.68	491.	491.	491.
16.000 111.5000	.7785	.39	197.71	2.02	.40	193.5000	2.0900	-.03	490.	490.	490.
17.000 93.8500	.6934	.30	195.43	2.05	-.03	167.3000	2.0550	.24	485.	485.	485.
18.000 78.0370	.6040	.29	193.52	2.60	.42	129.5000	2.0910	-.19	485.	485.	485.
19.000 65.5410	.5340	.29	200.99	2.67	.28	115.3000	1.6350	.04	483.	483.	483.
20.000 55.3470	.4627	.34	205.63	2.59	.09	95.4500	1.1750	.31	479.	479.	479.
21.000 47.6350	.4522	.40	203.47	2.43	.23	79.6100	.8401	.39	472.	472.	472.
22.000 40.7250	.4222	.44	216.39	2.28	.27	66.9700	.6930	.09	470.	470.	470.
23.000 34.9070	.3826	.49	214.49	2.07	.32	56.5300	.5930	.11	464.	464.	464.
24.000 29.7430	.3522	.40	215.40	2.35	.18	47.5000	.6294	.03	458.	458.	458.
25.000 25.4610	.3187	.37	210.51	2.53	.21	40.3500	.5993	.12	454.	454.	454.
26.000 21.2340	.2634	.22	221.66	2.61	.06	34.4100	.5331	.34	440.	440.	440.
27.000 18.7500	.2434	.03	223.04	2.62	-.02	29.2200	.4593	.27	414.	414.	414.
28.000 16.1420	.2231	-.02	223.07	2.55	-.10	24.8000	.4008	.18	410.	410.	410.
29.000 13.6340	.1933	-.10	222.44	2.63	-.18	21.2400	.3541	.28	347.	347.	347.
30.000 12.3210	.1733	-.10	220.49	2.58	-.35	18.1700	.2924	.17	339.	339.	339.
32.000 8.9772	.1303	-.23	233.67	3.23	.14	13.2500	.2104	.04	75.	75.	75.
34.000 6.7321	.1125	-.02	233.54	3.65	.04	9.9000	.1551	-.15	75.	75.	75.
36.000 5.6229	.0959	.13	241.15	4.20	.24	7.3400	.1281	-.36	75.	75.	75.
38.000 3.8355	.0651	.10	245.53	5.03	.18	5.4490	.1010	-.02	73.	73.	73.
40.000 2.9459	.0755	.07	252.14	5.25	-.27	4.0550	.0569	-.24	73.	73.	73.
42.000 2.6373	.0637	-.05	250.65	5.28	-.03	3.0780	.0704	.15	73.	73.	73.
44.000 1.7538	.0562	-.23	253.53	4.68	-.61	2.3040	.0595	.40	72.	72.	72.
46.000 1.3553	.0476	-.34	257.15	4.65	-.51	1.7770	.0493	.15	71.	71.	71.
48.000 1.0312	.0405	-.39	253.29	5.62	-.13	1.3760	.0447	-.08	69.	69.	69.
50.000 .9807	.0379	-.51	243.24	6.17	.42	1.0590	.0373	-.19	68.	68.	68.
52.000 .8454	.0374	-.14	270.03	6.17	.56	.8313	.0334	-.52	67.	67.	67.
54.000 .6035	.0225	-.20	263.21	6.04	.13	.6510	.0271	-.27	64.	64.	64.
56.000 .3623	.0189	-.19	267.66	6.57	.10	.5100	.0222	-.39	61.	61.	61.
58.000 .3245	.0160	.07	267.31	7.15	.25	.4213	.0181	-.47	56.	56.	56.
60.000 .2351	.0119	.22	259.26	8.30	.34	.3159	.0135	-.16	49.	49.	49.
62.000 .1501	.0037	.40	254.50	8.63	.63	.2453	.0101	-.07	37.	37.	37.
64.000 .1375	.0031	.50	249.20	9.42	1.22	.1913	.0067	-.15	29.	29.	29.
66.000 .1056	.0010	.50	233.21	10.10	1.65	.1523	.0033	-.87	10.	10.	10.

TABLE II-2. THERMODYNAMIC STATISTICAL PARAMETERS

## FEBRUARY

STATION = 619020										ASCENSION (HIDE APKE)										S.D. T		SKEW T		MEAN D		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	MEAN P	S.D. P	SKEW P	MEAN T	S.D. T	SKEW T	MEAN D	S.D. D	SKEW D	NOBS P	NOBS T	NOBS D																							
KN	PS	PS	PS	DEG K	DEG K	DEG K	G/M3	G/M3	G/M3																										
0.000	1006.3030	1.7199	.17	330.20	1.16	-.26	1157.0030	5.9330	.30	424.	424.	424.																							
0.050	1004.0030	1.7084	.17	331.19	1.15	-.24	1134.0030	5.9310	.29	446.	446.	446.																							
1.000	903.6300	1.4936	.18	331.05	1.13	-.20	1071.0030	4.7020	-.27	450.	450.	450.																							
2.000	804.0600	1.3612	.26	330.10	1.50	-.49	655.4030	5.0730	.32	449.	449.	449.																							
3.000	714.2700	1.3030	.43	333.59	1.27	-.07	875.0030	3.9163	.04	449.	449.	449.																							
4.000	632.7500	1.2679	.43	377.53	1.35	-.13	732.5030	3.7010	.02	449.	449.	449.																							
5.000	573.2100	1.2535	.53	372.40	1.37	-.24	714.2030	3.1030	-.02	449.	449.	449.																							
6.000	423.2500	1.2031	.52	300.30	1.44	-.15	642.0030	2.2410	.03	448.	448.	448.																							
7.000	433.3500	1.2537	.45	293.30	1.37	-.04	579.0030	2.0030	.02	448.	448.	448.																							
8.000	379.6300	1.3102	.33	293.73	1.31	.07	500.0030	2.4403	-.03	448.	448.	448.																							
9.000	331.3500	1.3042	.35	293.13	1.33	-.17	468.4030	2.3550	-.18	449.	449.	449.																							
10.000	230.0000	1.3110	.33	293.15	1.34	-.41	420.8030	2.1630	-.31	449.	449.	449.																							
11.000	245.2500	1.2524	.22	293.18	1.42	-.25	377.2030	1.5630	.27	448.	448.	448.																							
12.000	214.3030	1.2523	.28	292.33	1.44	.30	335.0030	1.5150	.02	449.	449.	449.																							
13.000	183.6000	1.2091	.24	214.67	1.50	.73	237.7030	1.0030	-.75	449.	449.	449.																							
14.000	156.3500	1.1375	.30	207.03	1.58	.22	200.0030	1.5000	-.25	449.	449.	449.																							
15.000	132.4500	1.0597	.51	231.93	1.84	.33	205.3030	1.5230	-.52	448.	448.	448.																							
16.000	111.7800	.9761	.55	197.95	1.65	.11	197.1030	1.5220	-.23	448.	448.	448.																							
17.000	94.0910	.8716	.57	153.35	1.54	.56	157.8500	2.1230	-.09	445.	445.	445.																							
18.000	79.1030	.7425	.54	159.50	2.73	.32	140.3030	2.4090	.21	442.	442.	442.																							
19.000	65.7050	.6259	.50	200.78	2.73	.31	115.8030	1.8420	.42	441.	441.	441.																							
20.000	56.4690	.5552	.37	225.14	2.25	.25	95.9000	1.3475	.44	438.	438.	438.																							
21.000	47.6420	.5224	.33	219.07	2.76	.61	79.6200	1.0100	.40	421.	421.	421.																							
22.000	40.6220	.4478	.37	212.14	2.49	.12	67.0030	.7847	.29	419.	419.	419.																							
23.000	34.6450	.4103	.38	214.52	2.34	.43	56.5030	.5651	-.17	411.	411.	411.																							
24.000	29.7770	.3524	.31	218.23	2.91	.33	40.0030	.0523	.00	397.	397.	397.																							
25.000	25.4250	.3230	.01	221.51	2.78	.21	34.3500	.5491	.21	385.	385.	385.																							
26.000	21.8040	.2834	-.10	224.13	2.72	.15	29.2030	.4863	.23	348.	348.	348.																							
27.000	18.7550	.2541	-.16	220.64	2.71	.05	24.6500	.4334	.05	339.	339.	339.																							
28.000	16.1750	.2168	-.13	220.30	2.71	.05	21.2030	.3578	.11	280.	280.	280.																							
29.000	13.9330	.1521	-.20	221.11	3.65	.09	18.1700	.3094	.21	275.	275.	275.																							
30.000	12.0520	.1506	.12	224.31	3.65	.24	13.4200	.1812	.29	68.	68.	68.																							
32.000	9.0410	.1534	.10	223.23	3.77	.73	9.5400	.1400	-.35	66.	66.	66.																							
34.000	5.7550	.1126	.24	212.07	4.10	-.24	7.3630	.1618	-.30	66.	66.	66.																							
35.000	5.1313	.0942	.19	220.07	4.57	-.22	5.4420	.1189	-.17	66.	66.	66.																							
40.000	2.9257	.0303	.01	227.29	5.28	-.57	4.0560	.0335	.40	66.	66.	66.																							
42.000	2.3156	.0099	-.13	225.11	6.17	-.25	3.0320	.0714	-.09	64.	64.	64.																							
44.000	1.6520	.0315	-.14	270.13	3.57	.19	2.3320	.0535	.04	66.	66.	66.																							
46.000	1.4075	.0315	-.14	272.49	5.63	.09	1.7390	.0574	-.02	68.	68.	68.																							
48.000	1.1021	.0441	.07	272.51	4.75	.19	1.4050	.0557	-.03	69.	69.	69.																							
50.000	.8523	.0316	.11	271.21	4.73	.93	1.1040	.0490	.06	68.	68.	68.																							
52.000	.6707	.0206	.15	229.29	5.67	-.23	.8701	.0401	.32	67.	67.	67.																							
54.000	.5224	.0212	.06	223.23	6.35	.09	.6322	.0285	.52	69.	69.	69.																							
56.000	.4064	.0175	.01	224.24	7.25	-.64	.5353	.0227	1.10	66.	66.	66.																							
58.000	.3147	.0145	.03	221.23	6.33	-.25	.4135	.0160	-.03	63.	63.	63.																							
60.000	.2418	.0121	.13	227.50	10.10	-.11	.3275	.0129	-.01	55.	55.	55.																							
62.000	.1825	.0111	.13	225.14	11.10	-.07	.2549	.0088	.01	46.	46.	46.																							
64.000	.1414	.0093	.16	250.41	11.26	.26	.1537	.0070	-.09	28.	28.	28.																							
67.000	.1044	.0078	1.22	222.21	12.16	1.13	.1510	.0039	-.41	11.	11.	11.																							

TABLE II-3. THERMODYNAMIC STATISTICAL PARAMETERS

## MARCH

STATION = 816020	ASLENSION (INDC AMPL)		S.D. T		SKEW T		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	MEAN P	MEAN T	S.D. P	SKEW P	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K
KH	MB	MB	MB	MB	MB	MB	MB	MB	MB	MB	MB	MB	MB	MB	MB	MB
.000	1006.0000	300.98	1.4761	.23	300.98	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08
.020	1003.7000	300.65	1.4762	.24	300.65	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08
1.000	903.5300	232.51	1.3331	.16	232.51	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33
2.000	804.1500	135.75	1.2235	.23	135.75	1.32	1.32	1.32	1.32	1.32	1.32	1.32	1.32	1.32	1.32	1.32
3.000	714.3200	233.67	1.2331	.23	233.67	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15
4.000	632.6900	277.55	1.2037	.13	277.55	1.13	1.13	1.13	1.13	1.13	1.13	1.13	1.13	1.13	1.13	1.13
5.000	558.4100	272.55	1.1232	.26	272.55	1.22	1.22	1.22	1.22	1.22	1.22	1.22	1.22	1.22	1.22	1.22
6.000	493.2800	1.0919	1.0519	.28	257.84	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15
7.000	433.6000	257.84	1.0528	.37	257.84	1.09	1.09	1.09	1.09	1.09	1.09	1.09	1.09	1.09	1.09	1.09
8.000	379.6300	254.10	1.2474	.53	254.10	1.14	1.14	1.14	1.14	1.14	1.14	1.14	1.14	1.14	1.14	1.14
9.000	331.7400	245.83	1.0375	.51	245.83	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21
10.000	293.4500	245.82	1.0316	.40	245.82	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25
11.000	249.7300	230.24	1.2472	.30	230.24	1.27	1.27	1.27	1.27	1.27	1.27	1.27	1.27	1.27	1.27	1.27
12.000	214.6000	232.78	1.0335	.39	232.78	1.23	1.23	1.23	1.23	1.23	1.23	1.23	1.23	1.23	1.23	1.23
13.000	194.0700	214.91	.9319	.37	214.91	1.26	1.26	1.26	1.26	1.26	1.26	1.26	1.26	1.26	1.26	1.26
14.000	153.7600	207.60	.9436	.44	207.60	1.40	1.40	1.40	1.40	1.40	1.40	1.40	1.40	1.40	1.40	1.40
15.000	132.7600	201.49	.8761	.45	201.49	1.58	1.58	1.58	1.58	1.58	1.58	1.58	1.58	1.58	1.58	1.58
16.000	111.5600	197.00	.8025	.47	197.00	1.59	1.59	1.59	1.59	1.59	1.59	1.59	1.59	1.59	1.59	1.59
17.000	84.1000	194.85	.7657	.49	194.85	1.67	1.67	1.67	1.67	1.67	1.67	1.67	1.67	1.67	1.67	1.67
18.000	70.1700	193.57	.5304	.53	193.57	2.84	2.84	2.84	2.84	2.84	2.84	2.84	2.84	2.84	2.84	2.84
19.000	66.7710	201.72	.4817	.57	201.72	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56
20.000	56.5310	205.60	.4463	.42	205.60	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46
21.000	48.0420	203.60	.4120	.23	203.60	2.23	2.23	2.23	2.23	2.23	2.23	2.23	2.23	2.23	2.23	2.23
22.000	40.9300	213.11	.3839	.22	213.11	2.14	2.14	2.14	2.14	2.14	2.14	2.14	2.14	2.14	2.14	2.14
23.000	34.9750	215.72	.3366	.21	215.72	1.88	1.88	1.88	1.88	1.88	1.88	1.88	1.88	1.88	1.88	1.88
24.000	29.8110	218.19	.3043	.14	218.19	2.32	2.32	2.32	2.32	2.32	2.32	2.32	2.32	2.32	2.32	2.32
25.000	25.6330	220.39	.2687	.06	220.39	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55
26.000	22.0170	222.31	.2332	.01	222.31	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
27.000	18.5200	222.22	.2046	.02	222.22	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47
28.000	16.3040	227.75	.1823	.05	227.75	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46	2.46
29.000	14.0760	230.10	.1620	.09	230.10	2.59	2.59	2.59	2.59	2.59	2.59	2.59	2.59	2.59	2.59	2.59
30.000	12.1670	232.10	.1459	.10	232.10	2.44	2.44	2.44	2.44	2.44	2.44	2.44	2.44	2.44	2.44	2.44
31.000	9.0755	235.59	.1458	.46	235.59	3.78	3.78	3.78	3.78	3.78	3.78	3.78	3.78	3.78	3.78	3.78
32.000	8.6342	239.61	.1275	.48	239.61	4.24	4.24	4.24	4.24	4.24	4.24	4.24	4.24	4.24	4.24	4.24
33.000	5.1731	244.60	.1139	.37	244.60	4.61	4.61	4.61	4.61	4.61	4.61	4.61	4.61	4.61	4.61	4.61
34.000	3.9453	251.60	.0926	.30	251.60	5.53	5.53	5.53	5.53	5.53	5.53	5.53	5.53	5.53	5.53	5.53
35.000	3.0341	259.73	.0674	.24	259.73	6.12	6.12	6.12	6.12	6.12	6.12	6.12	6.12	6.12	6.12	6.12
36.000	2.5515	256.33	.0775	.23	256.33	5.02	5.02	5.02	5.02	5.02	5.02	5.02	5.02	5.02	5.02	5.02
37.000	1.8322	270.61	.0620	.43	270.61	5.42	5.42	5.42	5.42	5.42	5.42	5.42	5.42	5.42	5.42	5.42
38.000	1.4305	272.11	.0530	.55	272.11	4.81	4.81	4.81	4.81	4.81	4.81	4.81	4.81	4.81	4.81	4.81
39.000	1.1185	271.27	.0428	.61	271.27	4.78	4.78	4.78	4.78	4.78	4.78	4.78	4.78	4.78	4.78	4.78
40.000	.8716	259.31	.0243	.63	259.31	5.35	5.35	5.35	5.35	5.35	5.35	5.35	5.35	5.35	5.35	5.35
41.000	.6790	265.52	.0277	.62	265.52	5.68	5.68	5.68	5.68	5.68	5.68	5.68	5.68	5.68	5.68	5.68
42.000	.5273	264.20	.0225	.57	264.20	6.52	6.52	6.52	6.52	6.52	6.52	6.52	6.52	6.52	6.52	6.52
43.000	.4003	251.43	.0184	.42	251.43	7.01	7.01	7.01	7.01	7.01	7.01	7.01	7.01	7.01	7.01	7.01
44.000	.3150	257.57	.0155	.42	257.57	7.08	7.08	7.08	7.08	7.08	7.08	7.08	7.08	7.08	7.08	7.08
45.000	.2417	254.07	.0131	.43	254.07	7.23	7.23	7.23	7.23	7.23	7.23	7.23	7.23	7.23	7.23	7.23
46.000	.1879	249.57	.0091	.27	249.57	8.71	8.71	8.71	8.71	8.71	8.71	8.71	8.71	8.71	8.71	8.71
47.000	.1360	242.40	.0032	.63	242.40	7.25	7.25	7.25	7.25	7.25	7.25	7.25	7.25	7.25	7.25	7.25
48.000	.1041	237.63	.0067	1.64	237.63	8.58	8.58	8.58	8.58	8.58	8.58	8.58	8.58	8.58	8.58	8.58



TABLE II-4. THERMODYNAMIC STATISTICAL PARAMETERS

## APRIL

STATION - 819020	MEAN P	MEAN T	S.D. T	SKEW T	MEAN D	S.D. D	SKEW D	NOBS P	NOBS T	NOBS D
Z	MB	DEG K	DEG K		G/M3	G/M3				
1.000	1006.1000	301.03	1.17	-.73	1153.0000	5.6200	.57	422.	422.	422.
.020	1003.8000	300.93	1.17	-.66	1151.0000	5.6200	.53	448.	448.	448.
1.000	903.7200	292.50	1.02	-.14	1059.0000	4.2410	-.10	459.	459.	459.
2.000	804.2400	263.62	1.48	-.16	622.6000	4.7200	.03	459.	459.	459.
3.000	714.4200	234.03	1.11	-.47	373.7000	3.6350	-.07	459.	459.	459.
4.000	633.0700	278.42	1.07	-.03	712.6000	3.1600	-.32	459.	459.	459.
5.000	559.6500	257.25	1.18	-.24	642.2000	2.9370	-.15	459.	459.	459.
6.000	493.5700	231.18	1.15	-.14	577.7000	2.6040	-.42	459.	459.	459.
7.000	433.9100	204.67	1.03	-.12	519.3000	2.5130	-.69	457.	457.	457.
8.000	380.3300	184.71	1.12	.01	456.5000	2.7760	-.78	457.	457.	457.
9.000	332.1500	161.52	1.12	.01	410.3000	2.8490	-.10	455.	455.	455.
10.000	289.9400	139.54	1.21	-.16	376.0000	1.6510	-.94	454.	454.	454.
11.000	250.2700	123.53	1.14	-.14	336.6000	1.1850	.20	455.	455.	455.
12.000	215.3200	105.34	1.17	-.16	299.7000	1.0970	-.21	455.	455.	455.
13.000	184.6100	87.71	1.31	-.05	253.7000	1.1040	.31	455.	455.	455.
14.000	157.2400	70.71	1.44	.17	230.7000	1.4500	-.27	453.	453.	453.
15.000	133.1600	50.63	1.51	.23	193.3000	1.9500	-.18	453.	453.	453.
16.000	112.2400	35.23	1.70	.32	163.3000	1.9530	-.03	449.	449.	449.
17.000	94.3750	19.15	2.72	.10	140.6000	2.3160	.24	448.	448.	448.
18.000	79.2630	15.54	2.74	-.25	115.5000	1.8290	.28	445.	445.	445.
19.000	66.0370	10.77	2.83	-.20	95.8000	1.1850	.24	443.	443.	443.
20.000	53.6270	8.49	2.24	.14	79.7100	1.0000	.17	432.	432.	432.
21.000	43.1630	6.63	2.29	.23	66.6000	1.6003	-.05	432.	432.	432.
22.000	35.1470	4.44	2.08	.23	55.3500	1.6544	.00	424.	424.	424.
23.000	30.0310	2.99	2.41	.46	47.6000	1.6413	-.06	419.	419.	419.
24.000	25.8720	2.42	2.52	.23	40.4400	1.5504	.18	412.	412.	412.
25.000	22.2100	1.77	2.42	-.04	34.4400	1.4521	.48	404.	404.	404.
26.000	19.1130	1.63	2.47	-.13	29.3500	1.3622	.37	373.	373.	373.
27.000	16.4250	1.63	2.65	-.17	25.0000	1.3073	.47	351.	351.	351.
28.000	14.2550	1.56	2.19	-.10	21.4400	1.2605	.30	275.	275.	275.
29.000	12.3260	1.47	2.04	-.23	18.4000	1.2175	.18	268.	268.	268.
30.000	10.2019	1.35	3.35	.01	13.5300	1.2540	.45	75.	75.	75.
31.000	8.9426	1.22	3.81	-.41	9.9200	1.1810	.17	75.	75.	75.
32.000	7.2700	1.03	4.32	-.11	7.4070	1.1212	-.51	75.	75.	75.
33.000	5.4037	0.83	4.39	-.55	5.5240	1.0144	-.07	75.	75.	75.
34.000	3.0037	0.63	4.60	-.41	4.1420	1.0000	.02	75.	75.	75.
35.000	2.4033	0.53	4.62	-.05	3.1230	1.0559	-.05	75.	75.	75.
36.000	1.8734	0.43	4.24	-.11	2.4133	1.0519	-.41	75.	75.	75.
37.000	1.4532	0.33	3.46	-.26	1.8760	1.0519	-.39	75.	75.	75.
38.000	1.1235	0.23	3.56	-.74	1.4530	1.0426	.05	75.	75.	75.
39.000	.8337	0.13	3.53	-.58	1.1530	1.0300	.03	74.	74.	74.
40.000	.6815	0.08	4.08	-.58	.9062	1.0280	.00	74.	74.	74.
41.000	.5565	0.07	5.19	-.14	.7109	1.0215	-.26	73.	73.	73.
42.000	.4153	0.07	6.29	.05	.5373	1.0133	-.05	70.	70.	70.
43.000	.3123	0.07	7.33	.07	.4355	1.0123	-.20	65.	65.	65.
44.000	.2445	0.07	7.33	.25	.3361	1.0106	-.23	61.	61.	61.
45.000	.1932	0.07	7.93	.25	.2361	1.0079	-.79	51.	51.	51.
46.000	.1373	0.07	7.33	.63	.1373	1.0032	-.11	27.	27.	27.
47.000	.1057	0.07	12.15	.93	.1549	1.0033	-.59	10.	10.	10.

TABLE II-5. THERMODYNAMIC STATISTICAL PARAMETERS

MAY

STATION = 619020				ASCENSION (LIDE ANGLE)				S.D. T		SKEW T		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	MEAN P	S.D. P	SKEW P	MEAN T	DEG K	DEG K	MEAN D	G/M3	G/M3	MEAN D	G/M3	MEAN D	G/M3	MEAN D	G/M3	MEAN D	G/M3	MEAN D	G/M3	MEAN D	G/M3
.000	1007.4000	1.4250	.18	377.52	1.05	-.28	1157.0000	4.4240	.14	412.	412.	412.	412.	412.	412.	412.	412.	412.	412.	412.	412.
.020	1005.2000	1.3339	.12	303.43	.958	-.17	1153.0000	4.2510	.03	409.	409.	409.	409.	409.	409.	409.	409.	409.	409.	409.	409.
1.030	504.5500	1.2448	.27	291.75	1.01	-.03	1073.0000	4.2540	-.03	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.
2.000	644.7300	1.1648	.24	233.03	1.75	-.27	913.0000	5.6230	.30	453.	453.	453.	453.	453.	453.	453.	453.	453.	453.	453.	453.
3.000	714.6300	1.1253	.32	224.03	1.36	-.58	874.1000	4.6410	-.07	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.
4.000	533.3100	1.1210	.25	272.59	1.17	-.20	750.1000	3.9550	-.06	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.
5.000	523.3000	1.0333	.15	272.59	1.18	-.13	713.0000	3.7150	-.08	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.	488.
6.000	493.7400	1.0352	.10	267.10	1.24	-.08	612.4000	3.4630	-.45	469.	469.	469.	469.	469.	469.	469.	469.	469.	469.	469.	469.
7.000	434.0300	1.0342	.24	261.06	1.17	-.06	577.9000	3.1610	-.60	468.	468.	468.	468.	468.	468.	468.	468.	468.	468.	468.	468.
8.000	380.4400	1.0349	.16	224.53	1.16	-.03	519.3000	3.0310	-.85	456.	456.	456.	456.	456.	456.	456.	456.	456.	456.	456.	456.
9.000	332.2400	1.0872	.18	247.45	1.24	-.14	456.0000	3.1520	-.86	486.	486.	486.	486.	486.	486.	486.	486.	486.	486.	486.	486.
10.000	293.0000	1.1152	.17	239.51	1.21	-.02	419.3000	2.9180	-.10	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.
11.000	250.3000	1.0858	.14	231.37	1.18	-.07	376.0000	1.6930	-.09	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.
12.000	215.3500	1.0934	.19	225.25	1.21	-.09	335.0000	1.3010	-.07	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.	485.
13.000	184.6100	1.0103	.22	215.29	1.26	.07	255.7000	1.2580	-.50	484.	484.	484.	484.	484.	484.	484.	484.	484.	484.	484.	484.
14.000	157.2500	.9352	.27	267.76	1.20	.34	223.7000	1.3130	-.55	483.	483.	483.	483.	483.	483.	483.	483.	483.	483.	483.	483.
15.000	133.2000	.9073	.24	201.51	1.51	.27	259.3000	1.5360	-.10	482.	482.	482.	482.	482.	482.	482.	482.	482.	482.	482.	482.
16.000	112.3300	.9539	.29	195.96	1.54	-.06	199.7000	1.6580	.03	482.	482.	482.	482.	482.	482.	482.	482.	482.	482.	482.	482.
17.000	94.5550	.7755	.33	195.28	1.81	.28	160.7000	2.6220	.00	475.	475.	475.	475.	475.	475.	475.	475.	475.	475.	475.	475.
18.000	79.5040	.6763	.25	158.01	2.60	-.01	139.0000	2.1800	.16	474.	474.	474.	474.	474.	474.	474.	474.	474.	474.	474.	474.
19.000	67.1680	.6105	.80	202.79	2.31	-.05	115.4000	1.6660	.33	456.	456.	456.	456.	456.	456.	456.	456.	456.	456.	456.	456.
20.000	55.9460	.5520	.62	207.50	2.20	.10	95.6200	1.2650	.52	469.	469.	469.	469.	469.	469.	469.	469.	469.	469.	469.	469.
21.000	48.4440	.4738	.53	211.53	2.17	.06	79.7700	.9371	.28	449.	449.	449.	449.	449.	449.	449.	449.	449.	449.	449.	449.
22.000	41.3410	.4048	.61	215.07	2.05	-.06	63.6700	.8340	.58	448.	448.	448.	448.	448.	448.	448.	448.	448.	448.	448.	448.
23.000	35.3730	.3434	.63	217.90	1.94	-.01	55.5500	.6559	.40	448.	448.	448.	448.	448.	448.	448.	448.	448.	448.	448.	448.
24.000	29.4000	.3043	.55	220.57	2.19	.15	47.5000	.6492	.29	431.	431.	431.	431.	431.	431.	431.	431.	431.	431.	431.	431.
25.000	23.3200	.2733	.43	223.29	2.11	.10	40.5000	.5405	.08	401.	401.	401.	401.	401.	401.	401.	401.	401.	401.	401.	401.
26.000	18.3820	.2243	.14	225.55	2.10	.00	34.5300	.4071	.22	395.	395.	395.	395.	395.	395.	395.	395.	395.	395.	395.	395.
27.000	18.6930	.1943	.00	227.59	2.15	.33	29.5200	.3409	.18	335.	335.	335.	335.	335.	335.	335.	335.	335.	335.	335.	335.
28.000	16.6330	.1740	-.12	229.42	1.63	.31	25.6000	.2732	.05	332.	332.	332.	332.	332.	332.	332.	332.	332.	332.	332.	332.
29.000	14.3530	.1573	-.09	231.08	1.79	.17	21.6500	.2603	.09	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.
30.000	12.4240	.1322	-.07	232.05	1.95	-.24	18.5000	.2355	.17	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.
31.000	9.3100	.1061	.65	233.13	4.13	.10	13.6000	.1707	.17	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.
32.000	7.8400	.0871	.73	234.19	4.19	.02	10.1100	.1473	.11	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.	04.
33.000	5.3523	.0711	.55	236.73	3.75	-.02	7.5200	.1193	.56	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.
34.000	4.1033	.0532	.41	234.54	4.20	-.08	5.6140	.0915	.42	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.
35.000	3.1580	.0759	.33	259.54	3.68	.03	4.2300	.0370	.51	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.
36.000	2.4433	.0627	.26	254.46	3.68	-.18	3.2190	.0756	.38	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.
37.000	1.8522	.0511	.18	267.04	3.97	.37	2.4710	.0218	.34	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.	63.
38.000	1.4419	.0419	.17	269.45	4.21	1.08	1.9110	.0523	.34	61.	61.	61.	61.	61.	61.	61.	61.	61.	61.	61.	61.
39.000	1.1477	.0341	.20	270.60	4.45	.43	1.6100	.0418	.25	59.	59.	59.	59.	59.	59.	59.	59.	59.	59.	59.	59.
40.000	.8990	.0275	.24	263.05	5.26	.62	1.1500	.0324	.09	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.
41.000	.6596	.0232	.27	255.77	5.51	.28	.9156	.0231	.53	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.
42.000	.5429	.0197	.32	263.33	6.34	.09	7.193	.0213	.23	64.	64.	64.	64.	64.	64.	64.	64.	64.	64.	64.	64.
43.000	.4185	.0171	.56	259.31	6.49	.27	.5324	.0165	.07	58.	58.	58.	58.	58.	58.	58.	58.	58.	58.	58.	58.
44.000	.3234	.0144	.34	253.11	7.23	.29	.4417	.0155	.14	57.	57.	57.	57.	57.	57.	57.	57.	57.	57.	57.	57.
45.000	.2473	.0123	.62	250.69	8.09	.11	.3442	.0125	.49	56.	56.	56.	56.	56.	56.	56.	56.	56.	56.	56.	56.
46.000	.1637	.0104	-.16	245.24	9.72	.15	.2677	.0106	.05	35.	35.	35.	35.	35.	35.	35.	35.	35.	35.	35.	35.
47.000	.1437	.0077	.32	270.95	9.01	.89	.2103	.0078	-.33	12.	12.	12.	12.	12.	12.	12.	12.	12.	12.	12.	12.
48.000	.0979	.0030	.90	269.00	23.99	59.53	.9353	.0020	99.53	4.	4.	4.	4.	4.	4.	4.	4.	4.	4.	4.	4.

TABLE II-6. THERMODYNAMIC STATISTICAL PARAMETERS

JUNE

STATION = 615020		ASCENSION (WILE ANAKE)				S.D. T		SKEW T		MEAN D		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	RA	MEAN P	S.D. P	SKEW P	MEAN T	DEG K	DEG K			C/MS	O/MZ	O/MZ									
.000	1009.1000	1.6373	.01	.01	209.50	1.11	1.11	-.51	1164.0000	5.2530	.60	368.	368.	.60	368.	368.	368.	368.	368.	368.	
.020	1006.6000	1.6303	.01	.01	209.44	1.09	1.09	-.49	1164.0000	5.1320	.19	426.	426.	.19	426.	426.	426.	426.	426.	426.	
1.000	905.0100	1.4534	.23	.23	209.05	1.05	1.05	.12	1079.0000	4.4400	.04	447.	447.	.04	447.	447.	447.	447.	447.	447.	
2.000	805.2600	1.4449	-.13	-.13	209.46	2.03	2.03	.05	975.5000	7.0320	-.03	447.	447.	-.03	447.	447.	447.	447.	447.	447.	
3.000	714.6500	1.3693	-.23	-.23	203.75	1.42	1.42	-.39	875.7000	4.7760	.25	447.	447.	.25	447.	447.	447.	447.	447.	447.	
4.000	633.3400	1.3375	-.03	-.03	277.02	1.30	1.30	.17	792.3000	4.2700	-.05	447.	447.	-.05	447.	447.	447.	447.	447.	447.	
5.000	559.7300	1.2518	.04	.04	272.20	1.26	1.26	-.22	715.1000	3.0740	.20	447.	447.	.20	447.	447.	447.	447.	447.	447.	
6.000	493.4100	1.2593	.20	.20	269.62	1.41	1.41	-.25	643.6000	3.5320	.41	447.	447.	.41	447.	447.	447.	447.	447.	447.	
7.000	433.6400	1.2593	.49	.49	269.05	1.47	1.47	.05	570.7000	3.2370	.63	447.	447.	.63	447.	447.	447.	447.	447.	447.	
8.000	379.5000	1.2765	.53	.53	269.60	1.35	1.35	.37	530.3000	3.1350	-.47	447.	447.	-.47	447.	447.	447.	447.	447.	447.	
9.000	331.6800	1.2646	.75	.75	246.50	1.40	1.40	.43	457.6000	3.2290	-1.00	444.	444.	-1.00	444.	444.	444.	444.	444.	444.	
10.000	288.3400	1.2679	.81	.81	245.38	1.42	1.42	.39	400.6000	2.9140	-1.33	444.	444.	-1.33	444.	444.	444.	444.	444.	444.	
11.000	245.5200	1.2403	.72	.72	230.24	1.49	1.49	.34	377.5000	1.7050	-.31	444.	444.	-.31	444.	444.	444.	444.	444.	444.	
12.000	214.5500	1.2318	.77	.77	222.25	1.40	1.40	.35	336.5000	1.5510	-.17	443.	443.	-.17	443.	443.	443.	443.	443.	443.	
13.000	183.8100	1.1753	.72	.72	214.56	1.30	1.30	.72	298.4000	1.5550	-.37	442.	442.	-.37	442.	442.	442.	442.	442.	442.	
14.000	155.5200	1.1072	.81	.81	207.53	1.48	1.48	.72	263.6000	1.0700	-.22	442.	442.	-.22	442.	442.	442.	442.	442.	442.	
15.000	132.6000	1.0141	.84	.84	202.03	1.61	1.61	.27	230.6000	1.9770	.01	439.	439.	.01	439.	439.	439.	439.	439.	439.	
16.000	111.5200	.9162	1.00	1.00	193.41	1.76	1.76	.27	190.5000	2.1130	.69	439.	439.	.69	439.	439.	439.	439.	439.	439.	
17.000	94.3120	.8115	1.09	1.09	197.45	2.05	2.05	-.05	160.4000	2.2370	.21	434.	434.	.21	434.	434.	434.	434.	434.	434.	
18.000	79.4040	.6355	1.08	1.08	200.35	2.67	2.67	-.03	133.3000	2.2320	.48	432.	432.	.48	432.	432.	432.	432.	432.	432.	
19.000	67.2670	.5837	.94	.94	203.01	2.41	2.41	.04	114.3000	1.7310	.98	431.	431.	.98	431.	431.	431.	431.	431.	431.	
20.000	57.1340	.4756	.75	.75	203.41	2.21	2.21	.03	95.0000	1.3420	.63	428.	428.	.63	428.	428.	428.	428.	428.	428.	
21.000	48.6620	.3523	.57	.57	212.74	2.26	2.26	-.04	79.7000	1.1500	.73	416.	416.	.73	416.	416.	416.	416.	416.	416.	
22.000	41.5330	.3302	.54	.54	215.62	1.36	1.36	-.15	67.1400	.9212	.60	412.	412.	.60	412.	412.	412.	412.	412.	412.	
23.000	35.5310	.2536	.23	.23	213.64	1.99	1.99	-.04	55.6200	.6714	.65	407.	407.	.65	407.	407.	407.	407.	407.	407.	
24.000	30.4610	.2074	.19	.19	200.65	2.27	2.27	.30	40.1000	.5313	.25	405.	405.	.25	405.	405.	405.	405.	405.	405.	
25.000	25.1020	.2548	.01	.01	223.09	2.21	2.21	.29	40.5500	.4740	.49	402.	402.	.49	402.	402.	402.	402.	402.	402.	
26.000	22.5000	.2112	-.13	-.13	225.17	2.09	2.09	.03	34.9100	.3757	.63	395.	395.	.63	395.	395.	395.	395.	395.	395.	
27.000	19.3730	.1833	-.28	-.28	227.09	2.19	2.19	.31	29.7200	.3335	.11	360.	360.	.11	360.	360.	360.	360.	360.	360.	
28.000	16.7050	.1702	-.34	-.34	227.66	1.68	1.68	.34	25.4600	.2735	.14	349.	349.	.14	349.	349.	349.	349.	349.	349.	
29.000	14.4260	.1537	-.10	-.10	229.66	2.18	2.18	-.41	21.0500	.2735	.16	294.	294.	.16	294.	294.	294.	294.	294.	294.	
30.000	12.4680	.1373	.04	.04	233.00	2.11	2.11	-.16	18.7200	.2354	-.04	287.	287.	-.04	287.	287.	287.	287.	287.	287.	
32.000	9.3457	.1207	.93	.93	237.14	3.63	3.63	-.13	13.7400	.2332	.16	55.	55.	.16	55.	55.	55.	55.	55.	55.	
34.000	7.7743	.1073	.73	.73	232.14	4.50	4.50	-.13	10.1500	.1703	-.10	55.	55.	-.10	55.	55.	55.	55.	55.	55.	
36.000	5.5343	.0732	.55	.55	230.53	4.31	4.31	-.11	7.5500	.1573	-.05	55.	55.	-.05	55.	55.	55.	55.	55.	55.	
38.000	4.0831	.0359	.45	.45	251.35	3.91	3.91	-.28	5.5520	.1012	.12	55.	55.	.12	55.	55.	55.	55.	55.	55.	
40.000	3.1341	.0734	.22	.22	255.09	3.68	3.68	-.73	4.2510	.0339	.52	55.	55.	.52	55.	55.	55.	55.	55.	55.	
42.000	2.4155	.0603	.23	.23	253.14	3.52	3.52	-.41	3.2360	.0774	.11	55.	55.	.11	55.	55.	55.	55.	55.	55.	
44.000	1.8392	.0400	.13	.13	254.05	3.58	3.58	-.68	2.4640	.0455	.41	55.	55.	.41	55.	55.	55.	55.	55.	55.	
46.000	1.4519	.0407	-.02	-.02	258.33	3.80	3.80	-.04	1.8970	.0455	.32	54.	54.	.32	54.	54.	54.	54.	54.	54.	
48.000	1.1234	.0341	-.07	-.07	257.73	5.81	5.81	.53	1.4650	.0332	.10	54.	54.	.10	54.	54.	54.	54.	54.	54.	
50.000	.8734	.0253	-.20	-.20	257.62	4.23	4.23	.35	1.1420	.0177	.27	54.	54.	.27	54.	54.	54.	54.	54.	54.	
52.000	.6345	.0241	.01	.01	255.01	5.15	5.15	-.30	.675	.0170	.17	54.	54.	.17	54.	54.	54.	54.	54.	54.	
54.000	.5315	.0200	.11	.11	263.04	4.53	4.53	-.73	.7035	.0335	-.15	54.	54.	-.15	54.	54.	54.	54.	54.	54.	
56.000	.4111	.0163	.25	.25	253.59	5.49	5.49	-.47	.5517	.0202	.63	47.	47.	.63	47.	47.	47.	47.	47.	47.	
58.000	.3153	.0143	.41	.41	244.62	6.71	6.71	-.32	.4518	.0130	.15	43.	43.	.15	43.	43.	43.	43.	43.	43.	
60.000	.2421	.0122	.30	.30	249.39	7.51	7.51	-.21	.3385	.0130	.26	26.	26.	.26	26.	26.	26.	26.	26.	26.	
62.000	.1831	.0103	.34	.34	241.20	7.74	7.74	.05	.2244	.0124	-.05	26.	26.	-.05	26.	26.	26.	26.	26.	26.	
64.000	.1334	.0076	.45	.45	234.16	5.21	5.21	-.43	.2014	.0123	.33	15.	15.	.33	15.	15.	15.	15.	15.	15.	
66.000	.1034	.0051	.05	.05	229.41	5.42	5.42	-.47	.1591	.0060	.12	8.	8.	.12	8.	8.	8.	8.	8.	8.	

TABLE II-7. THERMODYNAMIC STATISTICAL PARAMETERS

JULY

STATION = 819020		ASCENSION (HIDE ANAKE)		S.D. T		SKEW T		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	MEAN P	S.D. P	SKEW P	DEG K	MEAN T	DEG K	SKEW T	MEAN D	G/H3	S.D. D	SKEW D	NOBS P	NOBS T	NOBS D	NOBS P	NOBS T	NOBS D
MB	MB	MB	MB	DEG K	MB	DEG K	MB	G/H3	G/H3	G/H3	G/H3	MB	MB	MB	MB	MB	MB
0.000	1010.4000	1.3598	.33	253.62	.97	-39	1170.0000	4.6030	.48	396.	396.	396.	396.	396.	396.	396.	396.
0.020	1008.1000	1.3313	.26	239.55	.96	-44	1167.0000	4.4690	.52	451.	451.	451.	451.	451.	451.	451.	451.
1.000	906.5100	1.3393	.33	239.72	1.03	.04	1034.0000	4.2130	.07	461.	461.	461.	461.	461.	461.	461.	461.
2.000	825.0200	1.2789	.05	255.83	2.45	.13	978.3000	7.9930	-.05	461.	461.	461.	461.	461.	461.	461.	461.
3.000	715.0200	1.2901	-.12	232.87	1.44	-.52	678.6000	4.9140	.05	461.	461.	461.	461.	461.	461.	461.	461.
4.000	633.2400	1.2648	-.20	277.36	1.36	-.35	793.5000	4.4010	-.03	461.	461.	461.	461.	461.	461.	461.	461.
5.000	559.5100	1.2034	-.33	272.05	1.32	-.37	715.2000	3.7510	.06	461.	461.	461.	461.	461.	461.	461.	461.
6.000	493.1800	1.2214	-.29	253.91	1.25	.16	643.9000	3.3700	-.35	460.	460.	460.	460.	460.	460.	460.	460.
7.000	433.3500	1.1658	-.20	253.91	1.25	.21	579.8000	3.2700	-.34	460.	460.	460.	460.	460.	460.	460.	460.
8.000	379.5500	1.1638	-.04	252.25	1.29	.01	521.9000	3.2020	-.56	459.	459.	459.	459.	459.	459.	459.	459.
9.000	331.1200	1.1447	-.04	245.23	1.37	.05	469.6000	2.9370	-.86	458.	458.	458.	458.	458.	458.	458.	458.
10.000	277.5300	1.1575	-.02	237.14	1.36	-.16	421.2000	2.6700	-1.04	455.	455.	455.	455.	455.	455.	455.	455.
11.000	243.7400	1.1420	-.12	229.12	1.41	.04	378.2000	1.7020	.19	454.	454.	454.	454.	454.	454.	454.	454.
12.000	213.7600	1.1049	-.11	221.22	1.27	.03	336.9000	1.4360	.13	453.	453.	453.	453.	453.	453.	453.	453.
13.000	193.0200	1.0537	-.11	213.99	1.39	.17	237.9000	1.5810	-.19	450.	450.	450.	450.	450.	450.	450.	450.
14.000	155.8100	.9901	-.05	207.64	1.41	-.07	251.4000	1.7500	-.15	450.	450.	450.	450.	450.	450.	450.	450.
15.000	132.0300	.9072	.03	202.62	1.50	.19	227.0000	1.8090	-.02	449.	449.	449.	449.	449.	449.	449.	449.
16.000	111.5300	.8055	.14	193.39	1.48	.04	194.5000	1.7670	.08	447.	447.	447.	447.	447.	447.	447.	447.
17.000	94.0370	.7066	.22	179.35	1.88	-.02	164.4000	2.0750	.21	441.	441.	441.	441.	441.	441.	441.	441.
18.000	79.4700	.6153	.40	202.39	2.37	-.07	135.5000	1.9790	.13	441.	441.	441.	441.	441.	441.	441.	441.
19.000	67.3750	.5256	.65	207.03	2.39	.08	113.4000	1.6200	.24	440.	440.	440.	440.	440.	440.	440.	440.
20.000	57.3100	.4739	.77	210.93	2.23	.08	94.5700	1.3470	.34	430.	430.	430.	430.	430.	430.	430.	430.
21.000	48.6580	.3751	.67	214.01	2.19	.19	79.5300	1.0010	.36	416.	416.	416.	416.	416.	416.	416.	416.
22.000	41.7600	.3374	.74	216.20	2.31	.48	67.3000	.8500	-.01	411.	411.	411.	411.	411.	411.	411.	411.
23.000	35.7470	.2939	.62	218.23	2.24	.59	57.0700	.6466	-.06	405.	405.	405.	405.	405.	405.	405.	405.
24.000	30.6230	.2692	.48	220.02	2.40	.43	48.4900	.5667	.24	406.	406.	406.	406.	406.	406.	406.	406.
25.000	26.2890	.2234	.13	222.19	2.33	.32	41.2200	.4727	.38	391.	391.	391.	391.	391.	391.	391.	391.
26.000	22.5540	.2057	.04	224.29	2.29	.30	35.1000	.4010	.67	381.	381.	381.	381.	381.	381.	381.	381.
27.000	19.4450	.1659	-.04	223.19	2.28	.26	29.5300	.3267	.19	357.	357.	357.	357.	357.	357.	357.	357.
28.000	16.7550	.1231	.07	227.49	2.11	.09	25.6300	.2537	.02	350.	350.	350.	350.	350.	350.	350.	350.
29.000	14.4470	.1495	.23	236.59	2.16	-.22	22.0200	.2403	.08	291.	291.	291.	291.	291.	291.	291.	291.
30.000	12.4760	.1359	.22	230.33	2.34	.24	18.8700	.2293	.27	285.	285.	285.	285.	285.	285.	285.	285.
32.000	9.2933	.1394	-.21	234.96	4.88	.00	13.7800	.2425	.27	73.	73.	73.	73.	73.	73.	73.	73.
34.000	6.9325	.1325	-.12	239.34	5.35	-.14	10.1800	.1717	.73	76.	76.	76.	76.	76.	76.	76.	76.
36.000	5.2826	.1203	-.21	243.36	4.24	.18	7.5630	.1139	-.01	72.	72.	72.	72.	72.	72.	72.	72.
38.000	4.0211	.1051	-.16	248.92	4.30	.18	5.6220	.1107	.03	72.	72.	72.	72.	72.	72.	72.	72.
40.000	3.0774	.0301	-.15	254.39	4.51	.20	3.1850	.0324	-.03	72.	72.	72.	72.	72.	72.	72.	72.
42.000	2.3580	.0768	-.03	253.93	4.51	.20	2.4210	.0810	.00	72.	72.	72.	72.	72.	72.	72.	72.
44.000	1.6307	.0631	-.01	263.37	4.83	-.50	2.4210	.0810	.00	72.	72.	72.	72.	72.	72.	72.	72.
46.000	1.4216	.0569	.04	267.39	5.41	-.05	1.6510	.0532	.16	73.	73.	73.	73.	73.	73.	73.	73.
48.000	1.1081	.0417	.03	265.44	5.95	.06	1.4340	.0321	.24	71.	71.	71.	71.	71.	71.	71.	71.
50.000	.8634	.0339	.41	268.42	5.97	.42	1.1180	.0425	.50	71.	71.	71.	71.	71.	71.	71.	71.
52.000	.6718	.0293	.49	257.69	5.11	.00	.8729	.0350	-.07	70.	70.	70.	70.	70.	70.	70.	70.
54.000	.5223	.0233	.54	261.98	5.26	-.08	.6337	.0297	.30	70.	70.	70.	70.	70.	70.	70.	70.
56.000	.4051	.0191	.61	261.34	5.33	-.24	.5400	.0241	.55	70.	70.	70.	70.	70.	70.	70.	70.
58.000	.3126	.0150	.65	253.24	6.01	.10	.4702	.0192	.53	68.	68.	68.	68.	68.	68.	68.	68.
60.000	.2399	.0140	.63	251.07	8.23	.18	.3313	.0174	.47	59.	59.	59.	59.	59.	59.	59.	59.
62.000	.1815	.0123	.95	243.71	7.73	-.27	.2434	.0154	.47	38.	38.	38.	38.	38.	38.	38.	38.
64.000	.1353	.0108	1.01	235.32	9.70	.00	.2003	.0141	.65	25.	25.	25.	25.	25.	25.	25.	25.
66.000	.1037	.0114	1.20	230.10	14.74	-.14	.1572	.0157	.61	10.	10.	10.	10.	10.	10.	10.	10.

TABLE II-8. THERMODYNAMIC STATISTICAL PARAMETERS

AUGUST

STATION - 615020	ASCENSION (WIDE AREA)	S.D. T	MEAN D	S.D. D	NOBS P	NOBS T	NOBS D
Z	MEAN P	SKEM P	MEAN T	SKEM T	MEAN D	S.D. D	NOBS D
KN	MB	MB	DEG K	DEG K	G/M3	G/M3	
1.000 1010.6000	1.5177	.24	297.50	-72	1173.0000	5.3850	330.
1.020 1008.3000	1.4655	.26	297.83	-75	1171.0000	5.1350	461.
1.000 906.4000	1.3032	.39	293.53	.94	.23 1087.0000	4.0180	477.
2.000 805.5000	1.2947	.21	293.71	2.60	30 975.5000	9.2650	477.
3.000 714.9700	1.3119	-.02	293.08	1.45	-.44 872.0000	4.5350	477.
4.000 633.1700	1.2169	-.03	277.20	1.37	-.37 734.5000	4.4080	477.
5.000 559.4400	1.1645	-.01	272.00	1.32	-.29 715.4000	3.8250	477.
6.000 493.1500	1.1297	-.13	265.40	1.31	-.17 643.6000	3.4180	477.
7.000 433.3400	1.1177	-.04	253.24	1.28	-.03 579.4000	3.0470	477.
8.000 379.6100	1.1251	-.04	253.24	1.26	.18 521.4000	2.9670	476.
9.000 331.2300	1.1159	.04	245.53	1.40	.12 469.3000	2.9220	474.
10.000 287.7800	1.1333	.16	237.35	1.37	.64 421.6000	2.5970	473.
11.000 245.3200	1.1249	.22	233.57	1.39	.64 373.0000	1.9370	471.
12.000 213.9400	1.0377	.39	221.57	1.35	.51 335.2000	1.5350	471.
13.000 183.2200	1.0502	.44	214.32	1.54	.39 297.8000	1.2780	471.
14.000 153.0100	1.0168	.44	207.09	1.61	.23 251.4000	1.0350	470.
15.000 132.2200	.9354	.51	202.82	1.51	.64 227.1000	1.0250	470.
16.000 111.7100	.8475	.53	193.72	1.51	.22 194.9000	1.0750	470.
17.000 94.2710	.7354	.71	193.53	1.79	.22 164.6000	2.0650	467.
18.000 79.6250	.6449	.63	203.14	2.32	.07 135.6000	2.0750	465.
19.000 67.5270	.5508	.75	207.41	2.41	-.32 113.4000	1.5350	464.
20.000 57.4410	.4501	.62	211.18	2.24	-.10 94.7700	1.2370	461.
21.000 48.0030	.3510	.51	214.25	2.35	.63 76.0000	.9979	449.
22.000 41.6520	.3460	.41	210.19	2.34	.50 67.6000	.8161	446.
23.000 35.6540	.3050	.28	217.64	2.33	.49 57.2500	.6229	441.
24.000 30.6310	.2676	.18	219.37	2.39	.26 48.7300	.5463	440.
25.000 26.3170	.2055	.09	221.46	2.30	.15 41.4000	.4570	431.
26.000 22.6070	.2422	.09	223.42	2.11	.35 35.2500	.3643	416.
27.000 19.4430	.2220	.14	225.07	2.14	.25 30.1000	.3350	389.
28.000 16.7500	.1979	.07	221.50	2.11	-.03 25.7700	.3119	382.
29.000 14.4240	.1711	.04	227.64	2.22	.15 22.0700	.2532	328.
30.000 12.4510	.1533	.12	229.59	2.24	-.22 18.6900	.2051	314.
31.000 9.2237	.1461	.15	229.59	4.00	-.65 13.7100	.2540	72.
32.000 6.9537	.1239	-.02	230.30	3.63	-.32 10.1400	.1441	72.
33.000 5.2399	.1103	-.21	246.80	4.20	-.27 7.5100	.1205	71.
34.000 3.9251	.0953	-.34	246.80	4.02	-.18 5.5700	.1029	71.
35.000 3.0505	.0813	-.40	255.30	4.37	-.30 4.1700	.0316	71.
36.000 2.5469	.0679	-.42	240.53	4.28	-.02 3.1200	.0835	71.
37.000 1.6215	.0555	-.45	263.24	4.59	-.18 2.3510	.0694	71.
38.000 1.4182	.0457	-.49	269.79	3.65	-.29 1.8290	.0528	65.
39.000 1.1081	.0371	-.47	273.69	4.34	.13 1.4230	.0470	67.
40.000 .6332	.0371	-.42	235.86	4.09	.33 1.1130	.0363	66.
41.000 .5722	.0234	-.41	267.29	4.09	.18 .8755	.0312	68.
42.000 .5223	.0185	-.30	263.91	4.60	-.28 .6539	.0257	67.
43.000 .4050	.0158	.15	250.07	4.72	-.26 .5423	.0215	66.
44.000 .3119	.0123	.12	253.51	6.25	.33 .4132	.0151	64.
45.000 .2397	.0100	.25	230.59	7.30	.05 .3520	.0121	58.
46.000 .1819	.0054	.61	218.25	9.19	-.10 .2583	.0077	44.
47.000 .1376	.0070	.30	253.53	5.23	.21 .1593	.0077	20.
48.000 .1049	.0055	-.30	238.16	15.45	-.27 .1540	.0120	7.

TABLE II-9. THERMODYNAMIC STATISTICAL PARAMETERS

## SEPTEMBER

STATION = 619020		ASCENSION (WIDE AREA)		S.D. T		SKEW T		MEAN D		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	MEAN P	S.D. P	SKEW P	MEAN T	DEG K	SKEW T	DEG K	MEAN D	G/M3	S.D. D	G/M3	SKEW D	G/M3	NOBS P	NOBS T	NOBS D	NOBS P	NOBS T	NOBS D
1.000	1010.3000	1.3225	-0.03	297.05	1.17	-0.32	1174.0000	5.2930	.18	365.	365.	.18	365.	365.	365.	365.	365.	365.	365.
1.000	1007.9000	1.3714	-0.04	297.57	1.16	-0.32	1171.0000	5.3230	.15	410.	410.	.15	410.	410.	410.	410.	410.	410.	410.
1.000	905.0100	1.2593	-0.03	293.74	.85	-0.23	1097.0000	3.5630	-.13	410.	410.	-.13	410.	410.	410.	410.	410.	410.	410.
2.000	805.2200	1.1663	-0.18	283.09	2.24	-0.94	970.5000	7.6030	.92	410.	410.	.92	410.	410.	410.	410.	410.	410.	410.
3.000	719.0000	1.1865	-0.25	283.19	1.40	-0.60	877.6000	4.3310	-.06	410.	410.	-.06	410.	410.	410.	410.	410.	410.	410.
4.000	633.2300	1.1063	-0.19	270.60	1.23	-0.21	755.7000	3.9330	-.09	410.	410.	-.09	410.	410.	410.	410.	410.	410.	410.
5.000	550.4200	1.1112	-0.13	271.31	1.27	-0.01	716.0000	3.6120	-.05	410.	410.	-.05	410.	410.	410.	410.	410.	410.	410.
6.000	493.1100	1.0235	-0.12	253.13	1.29	.03	613.5000	3.2730	-.22	410.	410.	-.22	410.	410.	410.	410.	410.	410.	410.
7.000	433.3300	1.0753	.02	253.23	1.27	.03	579.2000	2.6230	-.58	410.	410.	-.58	410.	410.	410.	410.	410.	410.	410.
8.000	379.5200	1.0235	.21	253.23	1.16	.30	521.4000	2.6570	-.62	409.	409.	-.62	409.	409.	409.	409.	409.	409.	409.
9.000	331.2000	1.0234	.32	243.52	1.23	.40	469.2000	2.7030	-.78	409.	409.	-.78	409.	409.	409.	409.	409.	409.	409.
10.000	287.7400	1.1039	.43	237.43	1.24	.37	421.6000	2.4740	-.82	409.	409.	-.82	409.	409.	409.	409.	409.	409.	409.
11.000	248.8800	1.1060	.55	229.51	1.24	.17	377.6000	1.6600	-.14	409.	409.	-.14	409.	409.	409.	409.	409.	409.	409.
12.000	213.9100	1.0232	.55	221.63	1.31	.04	336.2000	1.4640	-.46	410.	410.	-.46	410.	410.	410.	410.	410.	410.	410.
13.000	183.1900	1.0425	.59	214.22	1.37	.70	297.9000	1.4170	-.15	409.	409.	-.15	409.	409.	409.	409.	409.	409.	409.
14.000	155.9600	1.5527	.76	207.81	1.47	.63	261.5000	1.6940	-.41	409.	409.	-.41	409.	409.	409.	409.	409.	409.	409.
15.000	132.1900	.9238	.84	202.60	1.23	.32	227.1000	1.6260	-.17	409.	409.	-.17	409.	409.	409.	409.	409.	409.	409.
16.000	111.6500	.8189	.77	193.47	1.23	-.22	195.0000	1.7530	.31	410.	410.	.31	410.	410.	410.	410.	410.	410.	410.
17.000	94.2050	.6888	.83	193.02	1.67	-.23	164.5000	2.0370	.58	405.	405.	.58	405.	405.	405.	405.	405.	405.	405.
18.000	79.5160	.5943	.91	202.65	2.44	.35	136.7000	2.0290	.06	402.	402.	.06	402.	402.	402.	402.	402.	402.	402.
19.000	67.4130	.4915	.95	205.97	2.27	-.11	113.5000	1.5920	.50	403.	403.	.50	403.	403.	403.	403.	403.	403.	403.
20.000	57.3230	.4138	.78	219.77	2.45	.29	94.7700	1.2350	.40	400.	400.	.40	400.	400.	400.	400.	400.	400.	400.
21.000	48.8760	.2538	.70	213.78	2.73	.61	79.6000	1.0200	.25	395.	395.	.25	395.	395.	395.	395.	395.	395.	395.
22.000	41.7620	.3449	.70	216.02	2.52	.56	67.3600	.7283	.22	383.	383.	.22	383.	383.	383.	383.	383.	383.	383.
23.000	35.7430	.3227	.74	216.00	2.20	.44	57.1200	.5304	.39	372.	372.	.39	372.	372.	372.	372.	372.	372.	372.
24.000	30.6150	.3046	.74	219.36	2.18	.15	48.4900	.5005	.29	372.	372.	.29	372.	372.	372.	372.	372.	372.	372.
25.000	26.2730	.2039	.74	211.88	2.35	.04	41.6500	.4735	.16	368.	368.	.16	368.	368.	368.	368.	368.	368.	368.
26.000	22.5700	.2058	.67	223.95	2.15	-.09	35.1300	.3560	.14	350.	350.	.14	350.	350.	350.	350.	350.	350.	350.
27.000	19.4170	.2080	.64	235.51	2.09	-.01	30.0000	.3030	.29	317.	317.	.29	317.	317.	317.	317.	317.	317.	317.
28.000	16.7240	.2033	.62	253.03	1.99	-.05	25.0000	.3263	.31	314.	314.	.31	314.	314.	314.	314.	314.	314.	314.
29.000	14.4170	.1735	.65	233.26	2.22	.11	22.0000	.3030	.39	295.	295.	.39	295.	295.	295.	295.	295.	295.	295.
30.000	12.4520	.1546	.53	230.33	2.06	-.24	18.8300	.2556	.47	251.	251.	.47	251.	251.	251.	251.	251.	251.	251.
32.000	9.2765	.1944	-.29	236.24	5.12	.59	13.6700	.2357	-.07	74.	74.	-.07	74.	74.	74.	74.	74.	74.	74.
34.000	6.5039	.1831	-.31	241.53	4.34	-.39	10.0900	.2146	.03	73.	73.	.03	73.	73.	73.	73.	73.	73.	73.
36.000	5.3112	.1442	-.26	247.11	5.00	.15	7.4300	.1537	-.13	73.	73.	-.13	73.	73.	73.	73.	73.	73.	73.
38.000	4.0598	.1249	-.28	253.53	4.83	-.31	5.5710	.1139	.07	73.	73.	.07	73.	73.	73.	73.	73.	73.	73.
40.000	3.1260	.1050	-.32	253.83	3.98	.07	4.2020	.1150	-.07	73.	73.	-.07	73.	73.	73.	73.	73.	73.	73.
42.000	2.4119	.0855	-.28	262.52	4.14	.09	3.2000	.1027	-.38	73.	73.	-.38	73.	73.	73.	73.	73.	73.	73.
44.000	1.8719	.0696	-.25	267.48	5.22	.54	2.4300	.0907	-.18	73.	73.	-.18	73.	73.	73.	73.	73.	73.	73.
46.000	1.4533	.0573	-.16	270.27	5.50	.07	1.6780	.0656	-.31	73.	73.	-.31	73.	73.	73.	73.	73.	73.	73.
48.000	1.1387	.0471	-.02	271.93	5.12	.08	1.4500	.0445	-.40	72.	72.	-.40	72.	72.	72.	72.	72.	72.	72.
50.000	.8333	.0335	-.11	271.13	4.71	.20	1.1430	.0465	-.40	72.	72.	-.40	72.	72.	72.	72.	72.	72.	72.
52.000	.6235	.0283	-.23	263.41	4.55	-.63	.6382	.0725	-.19	71.	71.	-.19	71.	71.	71.	71.	71.	71.	71.
54.000	.5369	.0223	-.17	255.16	4.76	-.26	.7082	.0295	-.25	69.	69.	-.25	69.	69.	69.	69.	69.	69.	69.
56.000	.4176	.0186	-.04	260.08	5.49	.26	.5593	.0306	-.42	69.	69.	-.42	69.	69.	69.	69.	69.	69.	69.
58.000	.3239	.0153	.10	235.54	6.41	-.04	.4378	.0190	-.14	69.	69.	-.14	69.	69.	69.	69.	69.	69.	69.
60.000	.2474	.0125	.07	252.19	6.82	-.15	.3419	.0151	.40	66.	66.	.40	66.	66.	66.	66.	66.	66.	66.
62.000	.1878	.0101	.17	247.05	7.14	-.29	.2649	.0125	.60	57.	57.	.60	57.	57.	57.	57.	57.	57.	57.
64.000	.1412	.0072	.01	243.40	8.16	-.28	.2035	.0104	1.14	31.	31.	1.14	31.	31.	31.	31.	31.	31.	31.
65.000	.1049	.0055	-.07	233.65	8.85	-.155	.1554	.0167	1.09	11.	11.	1.09	11.	11.	11.	11.	11.	11.	11.

TABLE II-10. THERMODYNAMIC STATISTICAL PARAMETERS

OCTOBER

STATION - 615020	MEAN P	ASCENSION CHISE ANGLE:	S.D. T	SKEN T	MEAN D	S.D. D	SKEN D	NOBS P	NOBS T	NOBS D
Z	MB	S.D. P	SKEN P	CEC K	G/M <sup>3</sup>	G/M <sup>3</sup>	G/M <sup>3</sup>			
1.000	1009.1000	1.5166	.03	237.71	1.16	1172.0000	.22	388.	388.	388.
.620	1006.6000	1.5137	-.02	237.57	1.15	1105.0000	.25	427.	427.	427.
1.000	505.0000	1.5011	.15	238.87	.83	1005.0000	-.10	433.	433.	433.
2.000	804.6700	1.2103	.11	239.05	1.06	975.9000	.71	433.	433.	433.
3.000	714.7600	1.1931	-.02	238.63	1.10	875.9000	.10	433.	433.	433.
4.000	633.1100	1.1043	.01	277.19	1.14	754.9000	-.09	433.	433.	433.
5.000	553.3700	1.0575	-.03	271.04	1.32	715.0000	-.14	433.	433.	433.
6.000	493.0000	1.0502	-.07	255.55	1.30	674.7000	.02	433.	433.	433.
7.000	473.3500	1.0576	-.04	253.23	1.28	653.0000	.07	433.	433.	433.
8.000	373.0000	1.0373	.00	253.46	1.24	621.0000	.07	433.	433.	433.
9.000	331.2000	1.0444	.03	265.62	1.23	423.6000	-.39	432.	432.	432.
10.000	237.8500	1.0537	.01	237.53	1.23	377.7000	-.71	432.	432.	432.
11.000	243.0300	1.0336	.00	220.91	1.23	377.7000	-.48	432.	432.	432.
12.000	214.0700	1.0540	.10	221.97	1.14	355.0000	-.65	431.	431.	431.
13.000	183.3000	.9753	.08	214.31	1.13	328.1000	-.10	430.	430.	430.
14.000	156.1100	.9057	.15	207.48	1.27	232.1000	-.45	430.	430.	430.
15.000	132.2400	.8328	.21	201.94	1.34	223.1000	-.07	429.	429.	429.
16.000	111.5100	.7655	.27	153.45	1.39	195.0000	.32	429.	429.	429.
17.000	94.0210	.6341	.31	157.65	1.05	163.0000	.55	427.	427.	427.
18.000	79.2830	.5360	.32	200.60	2.53	137.7000	.31	427.	427.	427.
19.000	67.1080	.4530	.45	205.30	2.50	115.9000	.25	425.	425.	425.
20.000	57.0050	.4035	.26	203.31	2.62	94.8000	.13	421.	421.	421.
21.000	48.5450	.3973	.14	212.35	2.50	79.6000	.03	406.	406.	406.
22.000	41.4350	.3785	.15	214.83	2.69	67.2000	.01	404.	404.	404.
23.000	35.4400	.3559	.20	217.07	2.47	53.6000	.32	396.	396.	396.
24.000	30.3590	.3442	.24	219.45	2.65	48.1600	.25	395.	395.	395.
25.000	26.0210	.3140	.18	221.55	2.46	40.9300	.25	385.	385.	385.
26.000	22.3500	.2830	.19	223.60	2.32	34.8200	.24	369.	369.	369.
27.000	19.2180	.2528	.20	225.63	2.26	29.6700	.07	330.	330.	330.
28.000	18.2510	.2271	.15	227.62	2.26	25.3300	-.05	326.	326.	326.
29.000	14.2760	.1915	.11	220.53	2.45	21.6000	.01	274.	274.	274.
30.000	12.3430	.1691	.12	222.12	2.32	18.5300	.08	208.	208.	208.
31.000	9.2531	.1427	-.03	220.66	3.69	13.5100	-.04	73.	73.	73.
32.000	6.8020	.1225	.13	200.48	2.84	10.6000	.35	73.	73.	73.
33.000	5.3563	.1033	.10	200.45	4.14	7.9400	-.42	73.	73.	73.
34.000	4.0737	.0833	.16	203.77	4.27	5.2910	.13	73.	73.	73.
35.000	3.1267	.0623	.25	202.28	4.14	4.2010	.00	73.	73.	73.
36.000	2.4190	.0565	.31	204.53	4.02	3.1320	.04	74.	74.	74.
37.000	1.8811	.0475	.40	229.10	3.47	2.4320	.02	70.	70.	70.
38.000	1.4033	.0475	.40	229.10	3.47	1.8760	-.23	73.	73.	73.
39.000	1.1478	.0375	.44	272.91	3.91	1.4350	.04	64.	64.	64.
40.000	.8609	.0315	.33	271.72	3.63	1.1500	-.53	72.	72.	72.
41.000	.7000	.0261	.27	255.03	3.41	.9000	-.55	72.	72.	72.
42.000	.5943	.0204	.13	225.02	4.39	.7143	.24	71.	71.	71.
43.000	.4615	.0166	-.07	201.72	5.03	.5612	-.83	70.	70.	70.
44.000	.3242	.0132	-.03	259.15	6.01	.451	-.47	64.	64.	64.
45.000	.2437	.0110	.32	263.70	6.92	.347	-.22	58.	58.	58.
46.000	.1690	.0093	-.05	246.80	7.19	.2633	.26	45.	45.	45.
47.000	.1427	.0077	-.01	220.52	9.13	.2073	.02	25.	25.	25.
48.000	.1078	.0074	-.25	232.02	9.64	.1612	.52	13.	13.	13.

TABLE II-1.1. THERMODYNAMIC STATISTICAL PARAMETERS

## NOVEMBER

STATION = 6180±0		ASCENSION (WIDE AREA)				S.D. T		SKEW T		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	MEAN P	S.D. P	MEAN T	SKEW P	DEG K	DEG K	DEG K	DEG K	DEG K	G/M3	G/M3	G/M3	G/M3						
KM	MB	MB	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K	G/M3	G/M3	G/M3	G/M3						
0.000	1008.0000	1.6294	298.18	.05	1.11	.07	1168.0000	5.5583	.02	405.	405.	.02	405.	405.	405.	405.	405.	405.	405.
.020	1005.5000	1.6288	298.13	.08	1.19	-.05	1165.0000	5.9410	.10	429.	429.	.10	429.	429.	429.	429.	429.	429.	429.
1.000	894.2500	1.3315	293.36	.14	1.10	.78	1002.0000	4.5010	-.46	430.	430.	-.46	430.	430.	430.	430.	430.	430.	430.
2.000	874.0000	1.2854	293.54	.14	1.80	-.09	857.6000	6.1830	.74	430.	430.	.74	430.	430.	430.	430.	430.	430.	430.
3.000	714.0500	1.2514	293.30	.14	1.25	-.23	875.0000	3.8530	.05	430.	430.	.05	430.	430.	430.	430.	430.	430.	430.
4.000	632.5000	1.1856	277.68	.01	1.27	-.01	762.2000	3.6530	-.21	430.	430.	-.21	430.	430.	430.	430.	430.	430.	430.
5.000	558.9300	1.1276	272.30	-.06	1.32	-.20	714.1000	3.6330	.01	430.	430.	.01	430.	430.	430.	430.	430.	430.	430.
6.000	492.7800	1.1486	265.43	.01	1.40	-.16	643.5000	3.4200	-.03	430.	430.	-.03	430.	430.	430.	430.	430.	430.	430.
7.000	433.1100	1.1560	260.00	-.01	1.41	-.01	579.4000	3.1010	-.21	430.	430.	-.21	430.	430.	430.	430.	430.	430.	430.
8.000	379.2600	1.1795	253.19	-.03	1.29	-.01	521.2000	2.6790	-.26	430.	430.	-.26	430.	430.	430.	430.	430.	430.	430.
9.000	330.9300	1.1738	245.70	-.08	1.37	-.25	469.6000	2.6200	-.45	428.	428.	-.45	428.	428.	428.	428.	428.	428.	428.
10.000	287.5500	1.2233	237.67	-.12	1.40	-.33	420.0000	2.4670	-.73	426.	426.	-.73	426.	426.	426.	426.	426.	426.	426.
11.000	243.7500	1.2259	229.68	-.17	1.39	-.23	377.3000	1.9100	.02	426.	426.	.02	426.	426.	426.	426.	426.	426.	426.
12.000	213.8200	1.1920	221.82	-.11	1.25	-.02	335.8000	1.6100	.08	425.	425.	.08	425.	425.	425.	425.	425.	425.	425.
13.000	183.1300	1.1300	214.36	-.08	1.27	-.23	297.6000	1.4470	-.24	424.	424.	-.24	424.	424.	424.	424.	424.	424.	424.
14.000	155.9400	1.0536	207.71	.00	1.27	.10	261.5000	1.3130	-.12	424.	424.	-.12	424.	424.	424.	424.	424.	424.	424.
15.000	132.0900	.9431	201.53	.09	1.46	-.25	227.8000	1.8000	-.57	423.	423.	-.57	423.	423.	423.	423.	423.	423.	423.
16.000	111.4700	.8514	197.63	.19	1.53	-.05	195.2000	2.0040	-.15	421.	421.	-.15	421.	421.	421.	421.	421.	421.	421.
17.000	93.8750	.7249	185.58	.30	1.74	-.14	163.4000	2.0250	.13	415.	415.	.13	415.	415.	415.	415.	415.	415.	415.
18.000	79.0300	.6129	172.63	.39	2.45	-.15	130.4000	2.0070	.33	412.	412.	.33	412.	412.	412.	412.	412.	412.	412.
19.000	66.7000	.5104	163.52	.20	2.48	.16	114.3000	1.9100	.24	409.	409.	.24	409.	409.	409.	409.	409.	409.	409.
20.000	56.0200	.4572	157.60	.15	2.42	.40	93.0000	1.6710	.27	408.	408.	.27	408.	408.	408.	408.	408.	408.	408.
21.000	40.1000	.4133	141.10	.09	2.50	.07	73.5100	.9130	-.01	393.	393.	-.01	393.	393.	393.	393.	393.	393.	393.
22.000	41.0960	.3956	131.87	.10	2.35	.59	66.9100	.7437	.28	392.	392.	.28	392.	392.	392.	392.	392.	392.	392.
23.000	35.1300	.3821	116.41	.18	2.14	.48	58.5600	.5373	.23	387.	387.	.23	387.	387.	387.	387.	387.	387.	387.
24.000	30.0270	.3632	101.70	.23	2.15	-.03	47.6200	.5422	.04	386.	386.	.04	386.	386.	386.	386.	386.	386.	386.
25.000	25.7740	.2633	82.105	.25	2.07	-.04	40.6200	.5187	.14	382.	382.	.14	382.	382.	382.	382.	382.	382.	382.
26.000	22.1260	.2542	63.64	.25	2.07	.05	34.4800	.4624	.17	367.	367.	.17	367.	367.	367.	367.	367.	367.	367.
27.000	19.0400	.2164	43.35	.21	2.37	.33	29.3100	.4293	.13	334.	334.	.13	334.	334.	334.	334.	334.	334.	334.
28.000	16.4140	.1631	23.07	.11	2.50	.30	24.9700	.3742	.07	324.	324.	.07	324.	324.	324.	324.	324.	324.	324.
29.000	14.1790	.1673	23.37	.21	2.52	-.03	21.3500	.2553	.23	266.	266.	.23	266.	266.	266.	266.	266.	266.	266.
30.000	12.2660	.1462	233.49	.17	2.42	.15	18.3070	.2335	.29	263.	263.	.29	263.	263.	263.	263.	263.	263.	263.
32.000	9.2042	.1374	238.01	-.16	3.80	-.08	13.5000	.2043	.23	57.	57.	.23	57.	57.	57.	57.	57.	57.	57.
34.000	6.9466	.1139	242.39	.01	5.07	-.27	9.9560	.1930	-.77	57.	57.	-.77	57.	57.	57.	57.	57.	57.	57.
35.000	5.2039	.1031	247.16	-.15	5.06	-.12	7.4340	.1482	.13	57.	57.	.13	57.	57.	57.	57.	57.	57.	57.
38.000	4.0255	.0827	253.45	-.14	5.01	-.65	5.5380	.1116	.09	57.	57.	.09	57.	57.	57.	57.	57.	57.	57.
40.000	3.0374	.0737	260.23	-.26	5.90	-.22	4.1520	.0707	.08	57.	57.	.08	57.	57.	57.	57.	57.	57.	57.
42.000	2.3926	.0643	265.03	-.50	5.26	-.42	3.1730	.0672	.24	57.	57.	.24	57.	57.	57.	57.	57.	57.	57.
44.000	1.8628	.0548	271.43	-.75	4.56	-.71	2.4130	.0509	.13	57.	57.	.13	57.	57.	57.	57.	57.	57.	57.
46.000	1.4530	.0455	271.25	-.02	4.53	.05	1.8720	.0337	-.03	57.	57.	-.03	57.	57.	57.	57.	57.	57.	57.
48.000	1.1354	.0373	271.48	-.03	4.82	.39	1.4620	.0410	-.23	57.	57.	-.23	57.	57.	57.	57.	57.	57.	57.
50.000	.8854	.0311	269.78	-.01	5.48	.42	1.1470	.0357	-.84	57.	57.	-.84	57.	57.	57.	57.	57.	57.	57.
52.000	.6916	.0278	267.60	-.55	5.73	-.09	.9020	.0307	-.12	56.	56.	-.12	56.	56.	56.	56.	56.	56.	56.
54.000	.5387	.0247	264.90	-.22	6.21	-.24	.7053	.0253	.38	59.	59.	.38	59.	59.	59.	59.	59.	59.	59.
56.000	.4123	.0206	261.04	-.25	6.35	-.28	.5578	.0215	.26	56.	56.	.26	56.	56.	56.	56.	56.	56.	56.
58.000	.2700	.0175	257.27	-.13	7.41	-.13	.4031	.0177	.35	53.	53.	.35	53.	53.	53.	53.	53.	53.	53.
60.000	.2403	.0130	259.41	-.23	8.31	-.24	.2417	.0167	.31	46.	46.	.31	46.	46.	46.	46.	46.	46.	46.
62.000	.1853	.0056	246.82	-.40	8.80	.53	.2381	.0154	.43	31.	31.	.43	31.	31.	31.	31.	31.	31.	31.
64.000	.1430	.0028	232.13	-.23	9.51	1.05	.2031	.0147	-.11	20.	20.	-.11	20.	20.	20.	20.	20.	20.	20.
66.000	.1093	.0004	227.45	-.75	9.02	-.75	.1505	.0159	-.27	9.	9.	-.27	9.	9.	9.	9.	9.	9.	9.



TABLE II-12. THERMODYNAMIC STATISTICAL PARAMETERS

## DECEMBER

STATION = 619020		ASCENSION (HIDE AWAKE)				S.D. T		SKEW T		MEAN D		S.D. D		SKEW D		NOBS P		NOBS T		NOBS D	
Z	MI	MEAN P	MB	SKW P	MEAN T	DEG K	DEG K	SKW T	SKW K	G/M3	G/M3	G/M3	G/M3	G/M3	G/M3						
.000	1007.3000	1.6470	1.6470	-.04	298.66	1.20	1.20	.01	.01	1165.0000	5.8310	.11	.11	.11	.11	428.	428.	428.	428.	428.	428.
.020	1005.0000	1.6220	1.6220	-.06	293.60	1.19	1.19	-.02	-.02	1163.0000	5.8290	.14	.14	.14	.14	453.	453.	453.	453.	453.	453.
1.000	903.9400	1.4240	1.4240	-.08	290.09	1.25	1.25	-.67	-.67	1079.0000	5.1940	-.79	-.79	-.79	-.79	453.	453.	453.	453.	453.	453.
2.000	803.8900	1.3345	1.3345	-.05	288.89	1.23	1.23	-.93	-.93	866.3000	6.0640	.25	.25	.25	.25	453.	453.	453.	453.	453.	453.
3.000	714.1200	1.3160	1.3160	-.14	283.49	1.33	1.33	-.54	-.54	875.4000	4.2190	-.07	-.07	-.07	-.07	453.	453.	453.	453.	453.	453.
4.000	632.5800	1.2835	1.2835	-.17	277.33	1.36	1.36	-.03	-.03	793.1000	3.2230	.07	.07	.07	.07	453.	453.	453.	453.	453.	453.
5.000	558.6300	1.2032	1.2032	-.10	272.10	1.42	1.42	-.16	-.16	714.7000	4.1600	.12	.12	.12	.12	453.	453.	453.	453.	453.	453.
6.000	482.7500	1.1845	1.1845	-.06	266.57	1.48	1.48	.11	.11	643.6000	3.5670	-.24	-.24	-.24	-.24	452.	452.	452.	452.	452.	452.
7.000	433.0300	1.1851	1.1851	.01	260.20	1.32	1.32	-.15	-.15	579.1000	2.6800	-.38	-.38	-.38	-.38	450.	450.	450.	450.	450.	450.
8.000	378.3200	1.2183	1.2183	.14	253.21	1.26	1.26	-.33	-.33	521.3000	2.5610	-.81	-.81	-.81	-.81	448.	448.	448.	448.	448.	448.
9.000	330.9800	1.1971	1.1971	-.03	245.55	1.33	1.33	-.35	-.35	468.9000	2.6100	-.1.03	-.1.03	-.1.03	-.1.03	448.	448.	448.	448.	448.	448.
10.000	287.5800	1.2136	1.2136	-.09	237.51	1.34	1.34	-.35	-.35	421.2000	2.5290	.24	.24	.24	.24	447.	447.	447.	447.	447.	447.
11.000	248.7500	1.1948	1.1948	-.15	233.50	1.36	1.36	-.12	-.12	377.0000	1.6750	.49	.49	.49	.49	447.	447.	447.	447.	447.	447.
12.000	213.6100	1.1374	1.1374	-.03	221.63	1.36	1.36	-.11	-.11	333.0000	1.5930	.19	.19	.19	.19	447.	447.	447.	447.	447.	447.
13.000	183.1000	1.1071	1.1071	-.07	214.35	1.39	1.39	.33	.33	287.0000	1.6370	.52	.52	.52	.52	446.	446.	446.	446.	446.	446.
14.000	155.8200	1.0221	1.0221	.01	207.73	1.53	1.53	.53	.53	231.3000	2.0200	.22	.22	.22	.22	440.	440.	440.	440.	440.	440.
15.000	132.0800	.9638	.9638	.15	201.57	1.53	1.53	.35	.35	185.9000	2.0950	.38	.38	.38	.38	439.	439.	439.	439.	439.	439.
16.000	111.4400	.8707	.8707	.30	197.56	1.60	1.60	-.06	-.06	144.0000	1.6930	.25	.25	.25	.25	436.	436.	436.	436.	436.	436.
17.000	93.7940	.7436	.7436	.39	193.37	1.59	1.59	.25	.25	137.4000	2.2150	.11	.11	.11	.11	424.	424.	424.	424.	424.	424.
18.000	78.8760	.6432	.6432	.39	193.19	2.67	2.67	.04	.04	167.2000	2.2150	.24	.24	.24	.24	420.	420.	420.	420.	420.	420.
19.000	68.5380	.5555	.5555	.29	201.62	2.76	2.76	-.09	-.09	114.6000	1.6930	.38	.38	.38	.38	418.	418.	418.	418.	418.	418.
20.000	52.4000	.4945	.4945	.23	205.47	2.55	2.55	-.06	-.06	95.1600	1.2030	.35	.35	.35	.35	416.	416.	416.	416.	416.	416.
21.000	47.9410	.4531	.4531	.16	210.31	2.42	2.42	.46	.46	73.4200	.8404	.25	.25	.25	.25	407.	407.	407.	407.	407.	407.
22.000	40.0630	.4288	.4288	.14	213.43	2.26	2.26	.40	.40	66.7000	.7712	.40	.40	.40	.40	374.	374.	374.	374.	374.	374.
23.000	34.9140	.3817	.3817	.15	215.78	2.05	2.05	.55	.55	56.3700	.5958	.24	.24	.24	.24	367.	367.	367.	367.	367.	367.
24.000	29.8250	.3477	.3477	.16	217.68	2.12	2.12	.11	.11	47.7500	.5704	.05	.05	.05	.05	293.	293.	293.	293.	293.	293.
25.000	25.5320	.3151	.3151	.07	220.23	2.25	2.25	.14	.14	40.4900	.5322	.26	.26	.26	.26	54.	54.	54.	54.	54.	54.
26.000	21.8750	.2785	.2785	.04	223.06	2.22	2.22	.31	.31	34.3200	.5215	.36	.36	.36	.36	54.	54.	54.	54.	54.	54.
27.000	18.8530	.2593	.2593	.06	225.60	2.51	2.51	.26	.26	29.1600	.4823	.14	.14	.14	.14	54.	54.	54.	54.	54.	54.
28.000	15.2200	.2423	.2423	.01	228.65	2.64	2.64	.44	.44	24.2100	.4145	.25	.25	.25	.25	54.	54.	54.	54.	54.	54.
29.000	14.8510	.1801	.1801	-.02	230.63	2.71	2.71	.39	.39	21.2100	.3409	.35	.35	.35	.35	54.	54.	54.	54.	54.	54.
30.000	12.1500	.1585	.1585	-.07	233.61	2.35	2.35	.33	.33	18.2100	.2637	.36	.36	.36	.36	54.	54.	54.	54.	54.	54.
32.000	9.0781	.1805	.1805	-.34	235.49	3.89	3.89	.23	.23	13.4400	.2150	.20	.20	.20	.20	54.	54.	54.	54.	54.	54.
34.000	6.8348	.1572	.1572	-.23	240.23	4.42	4.42	-.02	-.02	9.9150	.1627	.03	.03	.03	.03	54.	54.	54.	54.	54.	54.
36.000	5.1724	.1334	.1334	-.25	244.70	4.31	4.31	.23	.23	7.3330	.1447	.26	.26	.26	.26	54.	54.	54.	54.	54.	54.
38.000	3.9397	.1132	.1132	-.32	246.31	5.99	5.99	.08	.08	5.3090	.1177	.03	.03	.03	.03	54.	54.	54.	54.	54.	54.
40.000	3.0162	.1044	.1044	-.25	253.53	8.00	8.00	.02	.02	4.0350	.0900	.20	.20	.20	.20	54.	54.	54.	54.	54.	54.
42.000	2.7233	.0903	.0903	-.53	253.47	5.37	5.37	-.53	-.53	3.0910	.0937	.03	.03	.03	.03	54.	54.	54.	54.	54.	54.
44.000	1.6234	.0750	.0750	-.45	253.50	4.47	4.47	-.55	-.55	2.3310	.0930	.03	.03	.03	.03	54.	54.	54.	54.	54.	54.
46.000	1.4683	.0623	.0623	-.45	259.12	4.54	4.54	-.20	-.20	1.8230	.0565	.04	.04	.04	.04	54.	54.	54.	54.	54.	54.
48.000	1.0978	.0522	.0522	-.54	270.01	4.63	4.63	.12	.12	1.4170	.0576	.10	.10	.10	.10	54.	54.	54.	54.	54.	54.
50.000	.8551	.0427	.0427	-.53	272.24	5.36	5.36	-.05	-.05	1.1070	.0530	.10	.10	.10	.10	54.	54.	54.	54.	54.	54.
52.000	.6809	.0352	.0352	-.71	287.08	6.15	6.15	.04	.04	.8639	.0438	.41	.41	.41	.41	54.	54.	54.	54.	54.	54.
54.000	.5132	.0273	.0273	-.74	293.37	8.39	8.39	.16	.16	.6790	.0356	.50	.50	.50	.50	54.	54.	54.	54.	54.	54.
56.000	.4025	.0218	.0218	-.74	293.74	7.44	7.44	.31	.31	.5318	.0235	.50	.50	.50	.50	54.	54.	54.	54.	54.	54.
58.000	.3117	.0175	.0175	-.72	299.72	7.63	7.63	.42	.42	.450	.0230	.21	.21	.21	.21	54.	54.	54.	54.	54.	54.
60.000	.2404	.0125	.0125	-.52	307.03	8.91	8.91	.48	.48	.3297	.0130	.48	.48	.48	.48	54.	54.	54.	54.	54.	54.
62.000	.1641	.0094	.0094	-.39	313.62	13.01	13.01	.35	.35	.2233	.0142	.19	.19	.19	.19	54.	54.	54.	54.	54.	54.
64.000	.1425	.0061	.0061	-.37	320.33	13.35	13.35	.19	.19	.1972	.0112	.48	.48	.48	.48	54.	54.	54.	54.	54.	54.
66.000	.1074	.0045	.0045	-.38	340.38	18.01	18.01	.53	.53	.1577	.0097	.19	.19	.19	.19	54.	54.	54.	54.	54.	54.

TABLE II-13. THERMODYNAMIC STATISTICAL PARAMETERS

## ANNUAL

STATION - 619020 Z KM	MEAN P PB	ACCELERATION (GAL) (4000)			S.D. T DEG K	SKEW T	MEAN D G/H3	S.D. D G/H3	SKEW D	NOBS P	NOBS T	NOBS D
		S.D. P PB	SKEW P	MEAN T DEG K								
.000	1059.0000	2.2681	.13	229.25	1.66	-.05	1154.0000	9.1040	-.01	4924.	4924.	4924.
.020	1055.7000	2.2373	.10	229.15	1.64	-.07	1161.0000	9.9480	-.02	5393.	5393.	5393.
.100	934.7500	1.7454	.18	229.55	1.71	-.18	1078.0000	7.7700	-.13	5481.	5481.	5481.
.200	834.5000	1.4943	.10	229.10	2.24	-.73	873.0000	7.8510	.82	5480.	5480.	5480.
.300	714.5000	1.2950	.05	229.55	1.33	-.43	873.0000	4.4820	.65	5480.	5480.	5480.
.400	632.9500	1.2435	.01	227.63	1.35	-.12	702.0000	4.1510	.01	5479.	5479.	5479.
.500	563.3800	1.1935	.02	229.23	1.34	-.24	714.0000	3.0530	.07	5479.	5479.	5479.
.600	493.1500	1.1287	.04	223.67	1.36	-.13	643.0000	3.4030	-.03	5478.	5478.	5478.
.700	433.4100	1.1752	.11	230.42	1.35	-.11	578.0000	2.9330	-.16	5476.	5476.	5476.
.800	379.7100	1.2077	.13	223.63	1.36	-.05	570.0000	2.8780	-.36	5468.	5468.	5468.
.900	331.4000	1.2191	.14	225.13	1.51	-.03	403.0000	2.0380	-.66	5457.	5457.	5457.
10.000	253.0000	1.2735	.14	223.11	1.54	.02	403.0000	2.0330	-.05	5449.	5449.	5449.
11.000	243.6400	1.2779	.11	222.02	1.53	.02	377.0000	1.7510	-.16	5443.	5443.	5443.
12.000	214.5000	1.2571	.17	222.42	1.43	.10	275.0000	1.4540	.13	5440.	5440.	5440.
13.000	183.5000	1.2035	.18	214.61	1.40	.28	283.0000	1.5500	-.55	5432.	5432.	5432.
14.000	153.3300	1.1195	.23	227.75	1.45	.23	222.0000	1.8740	-.53	5430.	5430.	5430.
15.000	132.4400	1.0071	.35	222.02	1.05	.29	223.0000	2.1720	-.23	5417.	5417.	5417.
16.000	111.7700	.8029	.42	193.01	1.34	.02	153.0000	2.2270	.01	5413.	5413.	5413.
17.000	94.1400	.7833	.49	195.53	2.59	.16	153.0000	2.0000	.05	5355.	5355.	5355.
18.000	79.2710	.6770	.44	172.10	3.64	.11	133.0000	2.6120	.14	5344.	5344.	5344.
19.000	67.0370	.6338	.57	223.07	3.52	.00	114.0000	1.0220	.29	5327.	5327.	5327.
20.000	55.5100	.6012	.18	227.97	3.22	.04	53.0000	1.2000	.23	5281.	5281.	5281.
21.000	48.3710	.5716	.05	211.24	3.00	.24	79.0000	.5781	.30	5123.	5123.	5123.
22.000	41.2530	.5450	.03	214.40	2.70	.18	67.0000	.9171	.24	5098.	5098.	5098.
23.000	35.2240	.4983	-.01	216.75	2.50	.12	56.7100	.0541	.18	5021.	5021.	5021.
24.000	30.1990	.4165	-.04	218.90	2.75	.04	48.0000	.6389	.05	4997.	4997.	4997.
25.000	25.6720	.4165	-.11	221.33	2.82	-.11	40.7500	.5156	.04	4929.	4929.	4929.
26.000	22.2000	.3735	-.19	223.53	2.67	-.14	34.5700	.5522	.01	4764.	4764.	4764.
27.000	19.1370	.3371	-.20	223.07	2.63	-.04	23.0000	.0150	-.05	4393.	4393.	4393.
28.000	14.8200	.2847	-.20	222.75	2.59	.02	21.0000	.0432	.00	3545.	3545.	3545.
29.000	12.8220	.2239	-.34	221.68	2.62	-.18	18.0000	.2307	.28	3467.	3467.	3467.
30.000	9.1820	.1500	-.12	225.13	4.29	-.04	13.0000	.0330	.03	875.	875.	875.
34.000	6.0240	.1042	-.12	240.49	4.53	.01	10.0000	.1532	.03	874.	874.	874.
36.000	5.7434	.1431	-.14	225.42	5.01	-.02	7.4420	.1553	-.12	823.	823.	823.
38.000	3.9236	.1821	-.16	231.28	5.30	-.23	5.5420	.1270	-.03	821.	821.	821.
40.000	3.0523	.1943	-.20	227.03	5.57	-.18	4.1510	.1143	.02	820.	820.	820.
42.000	2.3713	.0371	-.03	225.03	5.53	-.12	3.1570	.1031	.00	837.	837.	837.
44.000	1.6719	.0715	-.23	227.57	5.16	-.03	2.1500	.0630	-.02	830.	830.	830.
46.000	1.4249	.0514	-.39	223.01	4.93	-.01	1.3310	.0530	-.12	815.	815.	815.
48.000	1.1194	.0477	-.40	210.45	5.01	-.02	1.4410	.0633	-.31	810.	810.	810.
50.000	.8725	.0255	-.35	223.66	5.16	-.01	1.1250	.0779	-.31	803.	803.	803.
52.000	.6507	.0303	-.35	227.49	5.76	-.01	.7550	.0411	-.36	798.	798.	798.
54.000	.5233	.0248	-.25	224.23	5.06	.07	.6259	.0225	-.40	790.	790.	790.
56.000	.4102	.0159	-.19	221.05	6.57	.12	.5433	.0230	-.40	771.	771.	771.
58.000	.3163	.0170	-.31	222.75	7.55	.21	.4000	.0177	-.20	732.	732.	732.
60.000	.2722	.0127	.14	223.57	6.24	.16	.3245	.0151	-.04	701.	701.	701.
62.000	.1653	.0102	.03	220.12	9.32	.34	.2500	.0131	.29	510.	510.	510.
64.000	.1323	.0073	.01	242.43	10.19	.25	.2000	.0111	.52	275.	275.	275.
66.000	.1024	.0055	.37	234.53	10.37	-.70	.1505	.0104	.03	115.	115.	115.

TABLE III-1. MOISTURE RELATED STATISTICAL PARAMETERS

## JANUARY

STATION # 619020		ASCENSION (WIDE AWAKE)			TV		DEWPT T		S.D. DPT		NOBS T+P		NOBS TV	
Z	VAPOR P	S.D. VP	SKEW VP	TV	S.D.	SKEW TV	MEAN	S.D. DPT	SKEW DPT					
KM	MB	MB		DEG K	DEG K		DEG K	DEG K						
.000	23.401	2.217	-.09	302.02	1.40	-.13	203.10	1.55	-.34	460.	460.			
.020	23.228	2.187	-.10	301.92	1.37	-.14	202.53	1.54	-.37	493.	493.			
1.000	15.791	1.970	-.02	293.00	1.31	.31	206.85	1.96	-.43	490.	493.			
2.000	7.190	2.004	.23	280.05	1.70	-.58	274.27	6.24	-.55	460.	493.			
3.000	4.450	1.713	.21	264.03	1.25	-.52	267.92	5.61	-.57	443.	493.			
4.000	2.708	1.170	.28	277.98	1.27	.07	261.29	6.02	-.53	363.	492.			
5.000	1.212	.650	1.02	272.42	1.45	-.27	251.41	6.05	.10	330.	492.			
6.000	.574	.320	1.43	258.03	1.43	-.07	243.26	5.50	.30	303.	492.			
7.000	.313	.170	1.23	250.39	1.47	-.55	237.07	5.23	.18	295.	492.			
8.000	.169	.104	1.47	253.29	1.48	-.22	230.87	5.54	.13	298.	493.			
9.000	.090	.055	1.10	245.62	1.61	.36	224.97	5.68	-.17	320.	493.			
10.000	.043	.024	1.03	257.01	1.69	.62	212.91	5.09	-.45	261.	493.			
11.000	.020	.009	1.25	255.05	1.44	.10	213.35	3.35	.02	220.	492.			
12.000	.009	.004	1.20	271.95	1.29	.00	207.13	2.93	.12	210.	492.			
13.000	.003	.001	.03	214.53	1.33	.44	200.69	3.01	-.56	123.	492.			
14.000	.001	.001	.90	203.03	1.58	.50	194.76	3.13	-.35	84.	492.			
15.000	.001	.000	.96	202.16	1.89	.42	191.03	1.72	.38	14.	491.			
16.000	99.999	99.999	999.99	197.71	2.02	.40	959.99	99.99	999.99	0.	490.			
17.000	99.999	99.999	999.99	195.43	2.05	-.03	959.99	99.99	999.99	0.	495.			
18.000	99.999	99.999	999.99	192.62	2.00	.42	959.99	99.99	999.99	0.	465.			
19.000	99.999	99.999	999.99	200.53	2.67	.29	959.99	99.99	999.99	0.	483.			
20.000	99.999	99.999	999.99	255.09	2.59	.09	959.99	99.99	999.99	0.	473.			
21.000	99.999	99.999	999.99	269.47	2.43	.26	959.99	99.99	999.99	0.	472.			
22.000	99.999	99.999	999.99	212.70	2.28	.27	959.99	99.99	999.99	0.	470.			
23.000	99.999	99.999	999.99	214.49	2.07	.32	959.99	99.99	999.99	0.	464.			
24.000	99.999	99.999	999.99	216.40	2.35	.18	959.99	99.99	999.99	0.	458.			
25.000	99.999	99.999	999.99	218.51	2.53	.21	959.99	99.99	999.99	0.	454.			
26.000	99.999	99.999	999.99	221.05	2.61	.06	959.99	99.99	999.99	0.	440.			
27.000	99.999	99.999	999.99	223.04	2.62	-.02	959.99	99.99	999.99	0.	414.			
28.000	99.999	99.999	999.99	226.07	2.55	-.10	959.99	99.99	999.99	0.	410.			
29.000	99.999	99.999	999.99	223.44	2.63	-.10	959.99	99.99	999.99	0.	347.			
30.000	99.999	99.999	999.99	220.43	2.58	-.35	959.99	99.99	999.99	0.	339.			

TABLE III-2. MOISTURE RELATED STATISTICAL PARAMETERS

FEBRUARY

STATION = 610020		ASCENSION (WIDE AREA)		TV		TV		DEWPT T		S.D. DPT		SKEW DPT		NOBS T+P		NOBS TV	
Z	VAPOR P	S.D. VP	SKEW VP	TV	S.D.	SKEW TV	DEWPT T	S.D. DPT	SKEW DPT	NOBS T+P	NOBS TV						
MM	MM	MM		DEG K	DEG K		DEG K	DEG K									
.000	24.535	2.264	-.25	303.10	1.30	-.26	293.87	1.53	-.55	424.	424.						
.020	24.395	2.237	-.21	302.98	1.28	-.24	293.78	1.51	-.52	446.	446.						
1.000	16.030	2.250	-.19	293.85	1.21	.13	287.03	2.28	-1.01	446.	450.						
2.000	7.372	2.879	.49	293.17	1.50	-.27	274.77	5.74	-.29	427.	449.						
3.000	4.278	1.654	.15	284.09	1.34	.07	267.35	5.09	-.63	428.	449.						
4.000	2.420	1.201	.40	278.05	1.37	.21	259.94	6.55	-.32	374.	449.						
5.000	1.130	.626	1.43	272.78	1.43	-.05	250.68	5.81	.33	316.	449.						
6.000	.641	.301	2.53	267.22	1.50	-.14	244.41	5.55	.37	293.	448.						
7.000	.355	.192	1.57	260.81	1.47	-.11	233.42	5.13	.17	291.	448.						
8.000	.187	.100	1.04	253.92	1.44	.00	232.08	5.14	-.06	295.	448.						
9.000	.098	.053	.74	246.42	1.50	-.07	226.01	5.30	-.42	314.	448.						
10.000	.048	.024	.68	238.45	1.55	-.11	220.10	4.77	-.74	254.	449.						
11.000	.023	.009	.69	230.18	1.42	-.25	214.46	3.23	-.29	212.	449.						
12.000	.009	.003	.67	222.33	1.44	.30	207.81	2.82	-.36	214.	449.						
13.000	.003	.001	.72	214.07	1.50	.73	200.43	3.22	-.43	129.	449.						
14.000	.001	.001	.79	207.06	1.63	.52	194.41	3.03	-.40	85.	449.						
15.000	.001	.000	-.57	201.93	1.84	.33	189.56	2.86	-.85	10.	448.						
16.000	99.999	99.999	999.99	197.55	1.85	.11	999.99	99.99	999.99	0.	448.						
17.000	99.999	99.999	999.99	195.33	1.94	.58	999.99	99.99	999.99	0.	445.						
18.000	99.999	99.999	999.99	175.50	2.73	.32	999.99	99.99	999.99	0.	442.						
19.000	99.999	99.999	999.99	130.78	2.79	.31	999.99	99.99	999.99	0.	441.						
20.000	99.999	99.999	999.99	99.14	2.70	.25	999.99	99.99	999.99	0.	440.						
21.000	99.999	99.999	999.99	97.07	2.70	.81	999.99	99.99	999.99	0.	441.						
22.000	99.999	99.999	999.99	212.14	2.49	.12	999.99	99.99	999.99	0.	449.						
23.000	99.999	99.999	999.99	214.52	2.34	.25	999.99	99.99	999.99	0.	441.						
24.000	99.999	99.999	999.99	216.80	2.68	.43	999.99	99.99	999.99	0.	443.						
25.000	99.999	99.999	999.99	218.63	2.91	.33	999.99	99.99	999.99	0.	397.						
26.000	99.999	99.999	999.99	211.51	2.76	.21	999.99	99.99	999.99	0.	395.						
27.000	99.999	99.999	999.99	204.13	2.72	.16	999.99	99.99	999.99	0.	398.						
28.000	99.999	99.999	999.99	203.61	2.71	.05	999.99	99.99	999.99	0.	399.						
29.000	99.999	99.999	999.99	205.30	2.71	.30	999.99	99.99	999.99	0.	200.						
30.000	99.999	99.999	999.99	231.11	2.66	.09	999.99	99.99	999.99	0.	275.						

TABLE III-3. MOISTURE RELATED STATISTICAL PARAMETERS

## MARCH

STATION # 619020		ASCENSION (WIDE AREA)												
Z	VAPOR P	S.D. VP	SKEW VP	TV	TV	SKEW TV	DEWPT T	S.D. DPT	SKEW DPT	NOBS T+P	NOBS TV			
KM	MEAN			MEAN	S.D.		MEAN							
	MB	MB		DEG K	DEG K		DEG K	DEG K						
.000	25.709	2.299	.48	303.52	1.18	-.23	294.64	1.46	-.13	466.	468.			
.020	25.533	2.267	.47	303.70	1.17	-.25	294.53	1.45	-.14	480.	480.			
1.000	16.650	2.300	-.12	294.08	1.01	-.15	287.09	2.20	-.57	479.	463.			
2.000	8.354	3.029	.15	289.54	1.44	-.61	276.60	5.81	-.79	466.	460.			
3.000	4.894	1.817	.31	284.44	1.18	-.19	269.22	5.53	-.71	448.	460.			
4.000	2.739	1.234	.67	278.52	1.17	.06	261.31	6.27	-.35	377.	460.			
5.000	1.460	.827	1.40	273.09	1.30	.02	253.47	6.32	.12	341.	480.			
6.000	.753	.452	1.33	267.45	1.23	.06	245.85	6.39	.32	303.	420.			
7.000	.413	.275	2.05	261.19	1.19	.24	230.67	5.95	.35	301.	480.			
8.000	.225	.148	2.17	254.45	1.29	.10	223.47	5.95	.10	289.	490.			
9.000	.115	.074	2.02	247.13	1.41	.11	227.18	5.09	-.29	309.	460.			
10.000	.058	.024	2.23	239.26	1.44	.17	221.42	5.03	-.40	251.	479.			
11.000	.026	.013	2.16	233.05	1.32	.20	215.30	3.70	-.05	225.	479.			
12.000	.010	.005	2.08	222.76	1.23	-.10	208.60	3.16	.06	229.	479.			
13.000	.004	.002	1.91	214.51	1.26	.27	201.29	3.31	.07	113.	479.			
14.000	.001	.001	1.23	207.60	1.40	.18	194.73	3.21	-.18	90.	479.			
15.000	99.999	99.999	99.999	201.49	1.58	.13	99.99	99.99	999.99	3.	478.			
16.000	99.999	99.999	99.999	197.00	1.58	.14	99.99	99.99	999.99	0.	479.			
17.000	99.999	99.999	99.999	184.00	1.67	-.17	99.99	99.99	999.99	0.	473.			
18.000	99.999	99.999	99.999	165.57	2.84	.38	99.99	99.99	999.99	0.	474.			
19.000	99.999	99.999	99.999	201.22	2.66	.08	999.99	99.99	999.99	0.	473.			
20.000	99.999	99.999	99.999	205.80	2.46	.15	999.99	99.99	999.99	0.	470.			
21.000	99.999	99.999	99.999	203.60	2.23	.18	999.99	99.99	999.99	0.	450.			
22.000	99.999	99.999	99.999	213.11	2.14	.21	999.99	99.99	999.99	0.	450.			
23.000	99.999	99.999	99.999	215.72	1.96	.33	999.99	99.99	999.99	0.	445.			
24.000	99.999	99.999	99.999	218.10	2.32	.25	999.99	99.99	999.99	0.	447.			
25.000	99.999	99.999	99.999	200.00	2.56	.11	999.99	99.99	999.99	0.	443.			
26.000	99.999	99.999	99.999	222.81	2.50	.04	999.99	99.99	999.99	0.	429.			
27.000	99.999	99.999	99.999	225.22	2.47	-.22	999.99	99.99	999.99	0.	396.			
28.000	99.999	99.999	99.999	227.75	2.45	-.22	999.99	99.99	999.99	0.	385.			
29.000	99.999	99.999	99.999	230.10	2.59	-.33	999.99	99.99	999.99	0.	307.			
30.000	99.999	99.999	99.999	232.10	2.44	-.36	999.99	99.99	999.99	0.	300.			

TABLE III-4. MOISTURE RELATED STATISTICAL PARAMETERS

APRIL

STATION # 619020		ASCENSION (WIDE AWAKE)		TV		DEWPT T		S.D. DPT		NOBS T+P		NOBS TV	
Z	VAPOR P	S.D. VP	SKW VP	TV	S.D.	MEAN	S.D.	SKW DPT	NOBS T+P	NOBS TV			
KM	MB	MB		DEG K	DEG K	DEG K	DEG K						
0.000	25.020	2.504	-1.12	303.58	1.31	294.58	1.67	-1.51	422.	422.			
1.000	25.613	2.540	-1.09	303.97	1.30	294.55	1.65	-1.48	448.	448.			
2.000	16.734	2.200	-1.20	294.57	1.12	297.72	2.31	-1.78	459.	459.			
3.000	8.593	3.143	-1.11	291.03	1.43	275.55	5.83	-1.69	433.	433.			
4.000	4.722	1.900	1.34	284.87	1.22	268.62	5.81	-1.55	390.	409.			
5.000	2.513	1.205	1.60	279.05	1.20	260.03	6.69	-1.23	335.	409.			
6.000	1.444	1.901	1.31	273.53	1.24	253.07	6.78	1.33	297.	409.			
7.000	1.757	1.500	1.79	267.75	1.35	245.55	6.44	1.32	272.	409.			
8.000	1.424	1.207	1.06	261.10	1.35	239.22	6.07	1.40	265.	409.			
9.000	1.215	1.143	1.08	254.10	1.39	232.92	5.93	1.34	267.	409.			
10.000	1.116	1.077	1.70	247.03	1.60	227.41	5.02	-1.12	273.	409.			
11.000	1.020	1.033	1.53	240.07	1.70	221.53	5.04	-1.05	250.	409.			
12.000	1.006	1.012	1.34	231.55	1.35	215.46	3.57	-1.25	189.	409.			
13.000	1.010	1.004	1.91	223.35	1.14	208.77	2.74	-1.10	213.	409.			
14.000	1.004	1.002	1.20	215.34	1.17	201.09	3.17	-1.28	118.	409.			
15.000	1.001	1.001	1.04	207.71	1.31	194.32	2.85	-1.34	69.	409.			
16.000	99.999	99.999	999.00	201.09	1.44	187.99	99.99	999.99	5.	453.			
17.000	99.999	99.999	999.99	193.23	1.51	180.03	99.99	999.99	0.	453.			
18.000	99.999	99.999	999.99	184.15	1.70	172.99	99.99	999.99	0.	449.			
19.000	99.999	99.999	999.99	175.54	2.72	163.99	99.99	999.99	0.	448.			
20.000	99.999	99.999	999.99	167.77	2.74	155.04	99.99	999.99	0.	445.			
21.000	99.999	99.999	999.99	160.49	2.23	146.03	99.99	999.99	0.	443.			
22.000	99.999	99.999	999.99	153.03	2.24	137.99	99.99	999.99	0.	432.			
23.000	99.999	99.999	999.99	145.20	2.29	129.99	99.99	999.99	0.	432.			
24.000	99.999	99.999	999.99	137.30	2.09	121.03	99.99	999.99	0.	424.			
25.000	99.999	99.999	999.99	129.25	2.41	112.03	99.99	999.99	0.	419.			
26.000	99.999	99.999	999.99	121.00	2.52	103.03	99.99	999.99	0.	412.			
27.000	99.999	99.999	999.99	112.69	2.42	94.99	99.99	999.99	0.	404.			
28.000	99.999	99.999	999.99	104.06	2.47	86.03	99.99	999.99	0.	373.			
29.000	99.999	99.999	999.99	95.25	2.25	77.99	99.99	999.99	0.	351.			
30.000	99.999	99.999	999.99	86.55	2.19	68.99	99.99	999.99	0.	275.			
				233.47	2.04	59.99	99.99	999.99	0.	263.			

TABLE III-5. MOISTURE RELATED STATISTICAL PARAMETERS

MAY

STATION - 610020		ASCENSION (WIDE AWAKE)		TV		TV		DEWPT T		S.D. DPT		NOBS T+P		NOBS TV	
Z	VAPOR P	S.D. VP	SKEW VP	TV	S.D.	SKEW TV	DEWPT T	S.D. DPT	SKEW DPT	NOBS T+P	NOBS TV				
KM	MEAN MB	MEAN MB	MEAN MB	DEG K	DEG K	DEG K	DEG K	DEG K	DEG K						
.000	24.216	2.299	-.09	303.28	1.04	-.20	293.65	1.56	-.39	412.	412.				
.020	23.919	2.323	-.05	303.16	1.06	-.12	293.45	1.60	-.37	469.	469.				
1.000	15.555	2.274	-.05	293.67	1.11	-.05	265.58	2.32	-.62	465.	469.				
2.000	7.831	3.345	.25	283.17	1.71	-.31	274.89	0.82	-.45	431.	408.				
3.000	3.774	1.648	.20	274.84	1.51	-.08	265.31	0.52	-.12	355.	428.				
4.000	1.370	1.032	1.22	279.24	1.40	.04	257.04	6.38	.20	303.	498.				
5.000	1.101	.733	2.30	273.55	1.47	.18	250.03	6.23	.67	270.	479.				
6.000	.029	.420	2.02	267.76	1.53	.26	243.93	6.02	.65	257.	453.				
7.000	.340	.204	2.33	261.06	1.52	.44	237.85	5.24	.42	257.	498.				
8.000	.199	.121	1.82	255.20	1.67	.48	232.53	5.26	.30	272.	486.				
9.000	.109	.063	1.09	245.03	1.69	.60	226.91	5.43	-.20	295.	485.				
10.000	.075	.027	1.17	240.14	1.93	.77	221.34	4.41	-.56	253.	485.				
11.000	.026	.011	1.75	231.43	1.35	.91	215.60	3.27	-.05	214.	485.				
12.000	.010	.004	1.52	223.26	1.21	.09	208.55	2.64	-.03	233.	485.				
13.000	.004	.002	1.15	215.29	1.25	.07	201.53	3.10	-.09	135.	484.				
14.000	.001	.001	.55	207.75	1.28	.34	194.58	2.78	-.52	80.	483.				
15.000	99.999	99.999	999.93	201.51	1.51	.27	999.99	99.99	999.99	2.	482.				
16.000	99.999	99.999	999.99	195.63	1.64	-.06	999.99	99.99	999.99	0.	482.				
17.000	99.999	99.999	999.99	195.23	1.81	.28	999.99	99.99	999.99	0.	475.				
18.000	99.999	99.999	999.99	190.01	2.60	-.01	999.99	99.99	999.99	0.	475.				
19.000	99.999	99.999	999.99	207.79	2.31	-.05	999.99	99.99	999.99	0.	474.				
20.000	99.999	99.999	999.99	207.50	2.20	.10	999.99	99.99	999.99	0.	469.				
21.000	99.999	99.999	999.99	211.59	2.17	.06	999.99	99.99	999.99	0.	450.				
22.000	99.999	99.999	999.99	215.07	2.05	-.06	999.99	99.99	999.99	0.	455.				
23.000	99.999	99.999	999.99	217.99	1.84	-.01	999.99	99.99	999.99	0.	449.				
24.000	99.999	99.999	999.99	220.57	2.19	.16	999.99	99.99	999.99	0.	448.				
25.000	99.999	99.999	999.99	223.29	2.11	.10	999.99	99.99	999.99	0.	448.				
26.000	99.999	99.999	999.99	225.60	2.10	.00	999.99	99.99	999.99	0.	431.				
27.000	99.999	99.999	999.99	227.59	2.15	.33	999.99	99.99	999.99	0.	401.				
28.000	99.999	99.999	999.99	229.42	1.89	.31	999.99	99.99	999.99	0.	395.				
29.000	99.999	99.999	999.99	231.08	1.79	.27	999.99	99.99	999.99	0.	335.				
30.000	99.999	99.999	999.99	232.53	1.65	-.24	999.99	99.99	999.99	0.	332.				

TABLE III-6. MOISTURE RELATED STATISTICAL PARAMETERS

JUNE

STATION # 016020		ASCENSION (WIDE AWAKE)		TV		DESKPT T		NOBS T+P		NOBS TV	
Z	V-M P	S.D. VP	SKWH VP	MEAN	S.D.	MEAN	S.D.				
KM	MB			DEG K	DEG K	DEG K	DEG K				
0.000	22.328	2.511	.09	302.03	1.23	-1.37	292.32	1.83	-1.30	368.	368.
1.000	22.018	2.465	.11	301.94	1.27	-1.35	292.10	1.81	-1.26	426.	426.
2.000	19.023	2.065	.10	292.45	1.14	.09	292.72	2.21	-1.40	446.	447.
3.000	7.564	3.164	.13	297.53	2.06	.02	274.04	6.71	-1.64	369.	447.
4.000	2.861	1.479	1.91	274.42	1.53	-1.10	261.69	5.95	.27	344.	447.
5.000	1.549	.700	2.00	278.47	1.51	.32	254.50	5.34	.23	318.	447.
6.000	.918	.522	2.23	272.70	1.51	.01	240.44	5.32	.02	301.	447.
7.000	.493	.250	1.73	257.00	1.61	-1.09	241.98	4.90	.47	283.	447.
8.000	.312	.162	1.33	251.04	1.72	.14	237.18	4.92	.20	273.	447.
9.000	.179	.094	1.10	254.33	1.73	.46	231.73	4.50	-1.06	308.	447.
10.000	.092	.051	.83	245.65	1.91	.85	226.24	4.35	-1.40	329.	444.
11.000	.031	.029	2.45	279.50	1.96	1.06	220.05	4.55	-1.45	279.	444.
12.000	.024	.010	1.71	230.25	1.50	.30	214.97	3.16	-1.34	234.	444.
13.000	.010	.007	.75	222.25	1.40	.35	208.29	2.61	-1.40	235.	443.
14.000	.004	.002	.64	214.55	1.39	.72	201.70	2.37	-1.50	170.	442.
15.000	.001	.001	.73	207.63	1.48	.72	192.33	2.62	-1.46	83.	442.
16.000	.001	.000	-1.05	202.03	1.61	.34	191.18	1.49	-1.38	6.	433.
17.000	99.999	99.999	999.99	198.41	1.75	.27	999.99	99.99	999.99	0.	439.
18.000	99.999	99.999	999.99	197.45	2.05	-1.06	999.99	99.99	999.99	0.	421.
19.000	99.999	99.999	999.99	200.35	2.67	-1.03	999.99	99.99	999.99	0.	432.
20.000	99.999	99.999	999.99	205.01	2.41	.04	999.99	99.99	999.99	0.	431.
21.000	99.999	99.999	999.99	202.41	2.21	.03	999.99	99.99	999.99	0.	428.
22.000	99.999	99.999	999.99	212.74	2.25	-1.04	999.99	99.99	999.99	0.	416.
23.000	99.999	99.999	999.99	215.02	1.93	-1.15	999.99	99.99	999.99	0.	412.
24.000	99.999	99.999	999.99	210.04	1.98	-1.04	999.99	99.99	999.99	0.	407.
25.000	99.999	99.999	999.99	220.63	2.27	.30	999.99	99.99	999.99	0.	405.
26.000	99.999	99.999	999.99	223.09	2.21	.29	999.99	99.99	999.99	0.	402.
27.000	99.999	99.999	999.99	225.17	2.09	.09	999.99	99.99	999.99	0.	363.
28.000	99.999	99.999	999.99	227.08	2.19	.31	999.99	99.99	999.99	0.	360.
29.000	99.999	99.999	999.99	220.03	1.98	.34	999.99	99.99	999.99	0.	349.
30.000	99.999	99.999	999.99	222.03	2.13	.35	999.99	99.99	999.99	0.	294.
31.000	99.999	99.999	999.99	232.00	2.11	-1.16	999.99	99.99	999.99	0.	287.



TABLE III-7. MOISTURE RELATED STATISTICAL PARAMETERS

JULY

STATION = 819023		ASCENSION (WIDE AWAKE)		TV		TV		DEWPT T		S.D. DPT		NOBS T+P		NOBS TV	
Z	VAPOR P	S.D. VP	SKEM VP	TV	S.D.	SKEM TV	DEWPT T	S.D. DPT	SKEM DPT	NOBS T+P	NOBS TV				
MEAN				MEAN			MEAN								
K4	MB	MB		DEG K	DEG K		DEG K	DEG K							
.000	20.036	2.138	-.03	300.56	1.05	-.36	291.21	1.63	-.42	396.	396.				
.020	20.034	2.092	-.01	300.63	1.02	-.41	291.08	1.63	-.39	451.	451.				
1.000	13.655	1.945	.24	291.41	1.11	-.01	284.84	2.14	-.13	459.	461.				
2.000	8.569	2.919	.17	295.98	2.35	.13	273.79	6.47	-.51	406.	461.				
3.000	2.902	1.304	.81	283.51	1.59	-.18	251.70	5.91	-.05	354.	461.				
4.000	1.424	.683	1.23	277.89	1.56	-.06	253.61	5.30	.29	322.	461.				
5.000	.840	.444	1.76	272.53	1.48	-.28	247.56	5.18	.53	309.	461.				
6.000	.506	.292	2.25	270.23	1.46	.24	242.00	5.24	.46	302.	461.				
7.000	.339	.173	1.72	268.40	1.53	.33	238.91	5.31	.15	304.	460.				
8.000	.175	.082	1.00	263.34	1.69	.50	231.39	5.34	-.29	322.	459.				
9.000	.033	.049	.01	245.66	1.76	.72	225.58	5.32	-.59	347.	458.				
10.000	.048	.021	.64	237.95	1.73	.48	220.23	4.35	-1.08	292.	455.				
11.000	.022	.008	1.00	229.12	1.41	.04	214.17	3.12	-.42	239.	454.				
12.000	.009	.003	.50	221.32	1.27	.03	207.67	2.50	-.56	239.	453.				
13.000	.004	.001	.61	213.09	1.38	.17	201.55	2.34	-.27	125.	450.				
14.000	.001	.001	1.24	207.64	1.41	-.07	195.93	2.25	.10	69.	450.				
15.000	.001	.000	-.40	202.52	1.50	.19	190.05	2.22	-.59	6.	449.				
16.000	99.999	99.999	999.99	197.37	1.46	.04	909.99	99.99	999.99	0.	447.				
17.000	99.999	99.999	999.99	193.36	1.88	-.02	909.99	99.99	999.99	0.	441.				
18.000	99.999	99.999	999.99	202.89	2.37	-.07	999.99	99.99	999.99	0.	441.				
19.000	99.999	99.999	999.99	207.03	2.39	.08	999.99	99.99	999.99	0.	440.				
20.000	99.999	99.999	999.99	210.93	2.23	.08	999.99	99.99	999.99	0.	430.				
21.000	99.999	99.999	999.99	214.01	2.19	.19	999.99	99.99	999.99	0.	416.				
22.000	99.999	99.999	999.99	216.20	2.31	.48	999.99	99.99	999.99	0.	411.				
23.000	99.999	99.999	999.99	218.23	2.24	.59	999.99	99.99	999.99	0.	405.				
24.000	99.999	99.999	999.99	220.02	2.40	.43	999.99	99.99	999.99	0.	406.				
25.000	99.999	99.999	999.99	222.19	2.33	.32	999.99	99.99	999.99	0.	331.				
26.000	99.999	99.999	999.99	224.29	2.29	.30	999.99	99.99	999.99	0.	381.				
27.000	99.999	99.999	999.99	226.19	2.28	.26	999.99	99.99	999.99	0.	357.				
28.000	99.999	99.999	999.99	227.49	2.11	.09	999.99	99.99	999.99	0.	350.				
29.000	99.999	99.999	999.99	230.59	2.16	-.22	999.99	99.99	999.99	0.	291.				
30.000	99.999	99.999	999.99	230.33	2.34	-.70	999.99	99.99	999.99	0.	285.				

TABLE III-8. MOISTURE RELATED STATISTICAL PARAMETERS

AUGUST

STATION - 619020		ASCENSION (WIDE AWAKE)				TV		DEWPT T		S.D. DPT		NOBS T+P		NOBS TV	
Z	VAPOR P	S.D. VP	SKEW VP	TV	TV	S.D.	SKEW TV	MEAN	MEAN	S.D. DPT	SKEW DPT				
MM	MB	MS		DEG K	DEG K			DEG K	DEG K						
.000	20.010	2.233	-.15	300.15	1.21	-.70		290.57	1.84		-.54	390.		390.	
.020	19.843	2.219	-.22	300.07	1.16	-.73		290.44	1.62		-.60	461.		461.	
1.000	13.740	1.823	.08	290.62	1.03	.11		284.71	2.18		-.27	475.		477.	
2.000	5.928	2.623	.61	287.63	2.71	-.28		271.29	6.90		-.27	406.		477.	
3.000	2.905	1.341	1.39	283.70	1.63	-.16		262.23	5.75		-.08	390.		477.	
4.000	1.545	.748	.63	277.68	1.52	-.19		254.45	5.69		.03	338.		477.	
5.000	.838	.413	1.55	272.43	1.48	-.15		247.65	4.92		.45	319.		477.	
6.000	.520	.269	1.16	265.82	1.48	.18		242.37	5.16		.29	322.		477.	
7.000	.316	.173	1.51	260.84	1.47	.23		237.18	5.21		.17	328.		477.	
8.000	.180	.076	.73	253.06	1.56	.54		231.63	5.40		-.34	335.		476.	
9.000	.033	.046	.43	245.20	1.73	.57		225.93	3.70		-.68	353.		474.	
10.000	.049	.023	.70	237.69	1.60	.70		220.44	4.30		-.02	290.		473.	
11.000	.021	.009	.62	229.33	1.44	1.04		214.03	3.04		-.32	298.		471.	
12.000	.009	.003	.44	221.67	1.36	.61		207.44	2.71		-.49	257.		471.	
13.000	.003	.001	.20	214.32	1.54	.39		200.82	3.01		-.52	140.		471.	
14.000	.001	.001	.44	207.69	1.61	.23		194.80	2.51		-.29	52.		470.	
15.000	99.999	99.999	999.99	202.82	1.51	.64		999.99	99.99	999.99	999.99	2.		470.	
16.000	99.999	99.999	999.99	193.72	1.51	.23		999.99	99.99	999.99	999.99	0.		470.	
17.000	99.999	99.999	999.99	193.03	1.79	.29		999.99	99.99	999.99	999.99	0.		467.	
18.000	99.999	99.999	999.99	203.14	2.32	.07		999.99	99.99	999.99	999.99	0.		466.	
19.000	99.999	99.999	999.99	207.41	2.41	-.32		999.99	99.99	999.99	999.99	0.		464.	
20.000	99.999	99.999	999.99	211.18	2.24	-.10		999.99	99.99	999.99	999.99	0.		461.	
21.000	99.999	99.999	999.99	214.23	2.33	.63		999.99	99.99	999.99	999.99	0.		449.	
22.000	99.999	99.999	999.99	216.19	2.74	.60		999.99	99.99	999.99	999.99	0.		445.	
23.000	99.999	99.999	999.99	217.84	2.33	.40		999.99	99.99	999.99	999.99	0.		441.	
24.000	99.999	99.999	999.99	219.37	2.39	.26		999.99	99.99	999.99	999.99	0.		440.	
25.000	99.999	99.999	999.99	221.46	2.30	.15		999.99	99.99	999.99	999.99	0.		431.	
26.000	99.999	99.999	999.99	223.42	2.11	.33		999.99	99.99	999.99	999.99	0.		416.	
27.000	99.999	99.999	999.99	225.07	2.14	.25		999.99	99.99	999.99	999.99	0.		389.	
28.000	99.999	99.999	999.99	226.30	2.11	-.03		999.99	99.99	999.99	999.99	0.		360.	
29.000	99.999	99.999	999.99	227.04	2.22	.15		999.99	99.99	999.99	999.99	0.		328.	
30.000	99.999	99.999	999.99	228.59	2.24	-.22		999.99	99.99	999.99	999.99	0.		314.	

TABLE III-9. MOISTURE RELATED STATISTICAL PARAMETERS

SEPTEMBER

STATION - 619320		ASCENSION (WIDE AWAKE)										
Z	VAPOR P	S.D. VP	SKEW VP	TV	S.D.	SKEW TV	DEPT T	S.D. OPT	SKEW OPT	NOBS T+P	NOBS TV	
KM	MEAN MB	MB		MEAN DEG K	S.D. DEG K		MEAN DEG K	DEG K				
.000	19.890	2.052	-.21	299.69	1.23	-.14	290.49	1.67	-.44	365.	365.	
.020	19.754	2.026	-.21	299.79	1.23	-.14	290.38	1.65	-.43	410.	410.	
1.000	13.925	1.714	.12	290.43	.92	.19	294.94	1.88	-.22	409.	410.	
2.000	5.371	2.436	.63	289.94	2.23	-.87	270.11	6.41	-.23	365.	410.	
3.000	3.481	1.354	.47	283.80	1.49	.02	264.72	5.42	-.47	357.	410.	
4.000	1.876	.859	.50	277.25	1.34	.01	255.75	5.09	-.30	302.	410.	
5.000	.873	.425	1.05	272.19	1.38	.21	248.05	5.11	.33	257.	410.	
6.000	.525	.280	1.25	266.83	1.42	.34	242.43	5.21	.39	251.	410.	
7.000	.314	.172	1.08	260.65	1.43	.41	237.10	5.24	.24	265.	410.	
8.000	.180	.037	.82	253.60	1.41	.63	231.64	5.29	-.05	273.	409.	
9.000	.094	.050	.59	245.90	1.60	.66	225.59	5.44	-.54	284.	409.	
10.000	.045	.022	.23	237.79	1.65	.68	219.61	4.73	-.86	254.	409.	
11.000	.020	.007	.34	229.01	1.35	.24	213.62	2.92	-.42	237.	409.	
12.000	.008	.003	.30	221.63	1.31	.04	207.27	2.03	-.41	240.	410.	
13.000	.003	.001	.57	214.22	1.37	.70	199.93	3.15	-.31	117.	409.	
14.000	.001	.000	.39	207.61	1.47	.63	194.40	2.64	-.35	55.	409.	
15.000	99.999	99.999	999.99	202.80	1.29	.32	999.99	99.99	999.99	1.	409.	
16.000	99.999	99.999	999.99	199.47	1.23	-.22	999.99	99.99	999.99	0.	410.	
17.000	99.999	99.999	999.99	199.02	1.67	-.23	999.99	99.99	999.99	0.	405.	
18.000	99.999	99.999	999.99	202.65	2.44	.35	999.99	99.99	999.99	0.	402.	
19.000	99.999	99.999	999.99	206.97	2.27	-.11	999.99	99.99	999.99	0.	403.	
20.000	99.999	99.999	999.99	210.77	2.45	.29	999.99	99.99	999.99	0.	400.	
21.000	99.999	99.999	999.99	213.73	2.73	.61	999.99	99.99	999.99	0.	365.	
22.000	99.999	99.999	999.99	216.02	2.52	.56	999.99	99.99	999.99	0.	383.	
23.000	99.999	99.999	999.99	218.00	2.20	.44	999.99	99.99	999.99	0.	372.	
24.000	99.999	99.999	999.99	219.96	2.18	.15	999.99	99.99	999.99	0.	372.	
25.000	99.999	99.999	999.99	221.88	2.35	.04	999.99	99.99	999.99	0.	368.	
26.000	99.999	99.999	999.99	223.85	2.15	-.09	999.99	99.99	999.99	0.	350.	
27.000	99.999	99.999	999.99	225.51	2.09	-.01	999.99	99.99	999.99	0.	317.	
28.000	99.999	99.999	999.99	226.03	1.99	-.05	999.99	99.99	999.99	0.	314.	
29.000	99.999	99.999	999.99	226.20	2.22	.11	999.99	99.99	999.99	0.	255.	
30.000	99.999	99.999	999.99	230.33	2.06	-.24	999.99	99.99	999.99	0.	251.	

TABLE III-10. MOISTURE RELATED STATISTICAL PARAMETERS

OCTOBER

STATION - 615020		ASCENSION (WIDE AWAKE)			TV		DEWPT T		S.D. OPT		NOBS T+P	NOBS TV
Z	VAPOR P	S.D. VP	SKEN VP	TV	S.D.	SKEN TV	MEAN	S.D. OPT	SKEN OPT			
KM	MB	MB		DEC K	DEC K		DEC K	DEC K				
.000	20.221	2.008	.01	203.99	1.22	.01	290.76	1.06	-.26	388.	388.	
.020	20.097	2.061	.00	209.94	1.20	-.03	290.66	1.04	-.27	427.	427.	
1.000	14.532	1.584	-.14	200.64	.95	.30	265.60	1.80	-.43	432.	433.	
2.000	5.631	2.195	.30	203.93	1.93	-.80	271.72	5.47	-.42	394.	433.	
3.000	3.944	1.571	.08	204.29	1.20	-.16	266.21	5.87	-.61	398.	433.	
4.000	2.139	1.025	.43	277.00	1.19	.35	250.20	6.27	-.24	334.	433.	
5.000	.949	.483	1.01	272.20	1.44	.30	245.83	5.54	.15	292.	433.	
6.000	.535	.273	1.06	200.59	1.49	.18	242.67	5.23	.20	274.	433.	
7.000	.323	.173	1.07	200.57	1.39	.19	237.42	5.16	.25	283.	433.	
8.000	.190	.100	1.52	203.78	1.42	.07	232.13	5.24	.10	287.	433.	
9.000	.080	.049	.58	240.23	1.44	.22	225.15	4.97	-.48	296.	432.	
10.000	.048	.032	.34	233.00	1.45	.41	220.22	4.59	-.96	256.	432.	
11.000	.022	.009	.54	220.91	1.26	.43	214.25	3.22	-.46	225.	432.	
12.000	.009	.003	.33	221.97	1.14	.41	207.78	2.84	-.54	225.	431.	
13.000	.003	.001	.53	214.31	1.13	.32	200.49	3.19	-.44	120.	430.	
14.000	.001	.001	1.08	207.48	1.23	.23	194.18	3.22	-.23	64.	430.	
15.000	.001	.000	.10	201.94	1.34	.35	190.18	3.45	-.43	7.	429.	
16.000	99.920	99.939	99.93	190.45	1.39	-.07	99.99	99.99	99.99	0.	429.	
17.000	99.909	99.933	99.90	107.56	1.86	-.48	99.99	99.99	99.99	0.	427.	
18.000	99.909	99.919	99.90	200.60	2.63	-.11	99.99	99.99	99.99	0.	427.	
19.000	99.907	99.909	99.90	206.30	2.50	-.26	99.99	99.99	99.99	0.	420.	
20.000	99.907	99.900	99.90	209.31	2.52	.34	99.99	99.99	99.99	0.	421.	
21.000	99.909	99.900	99.90	210.36	2.00	.43	99.99	99.99	99.99	0.	406.	
22.000	99.909	99.909	99.90	214.23	2.00	.38	99.99	99.99	99.99	0.	404.	
23.000	99.909	99.900	99.90	217.07	2.47	.17	99.99	99.99	99.99	0.	395.	
24.000	99.909	99.900	99.90	219.43	2.63	.21	99.99	99.99	99.99	0.	395.	
25.000	99.909	99.900	99.90	221.50	2.46	-.27	99.99	99.99	99.99	0.	369.	
26.000	99.909	99.900	99.90	223.60	2.32	-.15	99.99	99.99	99.99	0.	369.	
27.000	99.909	99.900	99.90	225.60	2.26	.09	99.99	99.99	99.99	0.	330.	
28.000	99.909	99.900	99.90	227.62	2.28	.03	99.99	99.99	99.99	0.	326.	
29.000	99.909	99.900	99.90	229.60	2.43	.12	99.99	99.99	99.99	0.	274.	
30.000	99.909	99.900	99.90	232.12	2.32	.05	99.99	99.99	99.99	0.	268.	

TABLE III-11. MOISTURE RELATED STATISTICAL PARAMETERS

NOVEMBER

STATION = 615020		ASCENSION (WIDE AWAKE)											
Z	VAPOR P	S.D. VP	SKW VP	TV	TV	SKW TV	DELT T	S.D. OPT	SKW OPT	NOBS T+P	NOBS TV		
	MEAN			MEAN	S.D.		MEAN						
KM	MB			DEG K	DEG K		DEG K	DEG K					
.000	21.037	2.091	-.30	290.55	1.21	.11	291.33	1.62	-.61	405.	405.		
.020	20.504	2.122	-.35	290.49	1.20	-.05	291.28	1.65	-.66	429.	429.		
1.000	15.008	1.783	-.01	291.19	1.10	.02	296.09	1.84	-.27	429.	430.		
2.000	6.518	2.477	.19	293.49	1.62	-.79	273.04	5.85	-.65	406.	430.		
3.000	4.044	1.630	.18	283.93	1.29	-.18	266.49	6.02	-.63	381.	430.		
4.000	2.005	1.026	.65	278.15	1.34	.20	257.37	6.26	-.03	325.	430.		
5.000	1.012	.544	1.81	272.69	1.43	.03	249.53	5.54	.31	302.	430.		
6.000	.581	.259	1.12	266.78	1.55	.10	243.52	5.27	.20	294.	430.		
7.000	.333	.176	1.02	260.35	1.60	.23	237.73	5.21	.12	293.	430.		
8.000	.191	.105	.07	253.02	1.51	.22	232.18	5.33	-.09	308.	430.		
9.000	.105	.056	.64	246.02	1.05	.16	225.63	5.34	-.54	315.	428.		
10.000	.052	.026	.73	239.00	1.73	.21	220.80	4.83	-.87	274.	426.		
11.000	.022	.009	.45	229.68	1.40	-.18	214.20	3.55	-.63	256.	425.		
12.000	.009	.004	.76	221.62	1.25	-.02	207.71	3.16	-.49	256.	425.		
13.000	.003	.001	.23	214.35	1.27	.23	200.55	3.37	-.60	139.	424.		
14.000	.001	.001	.21	207.71	1.27	.10	194.65	3.18	-.59	99.	424.		
15.000	.001	.000	-.24	201.53	1.46	.25	187.78	2.33	-.60	0.	423.		
16.000	99.999	99.999	999.99	187.88	1.56	-.05	999.99	99.99	999.99	0.	421.		
17.000	99.999	99.999	999.99	183.53	1.74	-.14	999.99	99.99	999.99	0.	415.		
18.000	99.999	99.999	999.99	180.33	2.45	.15	999.99	99.99	999.99	0.	412.		
19.000	99.999	99.999	999.99	203.52	2.49	.16	999.99	99.99	999.99	0.	409.		
20.000	99.999	99.999	999.99	207.60	2.42	.40	999.99	99.99	999.99	0.	406.		
21.000	99.999	99.999	999.99	211.16	2.50	.87	999.99	99.99	999.99	0.	393.		
22.000	99.999	99.999	999.99	213.97	2.35	.59	999.99	99.99	999.99	0.	392.		
23.000	99.999	99.999	999.99	215.41	1.92	.48	999.99	99.99	999.99	0.	387.		
24.000	99.999	99.999	999.99	218.70	2.14	-.03	999.99	99.99	999.99	0.	386.		
25.000	99.999	99.999	999.99	221.03	2.15	-.04	999.99	99.99	999.99	0.	382.		
26.000	99.999	99.999	999.99	223.04	2.07	.05	999.99	99.99	999.99	0.	367.		
27.000	99.999	99.999	999.99	226.53	2.37	.33	999.99	99.99	999.99	0.	334.		
28.000	99.999	99.999	999.99	229.07	2.50	.30	999.99	99.99	999.99	0.	324.		
29.000	99.999	99.999	999.99	231.37	2.52	-.03	999.99	99.99	999.99	0.	266.		
30.000	99.999	99.999	999.99	233.49	2.42	.15	999.99	99.99	999.99	0.	263.		

TABLE III-12. MOISTURE RELATED STATISTICAL PARAMETERS

DECEMBER

STATION = 619020		ASCENSION (WICE ARRIE)		TV		TV		DEPT T		S.D. DPT		NOBS T+P		NOBS TV	
Z	VAPOR P	S.D. VP	SKEM VP	TV	S.D.	SKEM TV	DEPT T	S.D. DPT	SKEM DPT	NOBS T+P	NOBS TV				
KM	MB	MB		DEG K	DEG K		DEG K	DEG K							
1.000	21.076	2.210	-1.19	201.11	1.29	.04	291.60	1.66	-1.43	428.	428.				
2.000	21.071	2.175	-1.16	201.04	1.23	.01	291.79	1.64	-1.43	453.	453.				
3.000	19.079	1.902	-1.07	201.00	1.34	.49	290.34	1.95	-1.48	450.	453.				
4.000	16.744	2.000	-.31	200.00	1.02	-.91	290.03	5.16	-1.47	428.	453.				
5.000	14.431	1.822	.24	200.21	1.41	-.39	290.04	5.32	-1.61	431.	453.				
6.000	12.000	1.101	.44	200.05	1.23	.03	290.72	6.01	-1.35	374.	453.				
7.000	10.014	1.000	1.64	200.49	1.05	.10	291.09	0.13	-.13	341.	453.				
8.000	8.000	1.315	1.00	200.00	1.09	.18	293.04	5.33	-.17	319.	453.				
9.000	6.237	1.178	.73	200.00	1.43	.23	297.91	5.16	-.02	318.	452.				
10.000	4.105	1.000	.64	200.00	1.40	.23	298.40	5.17	-1.04	332.	450.				
11.000	2.101	1.001	-.72	200.01	1.03	.46	299.43	5.17	-1.00	330.	449.				
12.000	0.000	1.000	.02	200.00	1.70	.67	200.51	4.00	-1.31	281.	448.				
13.000	0.000	1.000	.67	200.00	1.36	-.25	214.09	3.03	-1.49	250.	448.				
14.000	0.000	1.000	.69	201.00	1.36	-.12	207.79	2.97	-1.49	250.	447.				
15.000	0.004	1.002	.71	214.35	1.39	-.11	201.36	3.03	-1.48	147.	447.				
16.000	0.002	1.001	.61	207.73	1.50	.33	199.09	2.77	-1.64	S+.	447.				
17.000	0.001	1.000	.05	201.07	1.69	.53	191.53	1.49	-1.10	8.	446.				
18.000	99.000	99.000	99.00	199.00	1.80	.33	000.00	00.00	99.00	0.	446.				
19.000	99.000	99.000	99.00	199.00	1.69	.04	000.00	00.00	99.00	0.	420.				
20.000	99.000	99.000	99.00	197.19	2.67	.75	000.00	00.00	99.00	0.	440.				
21.000	99.000	99.000	99.00	201.09	2.78	-.09	000.00	00.00	99.00	0.	439.				
22.000	99.000	99.000	99.00	200.47	2.56	-.06	000.00	00.00	99.00	0.	436.				
23.000	99.000	99.000	99.00	210.31	2.42	.46	000.00	00.00	99.00	0.	427.				
24.000	99.000	99.000	99.00	213.43	2.26	.40	000.00	00.00	99.00	0.	424.				
25.000	99.000	99.000	99.00	215.70	2.05	.55	000.00	00.00	99.00	0.	420.				
26.000	99.000	99.000	99.00	217.65	2.12	.11	000.00	00.00	99.00	0.	418.				
27.000	99.000	99.000	99.00	210.20	2.06	.14	000.00	00.00	99.00	0.	416.				
28.000	99.000	99.000	99.00	223.05	2.22	.31	000.00	01.00	99.00	0.	407.				
29.000	99.000	99.000	99.00	219.00	2.51	.25	000.00	00.00	99.00	0.	374.				
30.000	99.000	99.000	99.00	219.05	2.64	.44	000.00	00.00	99.00	0.	307.				
31.000	99.000	99.000	99.00	230.05	2.71	.39	000.00	00.00	99.00	0.	293.				
32.000	99.000	99.000	99.00	232.61	2.35	.33	000.00	00.00	99.00	0.	293.				

TABLE III-13. MOISTURE RELATED STATISTICAL PARAMETERS

## ANNUAL

STATION - 015000		ASBESTOS (WIDE AREA)				TV		DOWNT		S.D. DPT		NOBS T+P	NOBS TV
Z	VAR OF P	S.D. VP	S.D. VP	TV	S.D.	SKEW TV	MEAN	S.D. DPT	SKEW DPT				
KM	MM	MM	MM	MM	MM		MM	MM					
100	20.000	3.000	15	201.00	1.91	.03	201.00	2.00	-.20	4924.	4924.		
200	20.000	3.000	17	201.00	1.93	.03	201.00	2.01	-.19	5003.	5003.		
300	20.000	3.000	19	201.00	1.95	.10	201.00	2.33	-.31	5403.	5403.		
400	20.00	3.00	20	201.00	2.22	-.76	201.00	6.40	-.46	5011.	5400.		
500	20.00	3.00	24	201.00	1.96	-.24	201.00	6.31	-.37	4725.	5400.		
600	20.00	3.00	25	201.00	1.97	.07	201.00	6.64	-.05	4091.	5400.		
700	20.00	3.00	26	201.00	1.98	.00	201.00	6.11	.43	3500.	5400.		
800	20.00	3.00	27	201.00	1.92	.08	201.00	5.69	.44	3473.	5400.		
900	20.00	3.00	28	201.00	1.94	.10	201.00	5.90	.27	3400.	5400.		
1000	20.00	3.00	29	201.00	1.96	.30	201.00	5.91	.00	3400.	5400.		
1100	20.00	3.00	30	201.00	1.95	.48	201.00	5.42	-.13	3770.	5400.		
1200	20.00	3.00	31	201.00	1.90	.55	201.00	4.73	-.00	3407.	5400.		
1300	20.00	3.00	32	201.00	1.93	.25	201.00	3.35	-.25	2400.	5400.		
1400	20.00	3.00	33	201.00	1.93	.10	201.00	2.87	-.29	2818.	5400.		
1500	20.00	3.00	34	201.00	1.90	.28	201.00	3.13	-.40	1536.	5400.		
1600	20.00	3.00	35	201.00	1.95	.39	201.00	2.03	-.42	951.	5400.		
1700	20.00	3.00	36	201.00	1.95	.33	201.00	2.00	-.50	72.	5400.		
1800	20.00	3.00	37	201.00	1.94	.02	201.00	2.00	-.50	0.	5400.		
1900	20.00	3.00	38	201.00	2.50	.16	201.00	2.00	-.50	0.	5400.		
2000	20.00	3.00	39	201.00	3.00	.11	201.00	2.00	-.50	0.	5400.		
2100	20.00	3.00	40	201.00	3.00	.00	201.00	2.00	-.50	0.	5400.		
2200	20.00	3.00	41	201.00	3.00	.04	201.00	2.00	-.50	0.	5400.		
2300	20.00	3.00	42	201.00	3.00	.24	201.00	2.00	-.50	0.	5400.		
2400	20.00	3.00	43	201.00	2.70	.18	201.00	2.00	-.50	0.	5400.		
2500	20.00	3.00	44	201.00	2.50	.12	201.00	2.00	-.50	0.	5400.		
2600	20.00	3.00	45	201.00	2.75	.04	201.00	2.00	-.50	0.	5400.		
2700	20.00	3.00	46	201.00	2.82	-.11	201.00	2.00	-.50	0.	5400.		
2800	20.00	3.00	47	201.00	2.67	-.14	201.00	2.00	-.50	0.	5400.		
2900	20.00	3.00	48	201.00	2.63	-.04	201.00	2.00	-.50	0.	5400.		
3000	20.00	3.00	49	201.00	2.57	.00	201.00	2.00	-.50	0.	5400.		
3100	20.00	3.00	50	201.00	2.69	.02	201.00	2.00	-.50	0.	5400.		
3200	20.00	3.00	51	201.00	2.62	-.18	201.00	2.00	-.50	0.	5400.		

TABLE IV-1. HYDROSTATIC MODEL ATMOSPHERE

JANUARY

STATION = 615020		ASCENSION (WIDE AWAKE)		
Z	GEO. HT.	P	D	TV
KM	KM	MB	G/M3	DEG K
.000	.000	1008.5000	1161.0000	302.02
.020	.020	1004.3000	1159.0000	301.92
1.000	.697	997.6300	1067.0000	275.00
2.000	1.634	798.6500	953.2000	260.05
3.000	2.671	700.4100	833.3000	254.63
4.000	3.687	620.5000	787.7000	277.93
5.000	4.693	555.4000	710.3000	272.42
6.000	5.678	460.0300	633.1000	265.63
7.000	6.674	430.3000	575.6000	260.33
8.000	7.669	377.0300	516.4000	253.39
9.000	8.664	329.0400	460.3000	245.02
10.000	9.653	285.0000	418.7000	237.91
11.000	10.633	247.2600	375.1000	229.05
12.000	11.643	212.7400	333.0700	221.55
13.000	12.640	182.1100	295.5000	214.68
14.000	13.633	155.1000	259.7000	208.06
15.000	14.626	131.4600	226.5000	202.16
16.000	15.618	110.0000	195.5000	197.71
17.000	16.611	93.3700	165.5000	193.43
18.000	17.603	78.6500	139.2000	189.52
19.000	18.604	66.2400	114.8000	200.90
20.000	19.613	56.0700	94.0000	205.69
21.000	20.677	47.6300	79.2300	209.47
22.000	21.637	40.6770	66.5000	213.29
23.000	22.653	34.6260	56.2400	214.49
24.000	23.648	29.5370	47.0500	216.40
25.000	24.637	25.3350	40.3500	218.51
26.000	25.627	21.7230	34.7500	221.00
27.000	26.610	18.0000	29.0700	223.04
28.000	27.705	16.0570	24.7400	223.07
29.000	28.703	13.0700	21.1100	223.44
30.000	29.781	11.9000	18.0000	220.49
32.000	31.757	8.0317	13.3000	233.67
34.000	33.731	6.7061	9.9130	225.94
36.000	35.704	5.0584	7.3470	241.15
38.000	37.676	3.6375	5.4510	246.59
40.000	39.646	2.9512	4.0570	253.04
42.000	41.615	2.2531	3.0220	259.85
44.000	43.583	1.7475	2.3030	265.53
46.000	45.550	1.3373	1.7800	267.13
48.000	47.518	1.0566	1.3790	269.38
50.000	49.480	.8234	1.0592	269.84
52.000	51.443	.6423	.8320	270.09
54.000	53.405	.5009	.6517	269.21
56.000	55.366	.3903	.5107	267.66
58.000	57.325	.3034	.4020	263.91
60.000	59.283	.2350	.3174	259.26
62.000	61.240	.1812	.2463	254.93
64.000	63.198	.1391	.1946	250.30
66.000	65.150	.1059	.1547	239.71



TABLE IV-2. HYDROSTATIC MODEL ATMOSPHERE

FEBRUARY

STATION • 618020		ASCENSION (WIDE AREA)		
Z	GEO. HT.	P	D	TV
KM	KM	MB	GM3	°C K
0.000	0.000	1006.3000	1157.0000	323.10
0.000	0.020	1004.0200	1154.0000	322.93
1.000	1.007	897.0000	1054.0000	277.00
2.000	1.954	790.0100	953.0000	232.17
3.000	2.881	709.0100	853.0000	194.50
4.000	3.787	639.7000	767.0000	160.05
5.000	4.683	580.0000	703.0000	128.92
6.000	5.579	529.0000	659.0000	101.42
7.000	6.474	480.0000	629.0000	78.81
8.000	7.360	437.0000	617.0000	58.02
9.000	8.236	390.0000	605.0000	39.42
10.000	9.106	340.0000	610.0000	22.45
11.000	9.965	297.0000	637.0000	7.10
12.000	10.816	253.0000	684.0000	-13.32
13.000	11.660	208.0000	750.0000	-24.67
14.000	12.493	163.0000	836.0000	-37.66
15.000	13.316	118.0000	943.0000	-52.03
16.000	14.128	73.0000	1070.0000	-67.55
17.000	14.931	27.0000	1216.0000	-84.00
18.000	15.723	0.0000	1380.0000	-101.00
19.000	16.504	0.0000	1560.0000	-118.00
20.000	17.273	0.0000	1750.0000	-135.00
21.000	18.037	0.0000	1950.0000	-152.00
22.000	18.797	0.0000	2160.0000	-169.00
23.000	19.551	0.0000	2380.0000	-186.00
24.000	20.300	0.0000	2610.0000	-203.00
25.000	21.043	0.0000	2850.0000	-220.00
26.000	21.781	0.0000	3100.0000	-237.00
27.000	22.513	0.0000	3360.0000	-254.00
28.000	23.240	0.0000	3630.0000	-271.00
29.000	23.961	0.0000	3910.0000	-288.00
30.000	24.677	0.0000	4200.0000	-305.00
31.000	25.387	0.0000	4500.0000	-322.00
32.000	26.091	0.0000	4810.0000	-339.00
33.000	26.790	0.0000	5130.0000	-356.00
34.000	27.483	0.0000	5460.0000	-373.00
35.000	28.171	0.0000	5800.0000	-390.00
36.000	28.853	0.0000	6150.0000	-407.00
37.000	29.530	0.0000	6510.0000	-424.00
38.000	30.201	0.0000	6880.0000	-441.00
39.000	30.866	0.0000	7260.0000	-458.00
40.000	31.525	0.0000	7650.0000	-475.00
41.000	32.178	0.0000	8050.0000	-492.00
42.000	32.825	0.0000	8460.0000	-509.00
43.000	33.466	0.0000	8880.0000	-526.00
44.000	34.101	0.0000	9310.0000	-543.00
45.000	34.730	0.0000	9750.0000	-560.00
46.000	35.353	0.0000	10200.0000	-577.00
47.000	35.970	0.0000	10660.0000	-594.00
48.000	36.581	0.0000	11130.0000	-611.00
49.000	37.186	0.0000	11610.0000	-628.00
50.000	37.785	0.0000	12100.0000	-645.00
51.000	38.378	0.0000	12600.0000	-662.00
52.000	38.965	0.0000	13110.0000	-679.00
53.000	39.546	0.0000	13630.0000	-696.00
54.000	40.121	0.0000	14160.0000	-713.00
55.000	40.690	0.0000	14700.0000	-730.00
56.000	41.253	0.0000	15250.0000	-747.00
57.000	41.810	0.0000	15810.0000	-764.00
58.000	42.361	0.0000	16380.0000	-781.00
59.000	42.906	0.0000	16960.0000	-798.00
60.000	43.445	0.0000	17550.0000	-815.00
61.000	43.978	0.0000	18150.0000	-832.00
62.000	44.505	0.0000	18760.0000	-849.00
63.000	45.026	0.0000	19380.0000	-866.00
64.000	45.541	0.0000	20010.0000	-883.00
65.000	46.050	0.0000	20650.0000	-900.00
66.000	46.553	0.0000	21300.0000	-917.00

TABLE IV-3. HYDROSTATIC MODEL ATMOSPHERE

## MARCH

STATION # 619020		ASCENSION (HIDE ANAKE)		
Z	DEC. HT.	P	D	TV
KM	KM	MB	G/M3	DEG K
.000	.000	1006.0000	1153.0000	303.92
.020	.020	1003.7000	1151.0000	303.78
1.000	.997	697.7500	1062.0000	294.58
2.000	1.994	703.9900	960.0000	289.94
3.000	2.991	709.6700	869.1000	284.44
4.000	3.987	628.8400	785.5000	278.52
5.000	4.983	535.6500	703.1000	273.09
6.000	5.979	490.1200	638.4000	267.46
7.000	6.974	430.8500	574.5000	261.19
8.000	7.969	377.7200	517.1000	254.45
9.000	8.964	329.0500	464.9000	247.18
10.000	9.958	286.0500	417.7000	239.26
11.000	10.953	248.2600	374.6000	230.86
12.000	11.946	213.7500	334.3000	222.76
13.000	12.940	183.0400	296.7000	214.91
14.000	13.933	155.6000	261.6000	207.60
15.000	14.926	132.0000	229.3000	201.49
16.000	15.918	111.3100	197.0000	197.00
17.000	16.911	93.0500	167.5000	194.65
18.000	17.903	78.7900	139.6000	193.57
19.000	18.894	66.4500	115.1000	201.22
20.000	19.886	56.2710	95.2500	205.80
21.000	20.877	47.9070	79.4100	209.60
22.000	21.867	40.7330	66.6000	212.11
23.000	22.858	34.7070	56.1300	215.72
24.000	23.848	29.7650	47.5200	218.19
25.000	24.837	25.5120	40.3300	210.39
26.000	25.827	21.9030	34.2500	222.61
27.000	26.816	18.8260	29.1300	225.22
28.000	27.805	16.2260	24.8200	227.75
29.000	28.793	14.0010	21.2000	230.10
30.000	29.781	12.0335	18.1600	232.10
32.000	31.757	9.0649	13.4100	235.53
34.000	33.731	6.0250	9.9290	239.61
36.000	35.704	5.1635	7.3350	244.60
38.000	37.676	3.9379	5.4560	251.60
40.000	39.646	3.0265	4.0620	259.73
42.000	41.615	2.3436	3.0670	256.33
44.000	43.593	1.8244	2.3500	270.61
46.000	45.590	1.4242	1.8240	272.11
48.000	47.516	1.1123	1.4250	271.27
50.000	49.480	.8677	1.1230	269.31
52.000	51.443	.6755	.8335	265.52
54.000	53.405	.5279	.6032	264.28
56.000	55.366	.4069	.5423	261.43
58.000	57.325	.3143	.4252	257.67
60.000	59.283	.2420	.3520	254.07
62.000	61.240	.1836	.2862	249.57
64.000	63.195	.1415	.2006	243.40
66.000	65.150	.1072	.1572	237.33

TABLE IV-4. HYDROSTATIC MODEL ATMOSPHERE

APRIL

STATION = 619020		ASCENSION (WIDE AWAKE)		
Z	GEO. HT.	P	D	TV
KM	KM	MB	G/MB	°C K
0.000	0.000	1000.0000	1153.0000	303.83
1.000	0.020	1000.0000	1151.0000	303.87
2.000	0.097	937.8100	1062.0000	294.57
3.000	1.234	793.0700	950.7000	290.05
4.000	2.931	709.8100	869.0000	284.07
5.000	3.997	629.0900	785.4000	279.05
6.000	4.993	556.2000	708.1000	273.53
7.000	5.979	490.5100	630.2000	267.75
8.000	6.974	431.2700	574.2000	261.66
9.000	7.929	379.2000	516.3000	255.16
10.000	8.931	320.4200	464.1000	249.03
11.000	9.958	267.4800	417.2000	240.07
12.000	10.953	248.9200	374.5000	231.05
13.000	11.946	214.4000	334.4000	223.36
14.000	12.940	183.6700	297.1000	215.34
15.000	13.933	155.4000	262.4000	207.71
16.000	14.925	132.5000	229.0000	201.00
17.000	15.918	111.7000	198.0000	193.23
18.000	16.911	93.9170	169.2000	184.10
19.000	17.903	78.0000	140.0000	170.54
20.000	18.884	63.0000	115.0000	151.77
21.000	19.870	50.0000	95.1000	135.49
22.000	20.877	47.0710	79.3400	119.03
23.000	21.857	40.0000	66.0000	104.20
24.000	22.803	34.0000	56.0000	91.70
25.000	23.648	29.0000	47.0000	80.00
26.000	24.007	25.7100	40.0000	70.53
27.000	25.827	22.1000	34.0000	63.00
28.000	26.816	19.0000	29.0000	57.00
29.000	27.605	16.4100	24.9000	52.25
30.000	28.793	14.1770	21.3400	48.50
31.000	29.781	12.0000	18.0000	45.47
32.000	31.757	9.2000	13.5000	37.00
33.000	33.731	6.9000	9.5000	29.00
34.000	35.704	5.2000	7.4100	24.00
35.000	37.676	4.0300	5.9000	20.00
36.000	39.646	3.1000	4.1400	16.00
37.000	41.615	2.4000	3.1500	12.00
38.000	43.583	1.8000	2.4100	9.00
39.000	45.550	1.4500	1.8700	7.00
40.000	47.516	1.1700	1.4000	5.00
41.000	49.460	0.9200	1.1400	4.00
42.000	51.403	0.6700	0.9000	3.00
43.000	53.405	0.5300	0.7000	2.00
44.000	55.359	0.4100	0.5400	1.00
45.000	57.305	0.3100	0.4300	0.00
46.000	59.283	0.2400	0.3300	0.00
47.000	61.240	0.1800	0.2400	0.00
48.000	63.156	0.1400	0.1800	0.00
49.000	65.150	0.1000	0.1300	0.00

TABLE IV-5. HYDROSTATIC MODEL ATMOSPHERE

MAY

STATION = 619020		ASCENSION (WIDE AREA)		
Z	GEO. HT.	P	D	TV
KM	KM	MB	G/M3	DEG K
.000	.000	1007.4000	1157.0000	303.29
.020	.020	1005.2000	1155.0000	303.16
1.000	.027	823.7800	1055.0000	273.67
2.000	1.024	752.6000	993.0000	263.17
3.000	2.991	710.1000	930.0000	254.24
4.000	3.937	670.4000	869.0000	247.24
5.000	4.903	636.5000	809.0000	241.23
6.000	5.979	600.8000	750.0000	236.76
7.000	6.974	571.0000	694.0000	231.65
8.000	7.939	539.4000	640.0000	225.20
9.000	8.874	506.0000	589.0000	218.08
10.000	9.950	477.6000	541.0000	210.14
11.000	10.953	449.0000	496.0000	201.43
12.000	11.946	424.5000	454.0000	192.06
13.000	12.940	403.7800	417.0000	182.29
14.000	13.933	385.5000	382.0000	172.75
15.000	14.926	369.6000	349.0000	162.51
16.000	15.918	355.8000	319.0000	151.90
17.000	16.911	344.1000	291.0000	140.28
18.000	17.903	334.2000	266.0000	128.01
19.000	18.894	325.8000	243.0000	115.79
20.000	19.885	318.7000	222.0000	103.50
21.000	20.877	312.5000	203.0000	91.59
22.000	21.867	307.1000	185.0000	79.07
23.000	22.859	302.4000	169.0000	67.00
24.000	23.843	298.3000	154.0000	55.57
25.000	24.827	294.8000	140.0000	44.29
26.000	25.827	291.8000	127.0000	33.65
27.000	26.816	289.3000	115.0000	23.59
28.000	27.800	287.3000	104.0000	14.02
29.000	28.793	285.7000	94.0000	4.00
30.000	29.791	284.4000	85.0000	-6.00
32.000	31.757	279.5000	65.0000	-26.13
34.000	33.731	275.0000	47.0000	-43.19
36.000	35.704	271.0000	31.0000	-59.78
38.000	37.676	267.5000	17.0000	-74.34
40.000	39.646	264.5000	5.0000	-87.34
42.000	41.615	262.0000	0.0000	-98.46
44.000	43.583	260.0000	0.0000	-107.04
46.000	45.550	258.5000	0.0000	-114.45
48.000	47.516	257.5000	0.0000	-120.60
50.000	49.480	256.8000	0.0000	-125.66
52.000	51.443	256.4000	0.0000	-129.77
54.000	53.405	256.2000	0.0000	-133.33
56.000	55.366	256.1000	0.0000	-136.31
58.000	57.325	256.1000	0.0000	-138.11
60.000	59.283	256.2000	0.0000	-139.62
62.000	61.240	256.4000	0.0000	-140.24
64.000	63.196	256.7000	0.0000	-140.96
66.000	65.150	257.1000	0.0000	-141.66

TABLE IV-6. HYDROSTATIC MODEL ATMOSPHERE

JUNI

STATION = 610020		ASCENSION (WIDE AREA)		
Z	GEO. HT.	P	D	TV
KM	KM	MB	G/M <sup>3</sup>	CEG K
0.000	0.000	1009.1000	1164.0000	302.03
0.020	0.020	1006.9000	1162.0000	301.94
1.000	0.937	929.3700	1072.0000	292.45
2.000	1.904	800.1700	959.3000	287.15
3.000	2.991	710.3500	870.1000	284.40
4.000	3.997	629.4700	787.4000	282.47
5.000	4.993	556.3300	710.7000	282.30
6.000	5.979	490.4400	633.9000	287.00
7.000	6.974	431.1700	575.4000	286.84
8.000	7.969	377.6100	517.5000	284.33
9.000	8.964	329.0200	465.5000	246.96
10.000	9.953	285.9100	419.1000	230.60
11.000	10.933	246.2300	375.1000	230.26
12.000	11.946	213.6400	334.9000	222.25
13.000	12.940	182.0900	295.9000	214.56
14.000	13.933	155.7300	261.3000	207.63
15.000	14.925	131.9700	227.5000	202.03
16.000	15.918	111.4100	195.0000	190.41
17.000	16.911	93.8740	165.5000	197.45
18.000	17.903	79.1000	137.7000	200.35
19.000	18.894	66.9330	113.6000	205.01
20.000	19.885	56.8320	94.6000	203.41
21.000	20.877	48.4550	79.3000	210.74
22.000	21.857	41.3710	65.8500	215.62
23.000	22.839	35.3540	56.5000	218.04
24.000	23.848	30.3330	47.8000	220.66
25.000	24.837	26.0480	40.6600	203.03
26.000	25.827	22.4010	34.5000	202.17
27.000	26.815	19.2000	29.5000	224.63
28.000	27.805	16.6370	25.3000	217.53
29.000	28.793	14.3550	21.7800	220.55
30.000	29.781	12.4034	18.6200	221.00
32.000	31.757	9.3017	13.7000	237.14
34.000	33.731	7.0002	10.1500	242.14
36.000	35.704	5.3708	7.5500	246.53
38.000	37.676	4.0645	5.6390	251.25
40.000	39.646	3.1176	4.2600	255.69
42.000	41.615	2.4074	3.2720	260.14
44.000	43.593	1.8507	2.4650	264.05
46.000	45.550	1.4423	1.8750	263.33
48.000	47.516	1.1220	1.4060	267.76
50.000	49.480	.8732	1.1410	267.52
52.000	51.443	.6753	.8843	265.81
54.000	53.405	.5273	.7002	253.94
56.000	55.365	.4082	.5722	259.50
58.000	57.325	.3146	.4724	264.72
60.000	59.285	.2412	.3897	260.53
62.000	61.240	.1875	.3200	244.10
64.000	63.196	.1425	.2670	254.16
65.000	65.150	.1037	.1602	226.41

TABLE IV-7. HYDROSTATIC MODEL ATMOSPHERE

JULY

STATION # 618020		ASCENSION (WIDE AWAKE)		
Z	GEO. HT.	P	D	TV
KM	KM	MB	G/M3	DEG K
.000	.000	1010.4000	1170.0000	230.00
.020	.020	1008.1000	1167.0000	230.00
1.000	.597	900.6000	1077.0000	231.41
2.000	1.924	800.5400	972.1000	205.68
3.000	2.991	710.4500	873.0000	203.51
4.000	3.587	629.3000	783.0000	277.03
5.000	4.993	555.1300	710.6000	272.53
6.000	5.379	490.2300	640.0000	263.62
7.000	6.974	430.9000	576.5000	253.40
8.000	7.909	377.4900	519.1000	253.34
9.000	8.934	329.4200	467.1000	245.66
10.000	9.958	286.2100	419.7000	237.55
11.000	10.953	247.4400	376.2000	229.12
12.000	11.946	212.8100	335.0000	221.32
13.000	12.940	182.0000	296.4000	213.59
14.000	13.933	155.0000	260.1000	207.64
15.000	14.925	131.0000	225.0000	202.02
16.000	15.918	110.0000	193.9000	193.37
17.000	16.911	93.0000	163.6000	183.26
18.000	17.903	79.1200	135.9000	202.53
19.000	18.894	67.0000	112.0000	207.03
20.000	19.885	57.0300	94.2000	210.93
21.000	20.877	48.0000	79.1000	214.01
22.000	21.867	41.0000	66.0000	218.20
23.000	22.859	35.0000	55.7000	219.03
24.000	23.840	30.4700	46.2000	220.02
25.000	24.837	26.1510	41.0000	222.13
26.000	25.827	22.4770	34.9100	224.29
27.000	26.816	19.3450	29.7000	226.19
28.000	27.805	16.6690	25.5300	227.49
29.000	28.793	14.3740	21.9100	228.59
30.000	29.781	12.4078	18.7700	230.33
32.000	31.757	9.2828	13.7600	234.96
34.000	33.731	6.2053	10.1000	239.34
36.000	35.704	5.2832	7.5720	243.26
38.000	37.676	4.0162	5.6300	246.62
40.000	39.646	3.0753	4.2160	254.23
42.000	41.615	2.3563	3.1870	258.93
44.000	43.583	1.8292	2.4220	263.37
46.000	45.550	1.4200	1.8520	267.39
48.000	47.516	1.1052	1.4380	263.44
50.000	49.480	.8608	1.1100	253.42
52.000	51.443	.6702	.8732	237.63
54.000	53.405	.5211	.6820	224.00
56.000	55.366	.4040	.5331	201.34
58.000	57.325	.3120	.4337	255.64
60.000	59.283	.2399	.3320	231.27
62.000	61.240	.1832	.2521	243.71
64.000	63.193	.1380	.2054	273.32
66.000	65.150	.1040	.1576	230.16

TABLE IV-8. HYDROSTATIC MODEL ATMOSPHERE

AUGUST

STATION • 819020		ASCENSION (WIDE AREA)			
Z	GEO. HT.	P	D	TV	
KM	KM	MG	G/M <sup>2</sup>	CM K	
.000	.000	1010.6000	1173.0000	250.15	
.000	.000	1009.3000	1171.0000	250.67	
1.000	.997	900.5000	1070.0000	250.62	
2.000	1.994	800.4000	989.4000	251.65	
3.000	2.991	710.5400	912.0000	252.70	
4.000	3.987	629.4000	839.6000	253.60	
5.000	4.983	555.1600	771.0000	254.43	
6.000	5.979	489.2400	706.0000	255.28	
7.000	6.974	430.0000	643.0000	256.04	
8.000	7.959	377.5000	581.0000	256.65	
9.000	8.954	329.5000	520.0000	257.00	
10.000	9.953	286.3000	469.0000	257.19	
11.000	10.953	247.5000	426.0000	257.33	
12.000	11.946	212.9700	384.7000	257.67	
13.000	12.940	182.8700	346.3000	258.32	
14.000	13.933	155.2100	309.1000	258.60	
15.000	14.925	131.5000	273.0000	258.62	
16.000	15.918	111.1700	238.0000	258.72	
17.000	16.911	93.8100	203.0000	258.80	
18.000	17.903	79.0000	168.0000	258.94	
19.000	18.896	67.2000	142.0000	259.41	
20.000	19.896	57.1700	124.3700	261.18	
21.000	20.877	48.7000	109.0000	264.00	
22.000	21.857	41.1000	97.0000	266.10	
23.000	22.858	35.0000	87.0000	267.04	
24.000	23.849	30.0000	78.0000	267.87	
25.000	24.837	26.0000	71.0000	268.40	
26.000	25.827	22.0000	65.0000	268.42	
27.000	26.816	19.3000	59.0000	268.07	
28.000	27.805	16.6600	53.0000	268.30	
29.000	28.793	14.3000	47.0000	267.64	
30.000	29.781	12.3900	41.0000	268.09	
32.000	31.757	9.2600	33.7100	264.53	
34.000	33.731	6.9000	26.1400	260.70	
35.000	35.704	5.2000	20.0000	263.10	
37.000	37.676	4.0000	15.0000	260.60	
40.000	39.646	3.0600	11.7200	255.00	
42.000	41.615	2.3600	9.1400	250.95	
44.000	43.583	1.8200	7.0000	246.20	
46.000	45.550	1.4200	5.3200	239.79	
48.000	47.516	1.1100	4.2400	230.63	
50.000	49.480	.8600	3.1100	219.60	
52.000	51.443	.6700	2.0700	207.23	
54.000	53.405	.5200	1.3000	203.91	
56.000	55.366	.4000	.9400	200.07	
58.000	57.325	.3100	.7200	193.03	
60.000	59.283	.2400	.5300	180.53	
62.000	61.240	.1800	.3900	165.25	
64.000	63.195	.1300	.2800	148.73	
66.000	65.150	.1000	.2000	132.16	

TABLE IV-9. HYDROSTATIC MODEL ATMOSPHERE

SEPTEMBER

STATION = 619020		ASCENSION (WIDE AWAKE)			
Z	GEO. HT.	P	D	TV	
KM	KM	MB	G/M3	DEG K	
.000	.000	1010.3000	1174.0000	299.83	
.020	.020	1008.0000	1171.0000	299.79	
1.000	.997	900.1700	1080.0000	293.43	
2.000	1.994	830.3500	974.0000	289.94	
3.000	2.991	710.6100	872.0000	283.50	
4.000	3.987	623.4100	750.0000	277.35	
5.000	4.983	556.0500	711.7000	272.19	
6.000	5.979	493.1500	639.0000	265.83	
7.000	6.974	430.6500	575.0000	260.05	
8.000	7.959	377.5000	518.0000	253.60	
9.000	8.954	329.4700	468.0000	245.30	
10.000	9.959	283.3000	419.4000	237.79	
11.000	10.953	247.0000	375.6000	229.51	
12.000	11.946	212.9700	334.0000	221.63	
13.000	12.940	182.0000	293.4000	214.22	
14.000	13.933	155.1600	260.1000	207.01	
15.000	14.926	131.5500	226.0000	200.00	
16.000	15.918	111.1400	194.1000	193.47	
17.000	16.911	93.7540	164.1000	189.02	
18.000	17.903	79.1370	136.1000	185.63	
19.000	18.894	67.1240	113.0000	183.37	
20.000	19.886	57.0770	94.3400	181.77	
21.000	20.877	48.6520	79.3000	181.79	
22.000	21.867	41.5710	67.0400	181.62	
23.000	22.858	35.5700	56.8400	181.00	
24.000	23.848	30.4760	48.2700	181.55	
25.000	24.837	26.1540	41.0600	181.09	
26.000	25.827	22.4720	34.9700	183.85	
27.000	26.816	19.3350	29.9700	185.51	
28.000	27.805	16.6530	25.0700	186.63	
29.000	28.793	14.3560	21.0100	186.26	
30.000	29.781	12.3310	18.7400	186.33	
32.000	31.757	9.2776	13.6000	186.24	
34.000	33.731	6.9958	10.0000	184.53	
36.000	35.704	5.3062	7.4340	184.11	
38.000	37.676	4.0565	5.5730	183.53	
40.000	39.646	3.1190	4.2010	183.63	
42.000	41.615	2.4004	3.1970	182.52	
44.000	43.583	1.8693	2.4340	187.48	
46.000	45.550	1.4561	1.8770	187.27	
48.000	47.516	1.1265	1.4560	187.93	
50.000	49.480	.8979	1.1400	187.19	
52.000	51.443	.6924	.8933	186.41	
54.000	53.405	.5333	.7075	185.16	
56.000	55.366	.4175	.5574	183.63	
58.000	57.325	.3224	.4370	183.04	
60.000	59.283	.2479	.3424	182.19	
62.000	61.240	.1806	.2674	187.02	
64.000	63.196	.1444	.2067	184.40	
66.000	65.150	.1093	.1615	185.63	



TABLE IV-10. HYDROSTATIC MODEL ATMOSPHERE

OCTOBER

STATION = 619020		ASCENSION (WIDE AREA)		
Z	GEO. HT.	P	D	TV
KM	KM	MG	G/M3	CG K
.000	.000	1009.1000	1172.0000	255.93
.020	.020	1006.8000	1169.0000	255.94
1.000	.937	899.1000	1078.0000	250.64
2.000	1.834	793.0000	989.0000	243.93
3.000	2.691	710.0000	879.0000	234.23
4.000	3.527	653.1700	789.0000	227.80
5.000	4.353	613.0000	711.0000	222.20
6.000	5.179	489.9000	640.0000	205.50
7.000	6.074	430.5700	575.0000	200.57
8.000	7.003	377.3000	510.0000	207.79
9.000	8.034	330.3000	456.0000	245.25
10.000	9.058	286.2000	413.0000	239.20
11.000	10.073	247.0000	375.0000	270.51
12.000	11.045	213.0000	339.0000	281.97
13.000	12.040	182.3000	303.0000	214.31
14.000	13.033	155.2700	269.0000	207.43
15.000	14.026	131.5000	227.0000	201.94
16.000	15.018	111.0500	193.0000	193.45
17.000	16.011	93.5680	165.0000	197.55
18.000	17.003	78.9400	137.0000	200.60
19.000	18.004	66.8000	113.4000	205.30
20.000	19.005	56.7300	94.4000	206.31
21.000	20.077	48.3190	79.2700	212.30
22.000	21.057	41.2730	65.3700	214.83
23.000	22.058	35.2550	56.0500	217.07
24.000	23.048	30.1930	47.9400	219.45
25.000	24.037	25.9030	40.7400	221.50
26.000	25.027	22.2530	34.6700	223.00
27.000	26.018	19.1450	29.0000	225.00
28.000	27.005	16.4050	25.0000	217.02
29.000	28.003	14.2320	21.5700	209.03
30.000	29.081	12.2073	18.4500	222.12
32.000	31.757	9.2252	13.9400	236.23
34.000	33.731	6.8715	10.0500	242.40
36.000	35.704	5.2076	7.4500	249.45
38.000	37.678	4.0510	5.5310	253.77
40.000	39.645	3.1162	4.2010	252.03
42.000	41.615	2.4109	3.1010	254.05
44.000	43.580	1.8743	2.4350	250.10
46.000	45.550	1.4621	1.8700	252.03
48.000	47.516	1.1427	1.4040	252.91
50.000	49.400	.8731	1.1400	251.73
52.000	51.443	.6559	.9057	258.53
54.000	53.405	.5425	.7120	266.02
56.000	55.335	.4209	.5521	261.72
58.000	57.325	.3253	.4405	263.15
60.000	59.283	.2505	.3451	253.70
62.000	61.240	.1910	.2714	257.93
64.000	63.195	.1459	.2123	250.92
66.000	65.150	.1099	.1648	253.08

TABLE IV-11. HYDROSTATIC MODEL ATMOSPHERE

NOVEMBER

STATION = 619020		ASCENSION (WIDE AREA)		
Z	GEOM. HT.	P	D	TV
KM	KM	MB	G/MB	SEC K
0.000	0.000	1005.0000	1159.0000	200.00
0.000	0.000	1005.7000	1168.0000	200.49
1.000	0.997	697.3700	1075.0000	291.19
2.000	1.994	799.9300	931.0000	283.48
3.000	2.991	709.4700	870.0000	282.93
4.000	3.987	628.0000	787.0000	278.15
5.000	4.983	553.0100	703.0000	278.62
6.000	5.979	493.0100	630.0000	278.70
7.000	6.974	430.0000	575.0000	278.31
8.000	7.969	377.0700	510.0000	278.02
9.000	8.964	329.1100	408.0000	278.02
10.000	9.958	285.0000	418.0000	278.00
11.000	10.953	247.3400	375.1000	278.03
12.000	11.946	212.8000	334.2000	278.02
13.000	12.940	182.1200	298.0000	278.05
14.000	13.933	155.0000	250.1000	277.71
15.000	14.925	131.4200	226.7000	278.60
16.000	15.918	110.9100	193.3000	197.03
17.000	16.911	93.4000	165.0000	165.03
18.000	17.903	78.6010	137.0000	150.03
19.000	18.894	65.4000	113.0000	203.02
20.000	19.886	56.0770	94.0000	207.60
21.000	20.877	47.9770	70.1000	211.18
22.000	21.867	40.0100	60.0000	213.97
23.000	22.853	34.0000	55.0000	216.01
24.000	23.848	29.9500	47.0700	216.70
25.000	24.837	25.0000	40.4400	221.00
26.000	25.827	22.0430	34.3400	223.04
27.000	26.816	18.9600	28.1000	220.30
28.000	27.803	16.3540	24.8700	229.07
29.000	28.793	14.1230	21.2600	231.37
30.000	29.781	12.2141	18.0200	233.49
32.000	31.757	9.1723	13.4700	233.01
34.000	33.731	6.9275	9.0000	242.38
35.000	35.704	5.2500	7.4000	247.16
36.000	37.676	4.0189	5.5000	253.45
40.000	39.646	3.0925	4.1540	260.29
42.000	41.615	2.3551	3.1470	263.09
44.000	43.583	1.8533	2.4170	269.48
46.000	45.550	1.4533	1.8730	271.26
48.000	47.516	1.1347	1.4610	271.48
50.000	49.480	.8825	1.1470	267.72
52.000	51.443	.6070	.9013	257.00
54.000	53.405	.5004	.7076	254.90
56.000	55.365	.4159	.5500	261.04
58.000	57.325	.3211	.4032	257.00
60.000	59.283	.2473	.3200	254.41
62.000	61.240	.1804	.2582	246.02
64.000	63.196	.1429	.2103	239.16
65.000	65.150	.1091	.1660	237.48

TABLE IV-12. HYDROSTATIC MODEL ATMOSPHERE

DECEMBER

STATION = 616000		ACCELERATION UNITS		REF.
Z	DEG. HT.	P	C	TV
KM	KM	PO	CM	CM
0.000	0.000	1007.7500	1165.7000	120.41
0.000	0.000	1007.7500	1165.7000	120.41
1.000	1.000	870.0000	1070.0000	111.70
2.000	1.994	760.0000	950.0000	100.00
3.000	2.991	700.0000	850.0000	94.21
4.000	3.987	670.0000	770.0000	89.80
5.000	4.983	650.0000	710.0000	86.00
6.000	5.979	630.0000	660.0000	82.70
7.000	6.974	610.0000	620.0000	79.80
8.000	7.969	590.0000	580.0000	77.20
9.000	8.964	570.0000	550.0000	74.80
10.000	9.959	550.0000	520.0000	72.60
11.000	10.953	530.0000	490.0000	70.50
12.000	11.948	510.0000	460.0000	68.50
13.000	12.940	490.0000	430.0000	66.60
14.000	13.933	470.0000	400.0000	64.70
15.000	14.926	450.0000	370.0000	62.90
16.000	15.919	430.0000	340.0000	61.10
17.000	16.911	410.0000	310.0000	59.40
18.000	17.903	390.0000	280.0000	57.70
19.000	18.894	370.0000	250.0000	56.10
20.000	19.886	350.0000	220.0000	54.50
21.000	20.877	330.0000	190.0000	53.00
22.000	21.867	310.0000	160.0000	51.50
23.000	22.858	290.0000	130.0000	50.00
24.000	23.848	270.0000	100.0000	48.50
25.000	24.837	250.0000	70.0000	47.00
26.000	25.827	230.0000	40.0000	45.50
27.000	26.816	210.0000	10.0000	44.00
28.000	27.805	190.0000	0.0000	42.50
29.000	28.793	170.0000	0.0000	41.00
30.000	29.781	150.0000	0.0000	39.50
32.000	31.757	9.0000	13.4000	27.49
34.000	33.731	6.0000	0.0000	24.00
36.000	35.704	3.0000	7.0000	20.00
38.000	37.675	0.0000	5.0000	16.00
40.000	39.646	0.0000	4.0000	12.00
42.000	41.615	0.0000	3.0000	8.00
44.000	43.583	0.0000	2.0000	4.00
46.000	45.550	0.0000	1.0000	0.00
48.000	47.516	0.0000	0.0000	0.00
50.000	49.480	0.0000	0.0000	0.00
52.000	51.443	0.0000	0.0000	0.00
54.000	53.405	0.0000	0.0000	0.00
56.000	55.366	0.0000	0.0000	0.00
58.000	57.325	0.0000	0.0000	0.00
60.000	59.283	0.0000	0.0000	0.00
62.000	61.240	0.0000	0.0000	0.00
64.000	63.195	0.0000	0.0000	0.00
66.000	65.150	0.0000	0.0000	0.00

TABLE IV-13. HYDROSTATIC MODEL ATMOSPHERE

## ANNUAL

STATION - 616020		ASLINGTON (MOE) (1961)		
Z	OC. HT.	P	D	TV
MM	MM	MM	MM	MM
0.000	0.000	1020.0000	1100.0000	251.00
1.000	0.070	1020.7000	1161.0000	251.00
1.000	0.027	098.0000	1071.0000	252.00
2.000	1.924	700.0000	953.0000	253.14
3.000	2.051	700.0000	870.0000	253.25
4.000	3.087	609.0000	767.0000	253.10
5.000	4.003	525.0000	710.0000	252.73
6.000	5.073	450.0000	630.0000	252.00
7.000	6.074	400.0000	570.0000	250.00
8.000	7.003	377.0000	517.0000	250.00
9.000	8.004	300.0000	450.0000	246.52
10.000	9.003	200.0000	410.0000	243.50
11.000	10.003	247.0000	370.0000	239.10
12.000	11.006	213.0000	334.0000	232.18
13.000	12.040	160.0000	285.0000	214.61
14.000	13.033	155.0000	250.0000	207.75
15.000	14.000	131.0000	227.0000	201.00
16.000	15.019	111.0000	190.0000	191.00
17.000	16.011	93.0000	160.0000	181.00
18.000	17.003	70.0000	130.0000	169.10
19.000	18.004	60.0000	114.0000	163.67
20.000	19.000	50.0000	94.0000	157.97
21.000	20.007	40.0000	79.0000	211.54
22.000	21.007	41.0000	66.0000	214.40
23.000	22.000	25.0000	50.0000	216.70
24.000	23.009	30.0000	47.0000	210.00
25.000	24.007	25.0000	40.0000	221.00
26.000	25.007	20.0000	34.0000	223.00
27.000	26.016	10.0000	29.0000	220.76
28.000	27.005	10.0000	25.0000	227.83
29.000	28.003	14.0000	21.0000	229.73
30.000	29.001	12.0000	18.0000	231.69
32.000	31.007	9.0000	13.0000	236.13
34.000	33.001	6.0000	10.0000	240.49
36.000	35.004	5.0000	7.0000	245.42
38.000	37.006	3.0000	5.0000	251.00
40.000	39.006	3.0000	4.0000	257.60
42.000	41.005	2.0000	3.0000	263.29
44.000	43.003	1.0000	2.0000	267.57
46.000	45.000	1.0000	1.0000	269.91
48.000	47.006	1.0000	1.0000	270.46
50.000	49.000	0.0000	1.0000	269.55
52.000	51.003	0.0000	0.0000	267.00
54.000	53.003	0.0000	0.0000	264.00
56.000	55.000	0.0000	0.0000	261.00
58.000	57.000	0.0000	0.0000	257.79
60.000	59.003	0.0000	0.0000	253.37
62.000	61.000	0.0000	0.0000	249.12
64.000	63.006	0.0000	0.0000	242.49
66.000	65.000	0.0000	0.0000	234.93

## APPENDIX A

### EXAMPLES OF WIND STATISTICS FOR ASCENSION ISLAND, SOUTH ATLANTIC

Appendix A gives some examples of graphical displays of wind statistics that can be derived from the statistical parameters presented in table I. These illustrations should aid the user of the RRA to understand the functional relationships of the probability wind models and, thus, to develop an appreciation of the powerful properties of the bivariate normal probability distribution function.

All illustrations for this appendix are derived from the five wind component statistical parameters from table I.1 for January and table I.7 for July for eight selected altitudes. These selected altitudes are 4, 12, 20, 30, 40, 50, 60, and 66 km.

#### 1. Frequency of Wind Direction (Figures A-1 through A-16)

The derived frequencies for wind direction shown in figures A-1 through A-16 were obtained using the five wind component parameters from tables I.1 and I.7 as input values in equation (35). The limits of integration (performed numerically) are over the 22.5-degree interval for each of the 16 compass points. These graphs give the percentage frequency that the wind will blow from the direction intervals.

#### 2. Mean Wind Components and 80th Interpercentile Range of Wind Components (Figures A-17 through A-32).

The wind component means with respect to any orthogonal axes are obtained by using the zonal and meridional mean wind components in equations (44) and (45). These component means form the circles shown in figures A-17 through A-32. Further, the zonal and meridional wind component variances and correlation coefficients are used in equations (46) and (47) to obtain the variances with respect to any orthogonal axes. These rotated component variances and the rotated component means are used in equation (8) to obtain the 80th interpercentile range of wind components and are then illustrated in figures A-17 through A-32.

#### 3. Probability Ellipses (Figures A-33 through A-48)

Using the five wind component parameters from tables I.1 and I.7 and  $p = 0.50$ ,  $p = 0.95$ , and  $p = 0.99$  as input values to equation (13), the wind probability ellipses shown in figures A-33 through A-48 were obtained by computer graphics. The statistical inferences are, for example, that 50 percent of the wind vectors lie within the smaller ellipse and 99 percent of the wind vectors lie within the outer ellipse. These probability ellipses are illustrated using the standard meteorological coordinate system explained in section I.B.1.

#### 4. Conditional Windspeed Given the Wind Direction (Figures A-49 through A-64)

The five wind component parameters from table I.1 and table I.7 are used to evaluate the conditional probability distribution function, equation (41). Figures A-49 through A-64 show interpolations of the conditional function made to

obtain the 5th, 15th, 50th (median), 85th, 95th, and 99th conditional percentile values of windspeed, given the wind directions. The conditional mean windspeed, given the wind direction, is obtained from equation (40). The conditional mode (most probable) windspeed, given the wind direction, is obtained from equation (38). The conditional mean windspeed and the conditional windspeed modal value, given the wind direction, are also shown in these figures. For some figures, the conditional windspeed values are invalid for the given wind direction near  $270^\circ$  (from the west). This is caused by the lack of computational precision in evaluating equations (40) and (41) when the arguments for the Gaussian probability distribution have large negative values, i.e., when the coefficients  $(b/a)$  become less than -4 in these equations.

This appendix contains only a few of the many options in presenting wind statistics illustrations.

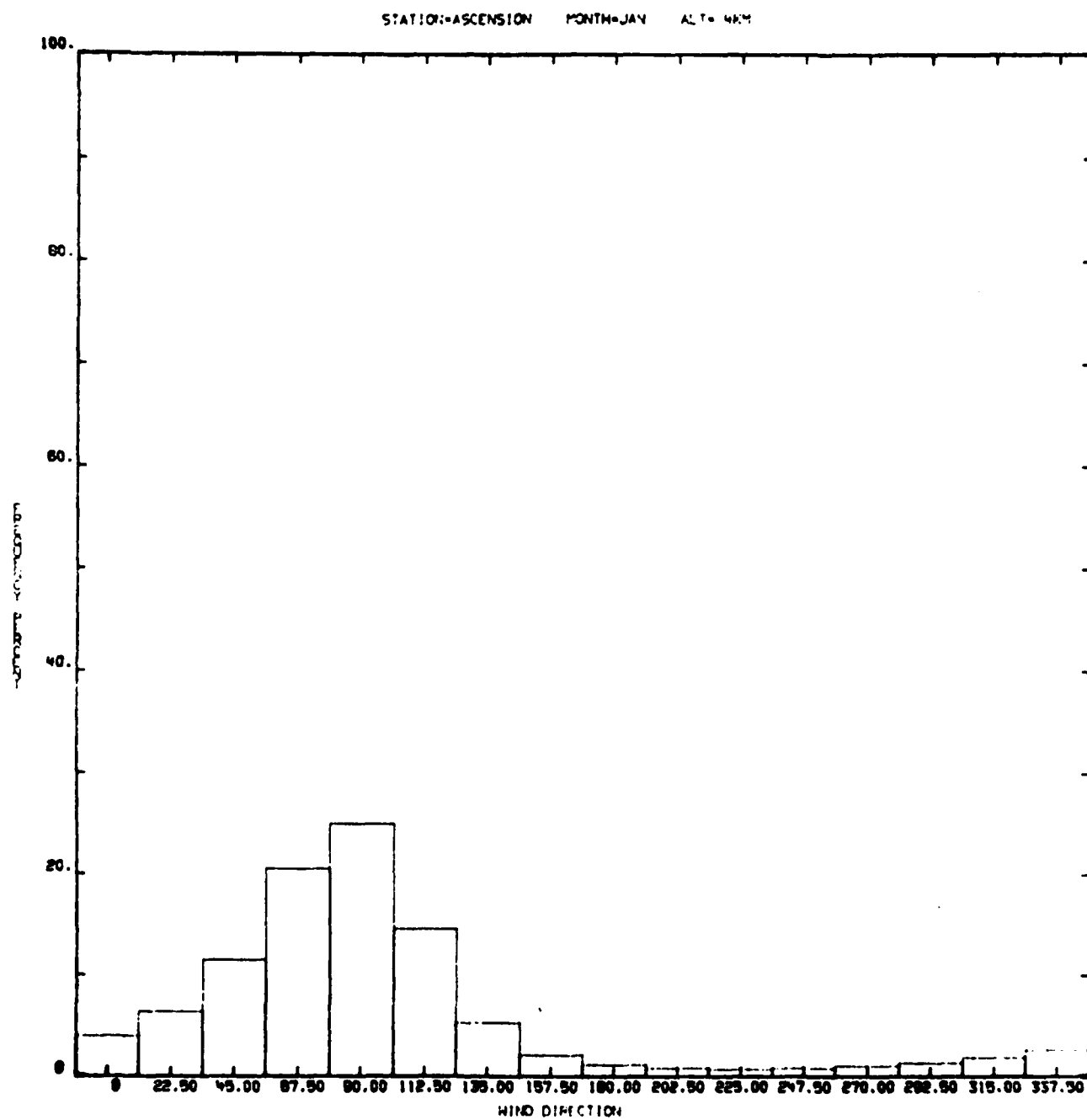


Figure A-1.

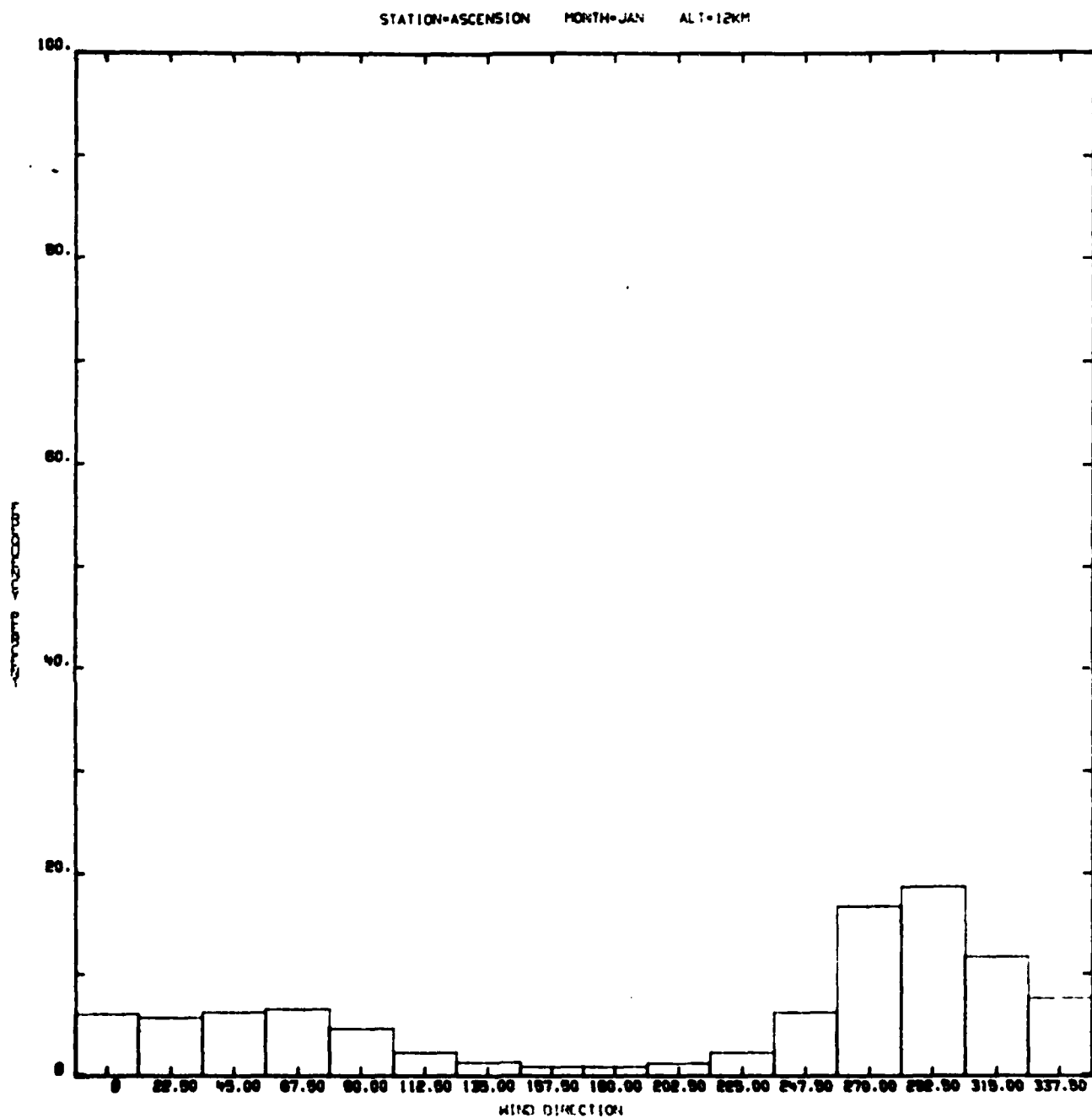


Figure A-2.



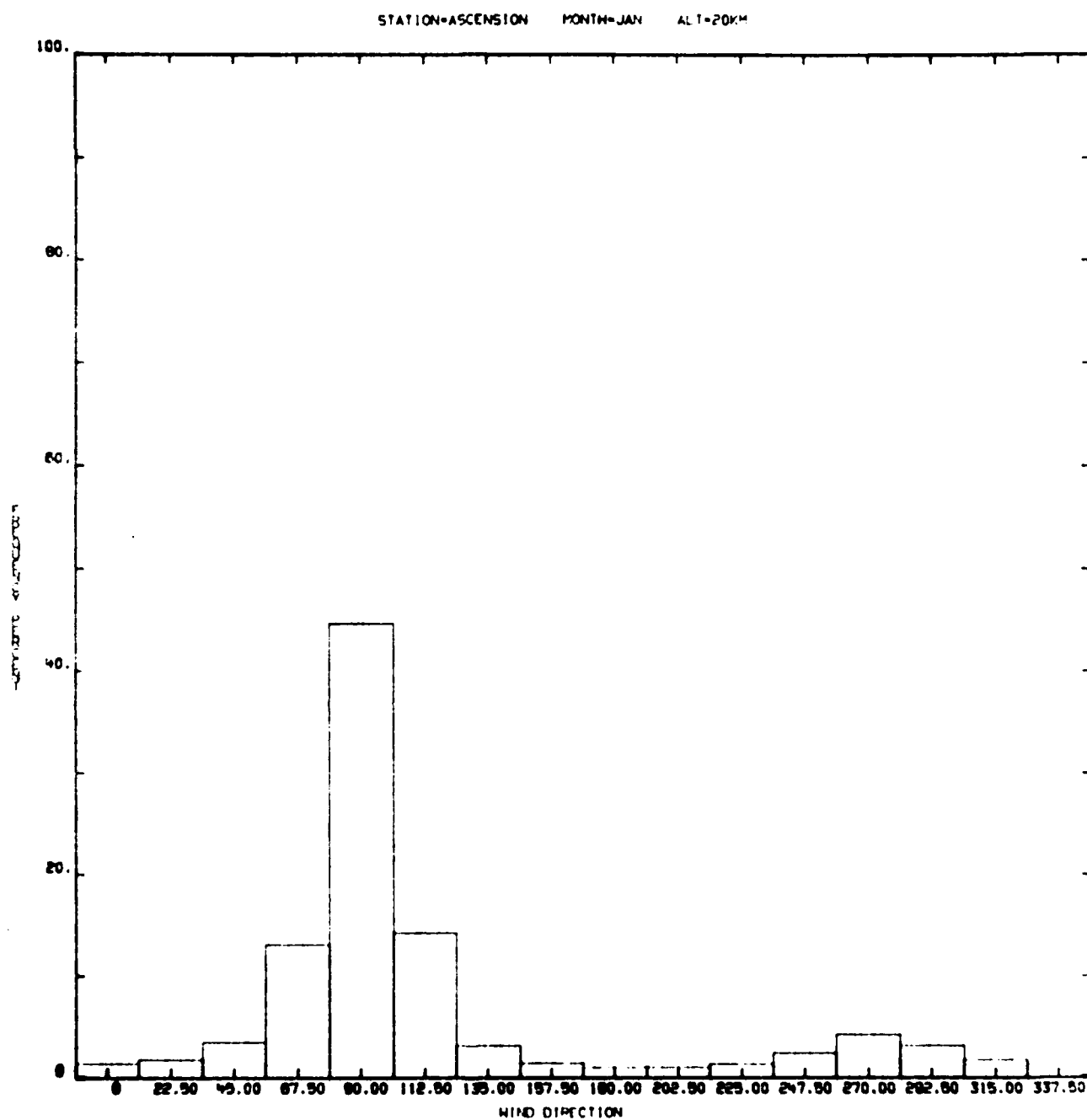


Figure A-3.

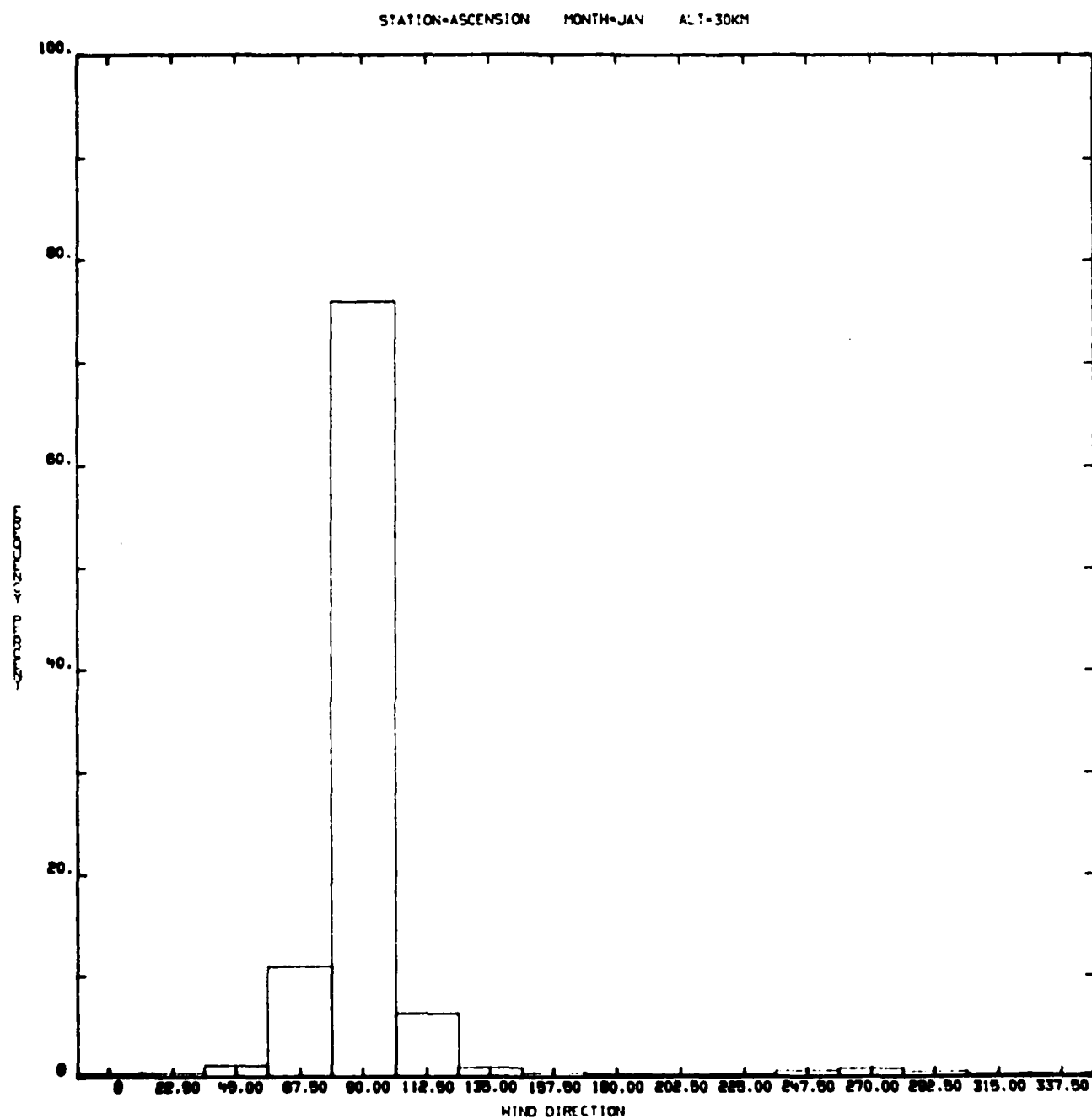


Figure A-4.

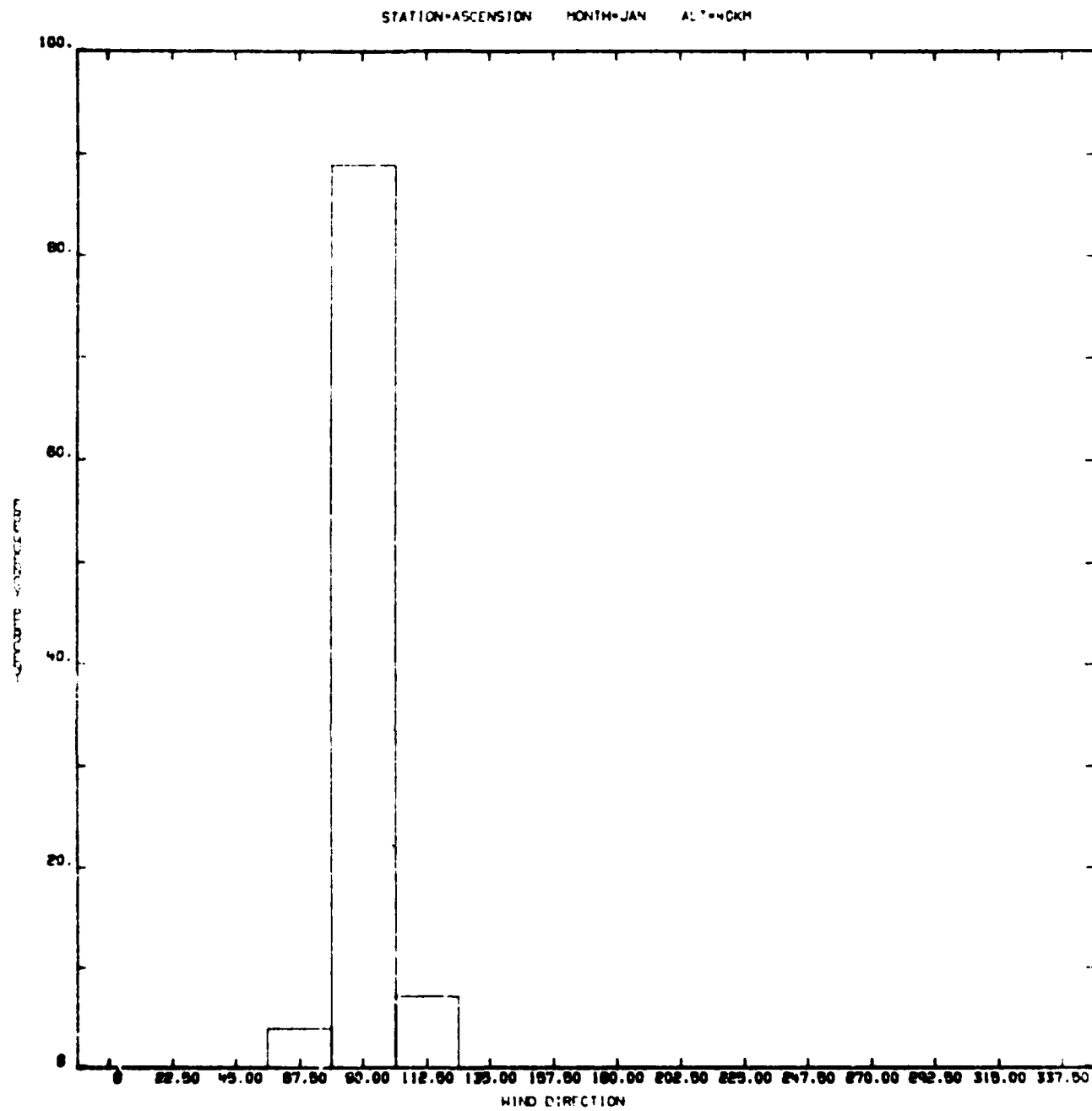


Figure A-5.

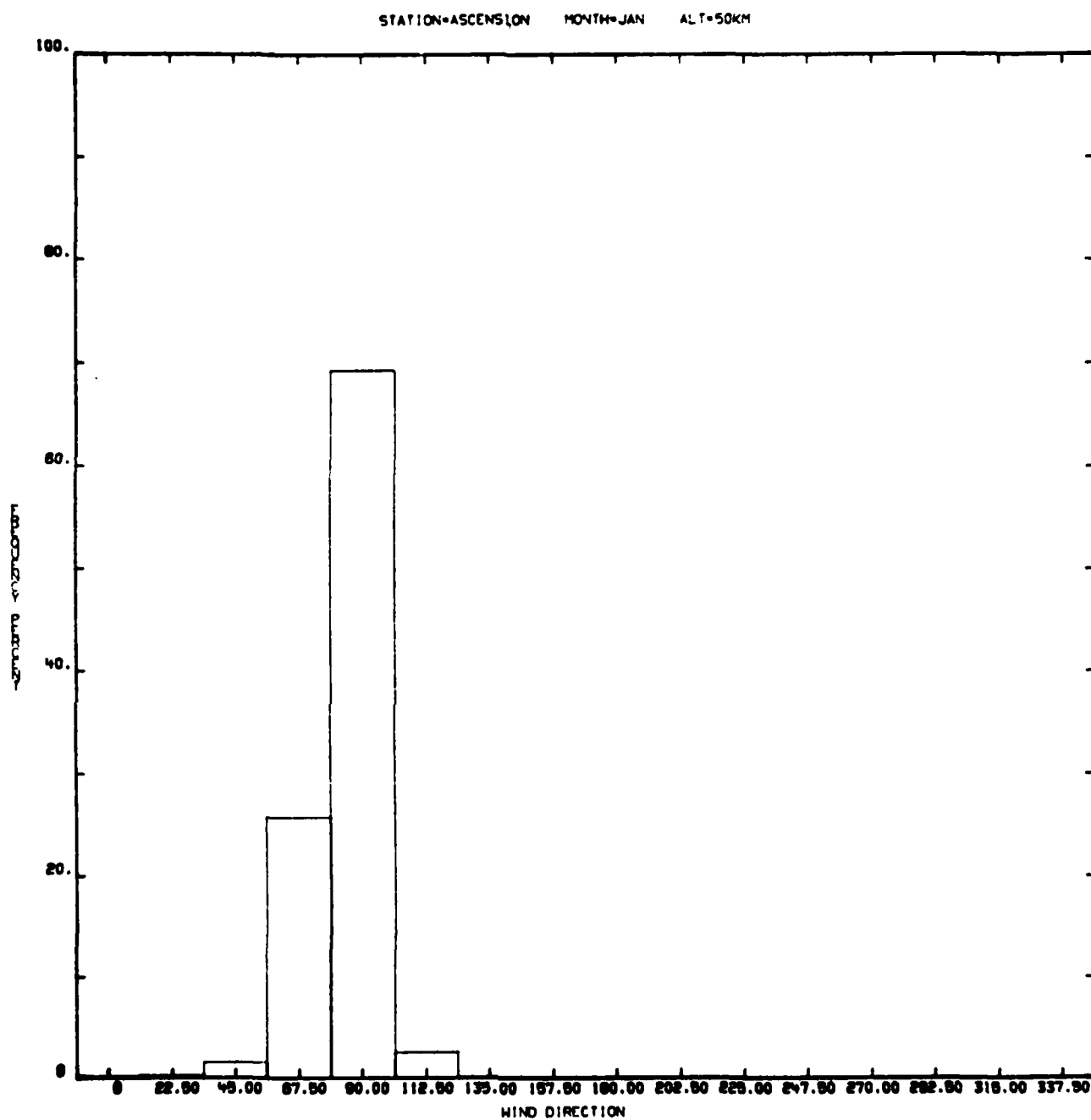


Figure A-6.

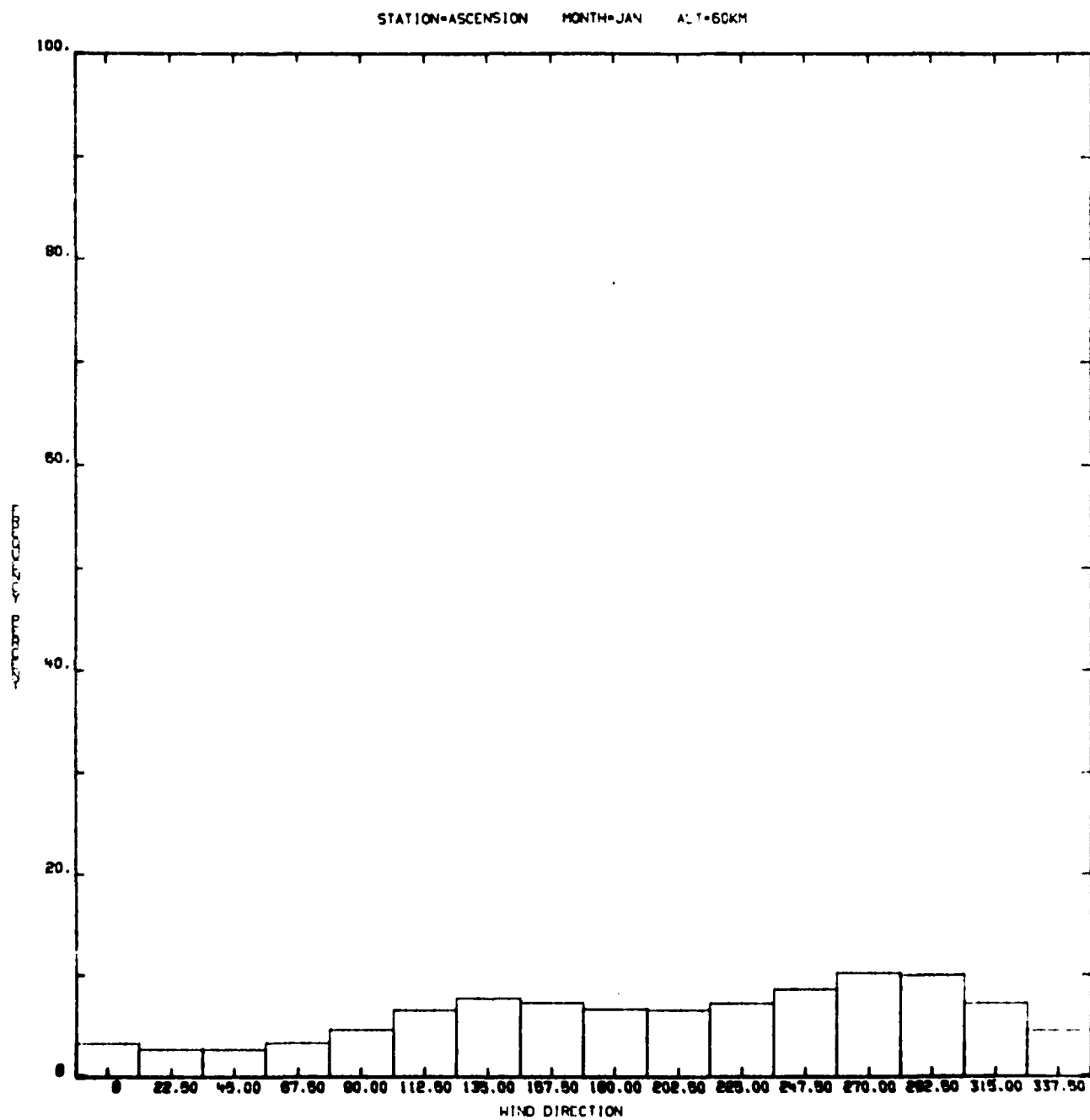


Figure A-7.

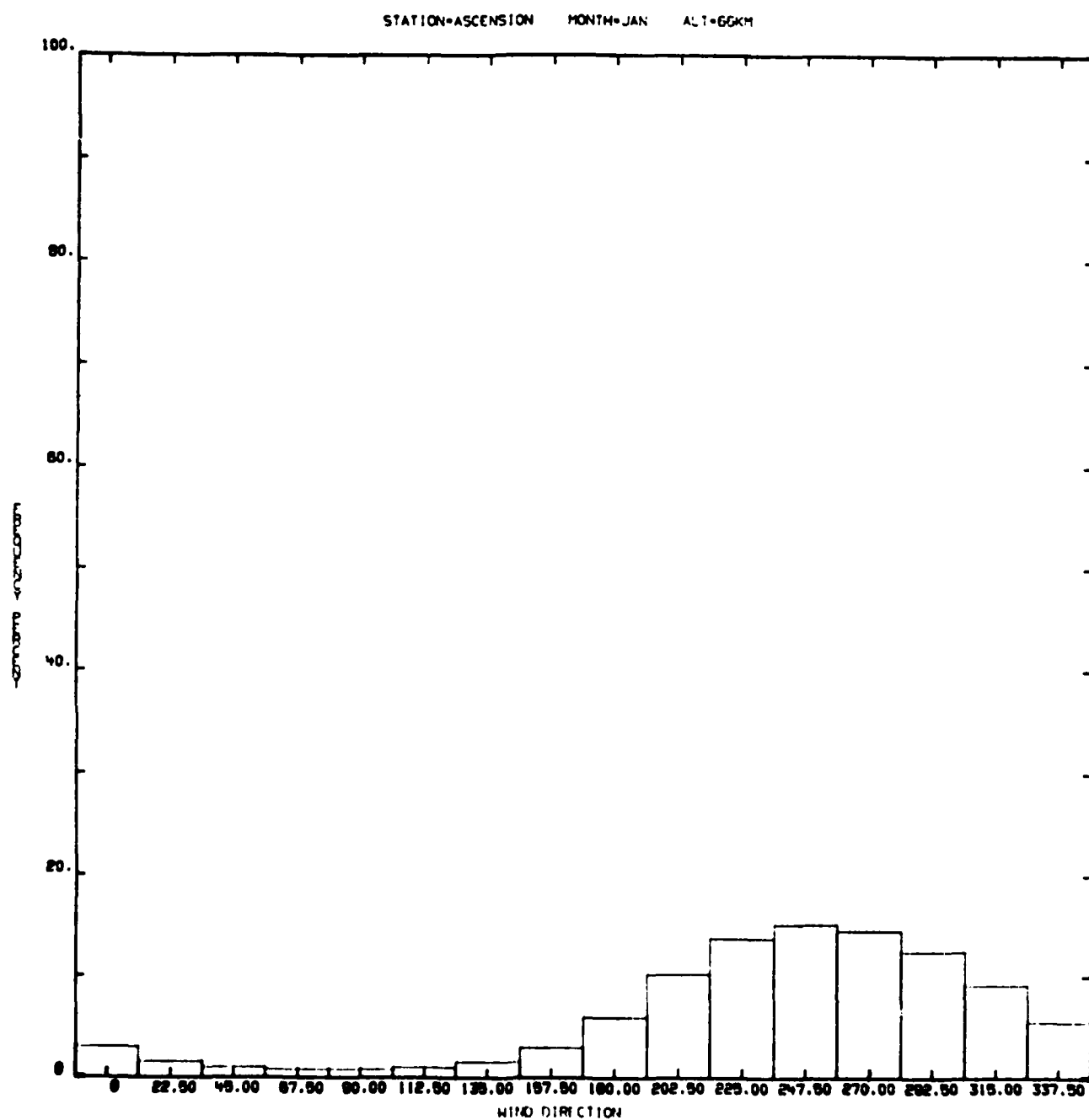


Figure A-8.

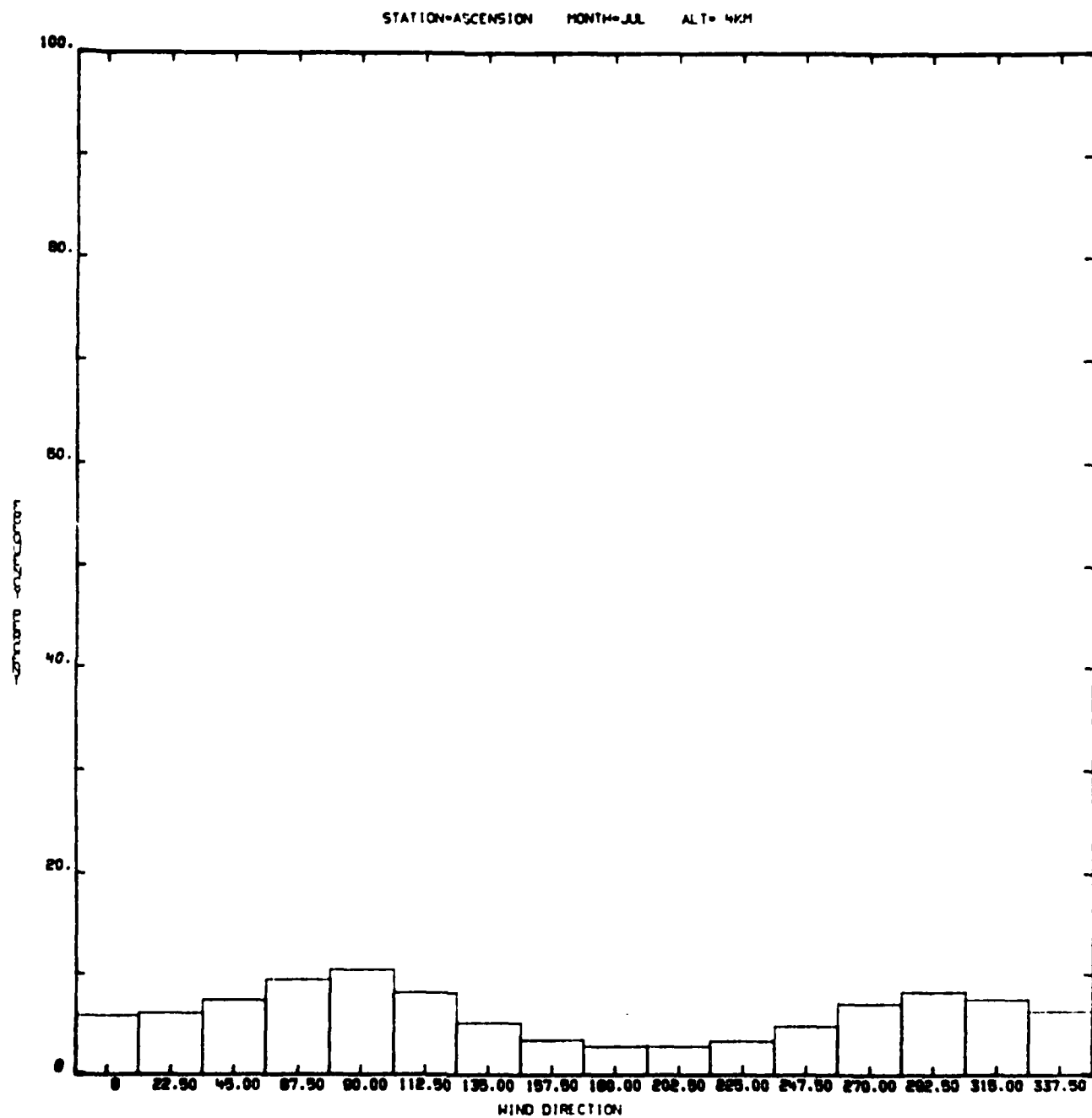


Figure A-9.

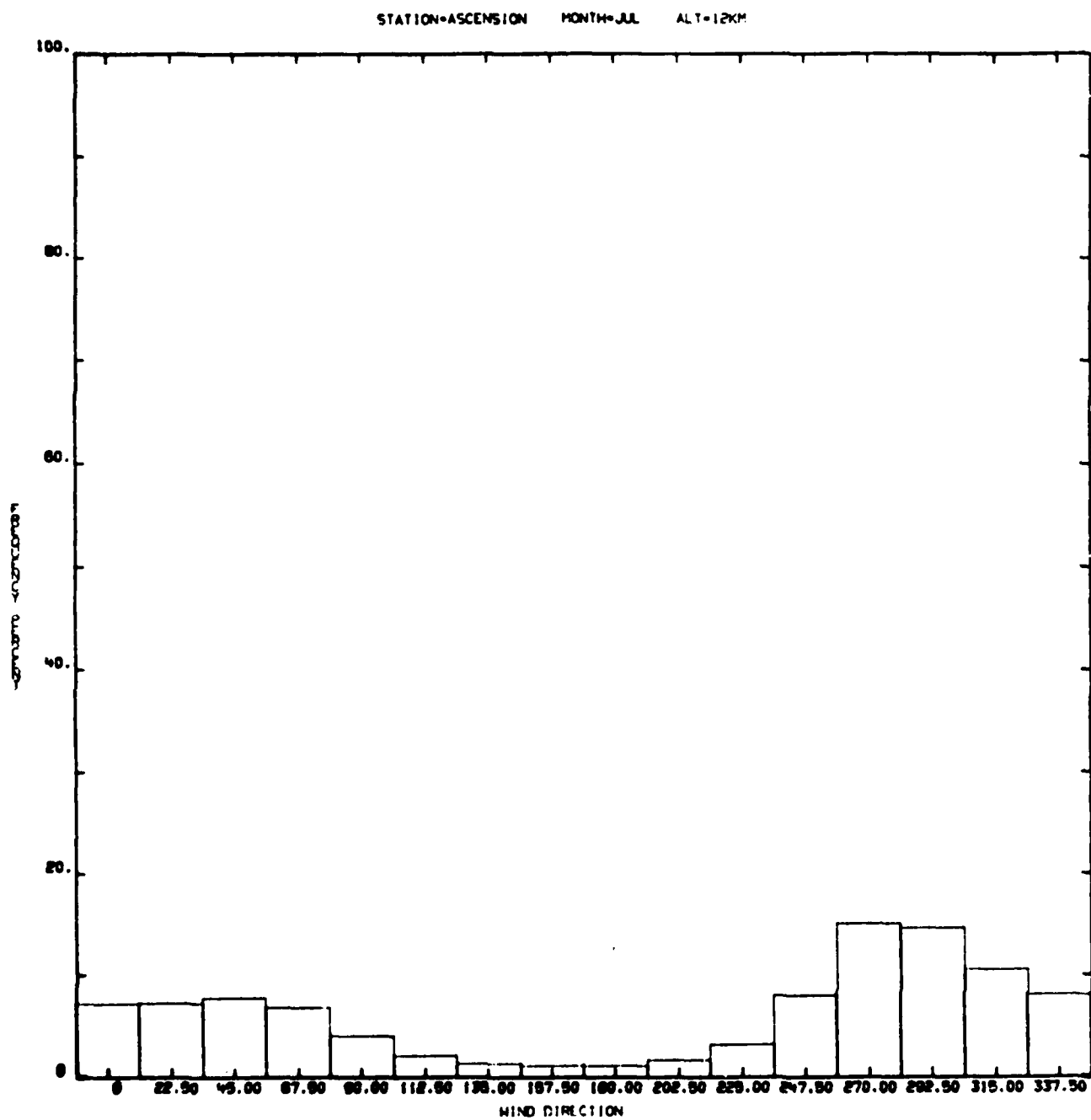


Figure A-10.



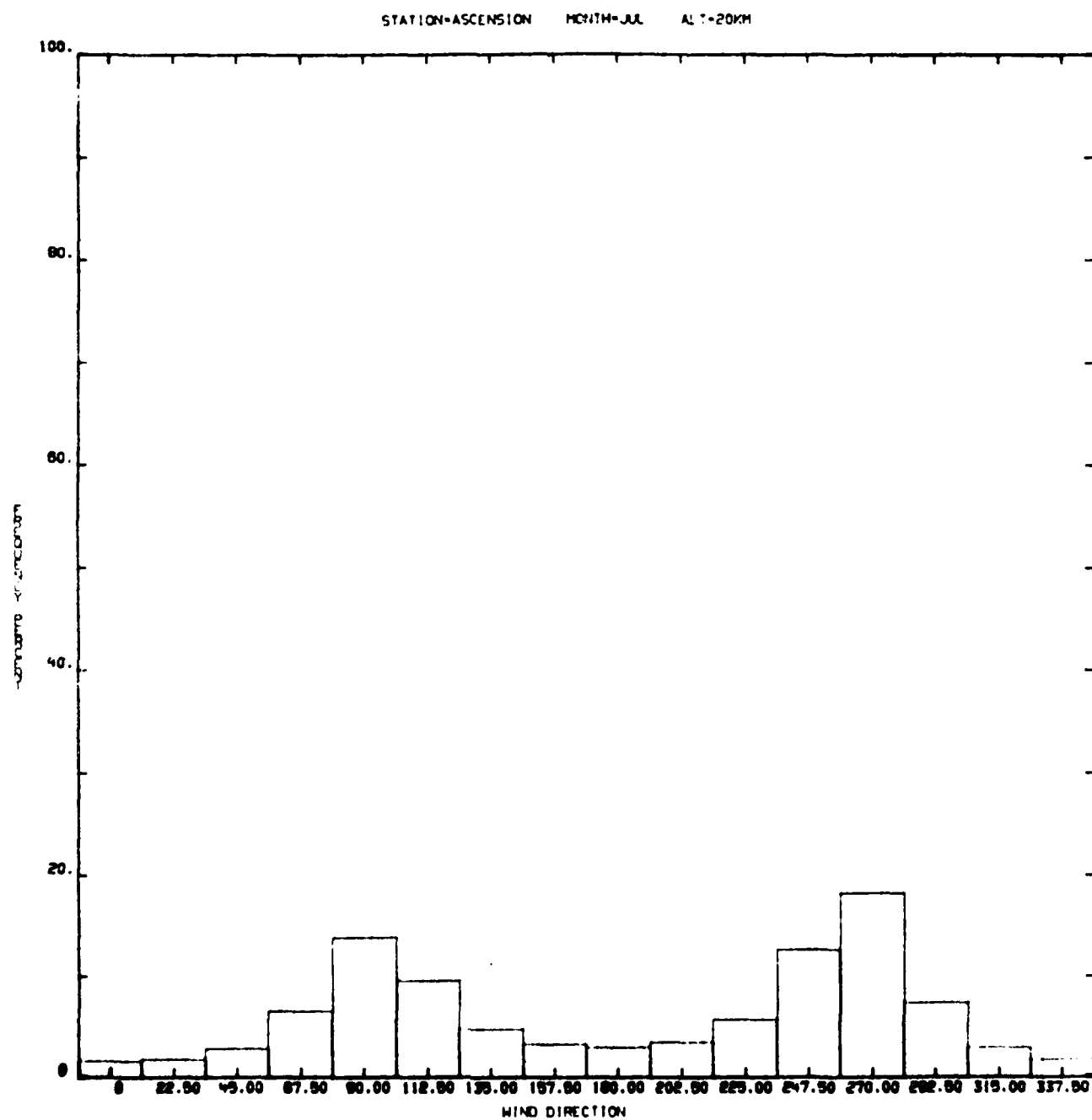


Figure A-11.

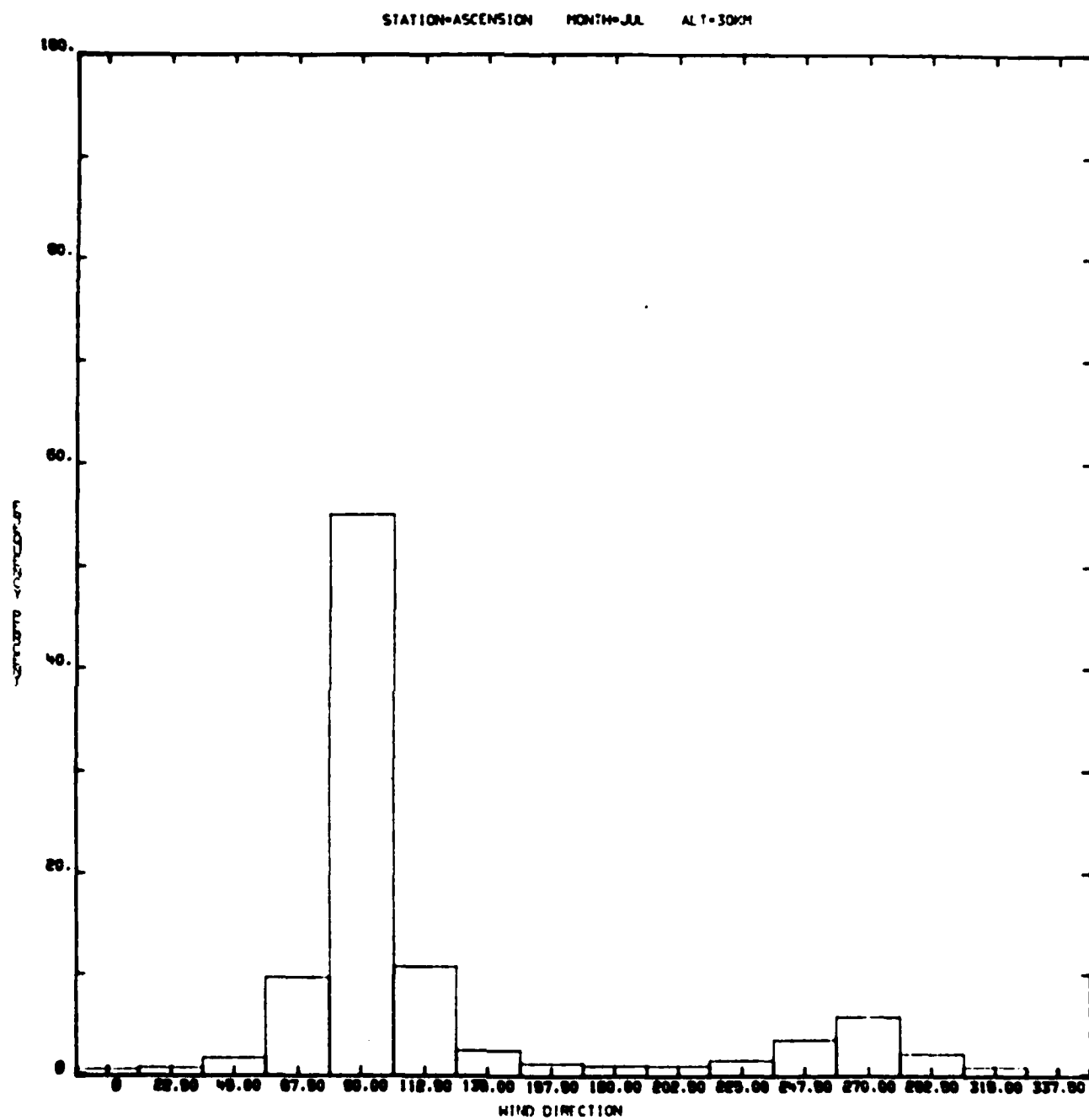


Figure A-12.

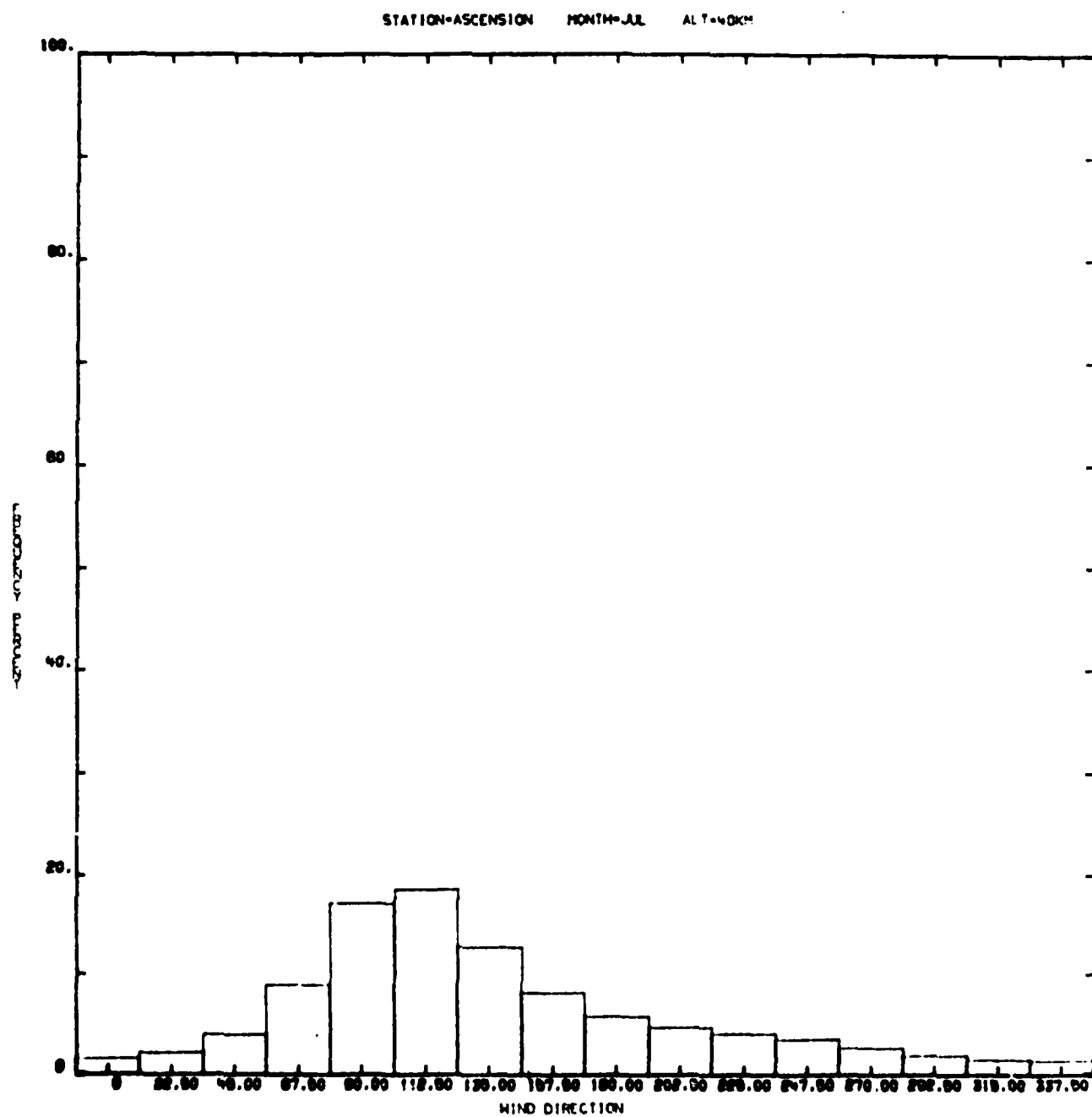


Figure A-13.

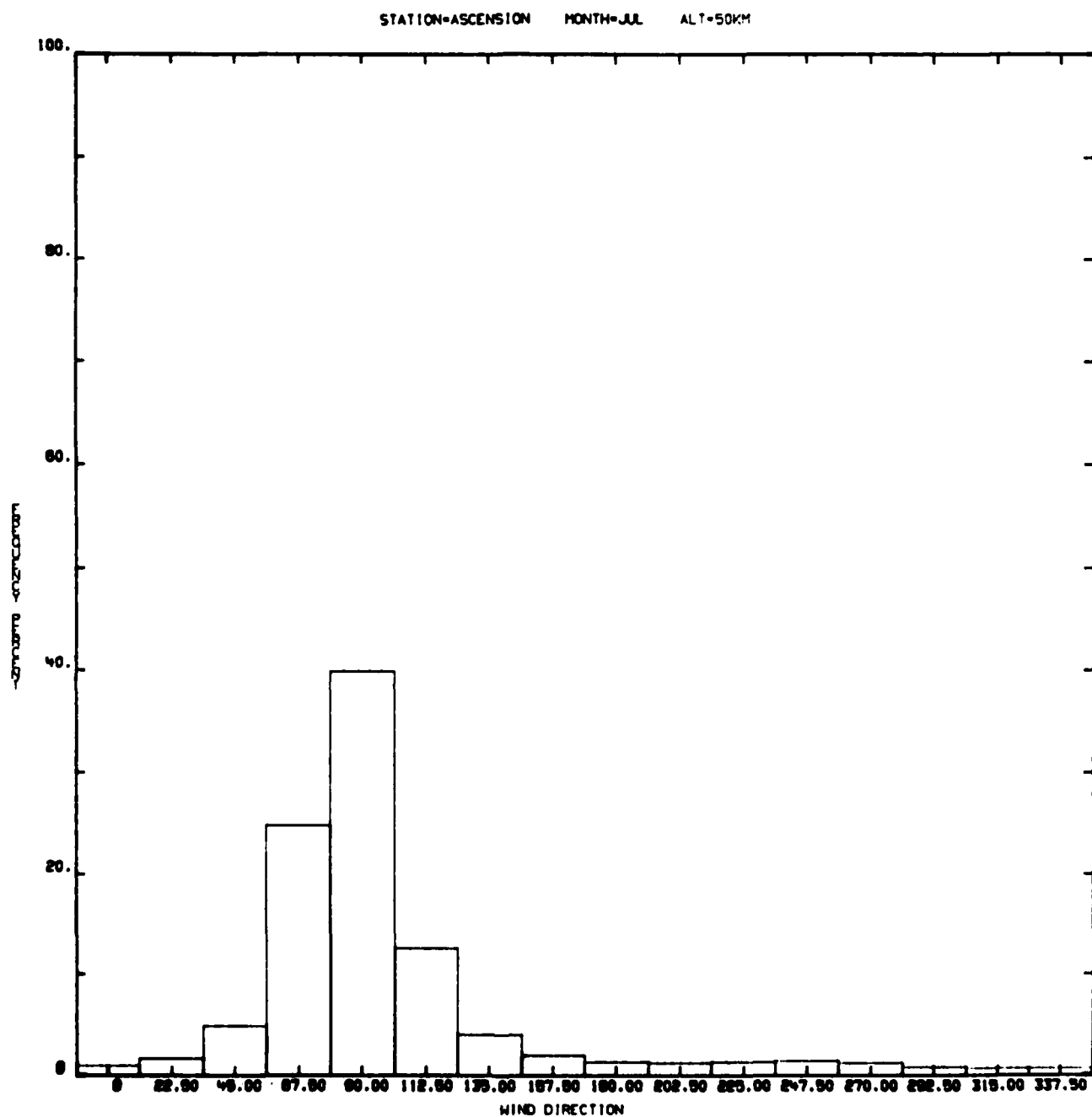


Figure A-14.

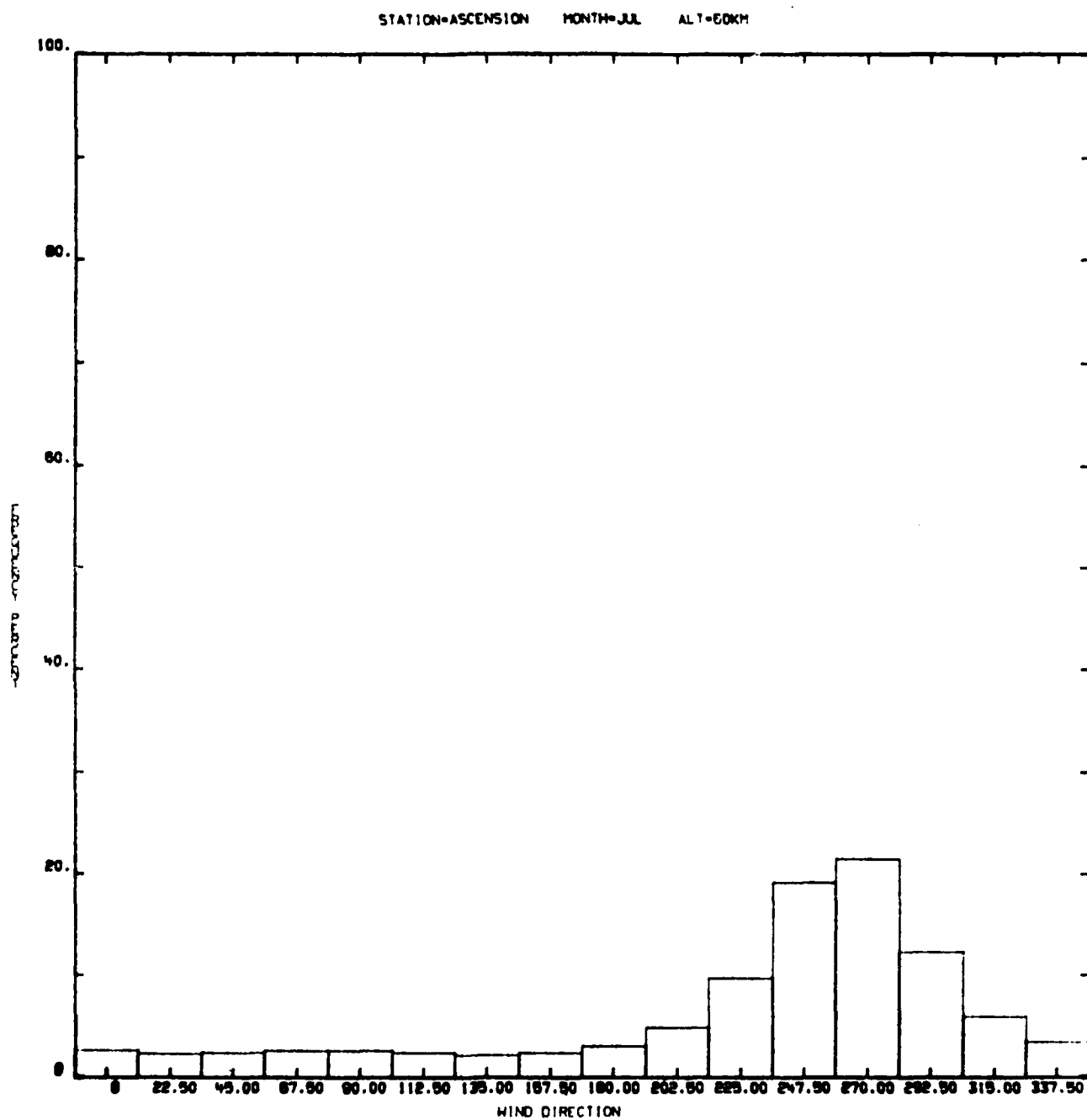


Figure A-15.

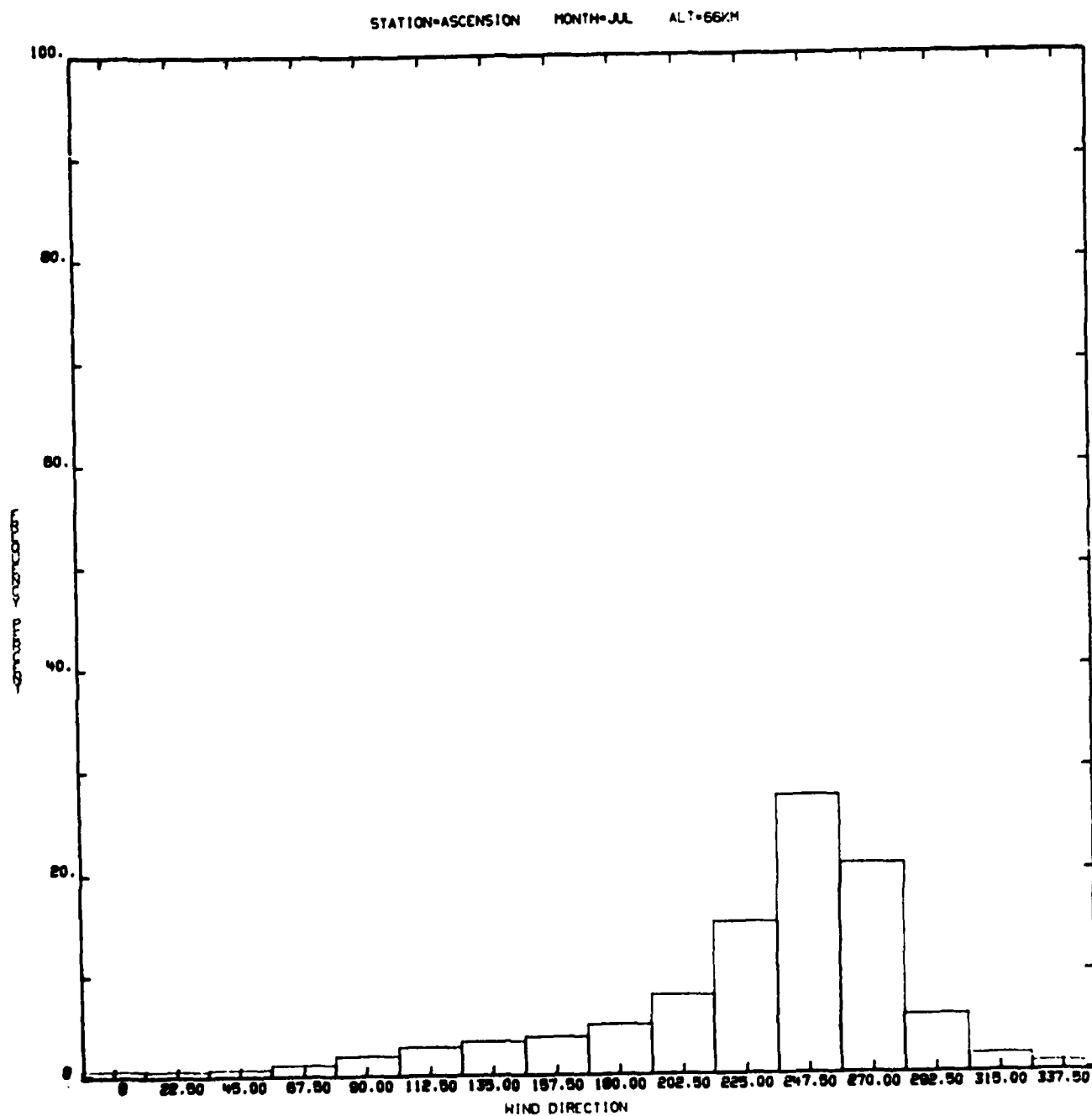


Figure A-16.

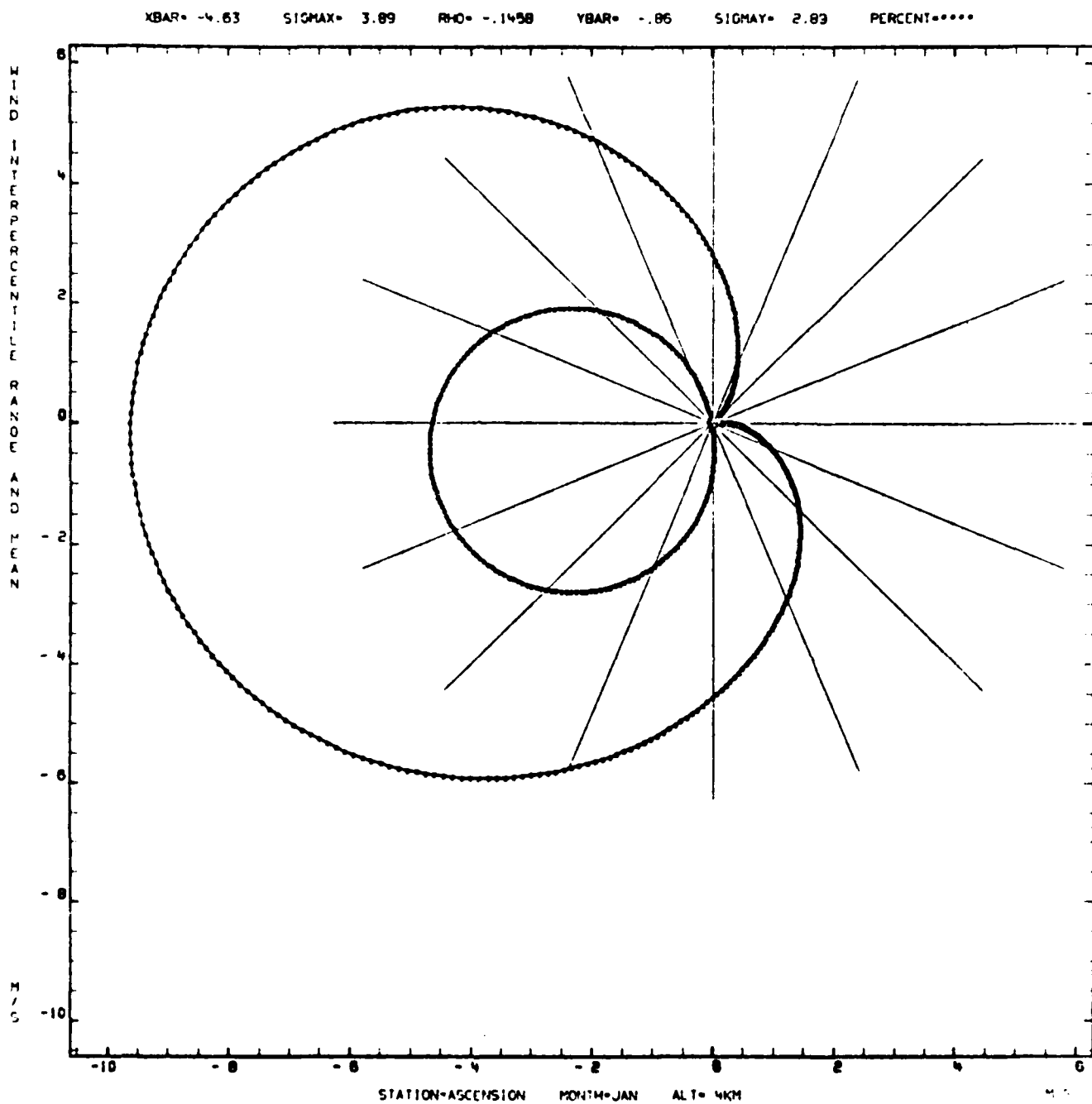


Figure A-17.

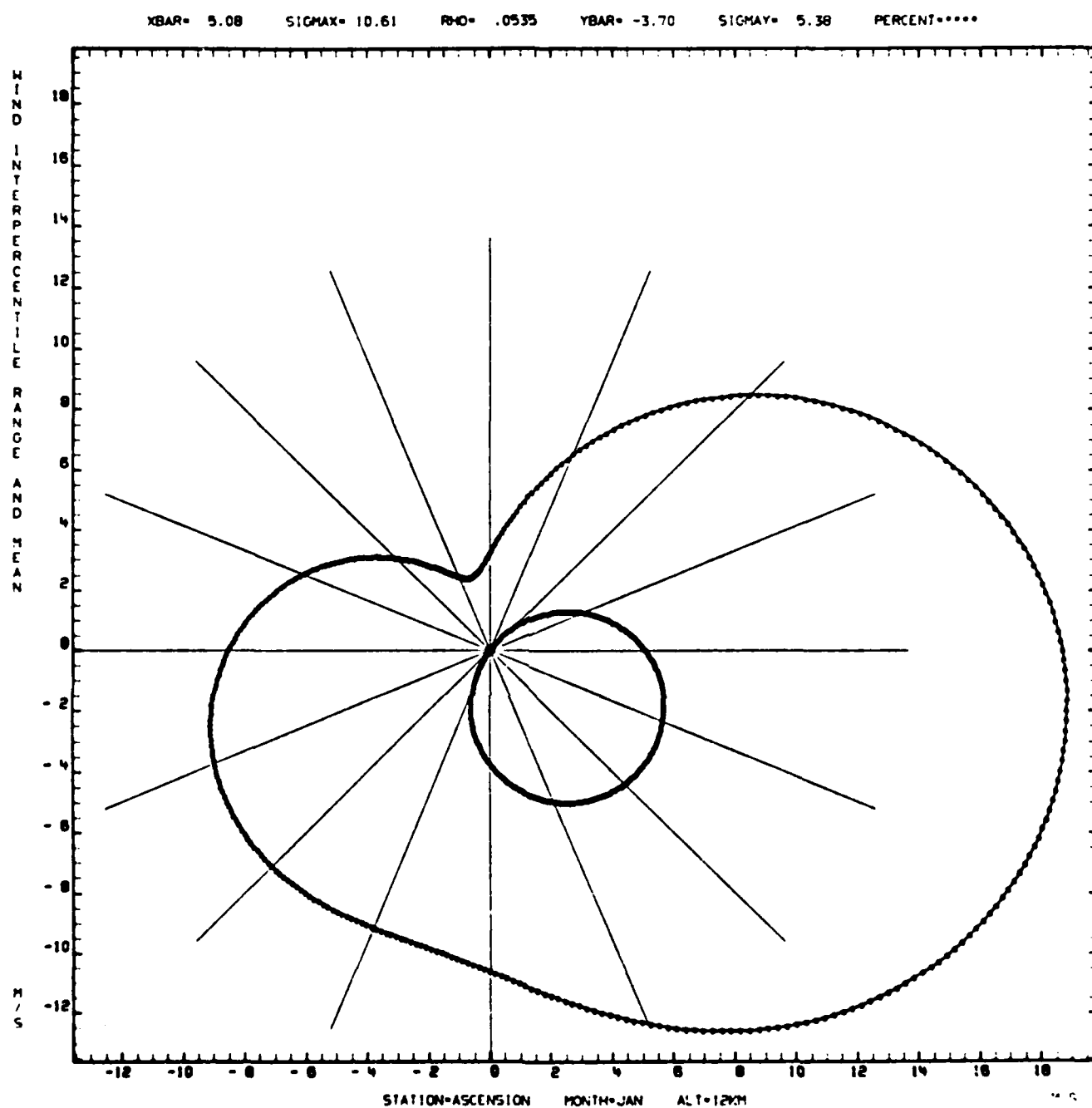


Figure A-18.



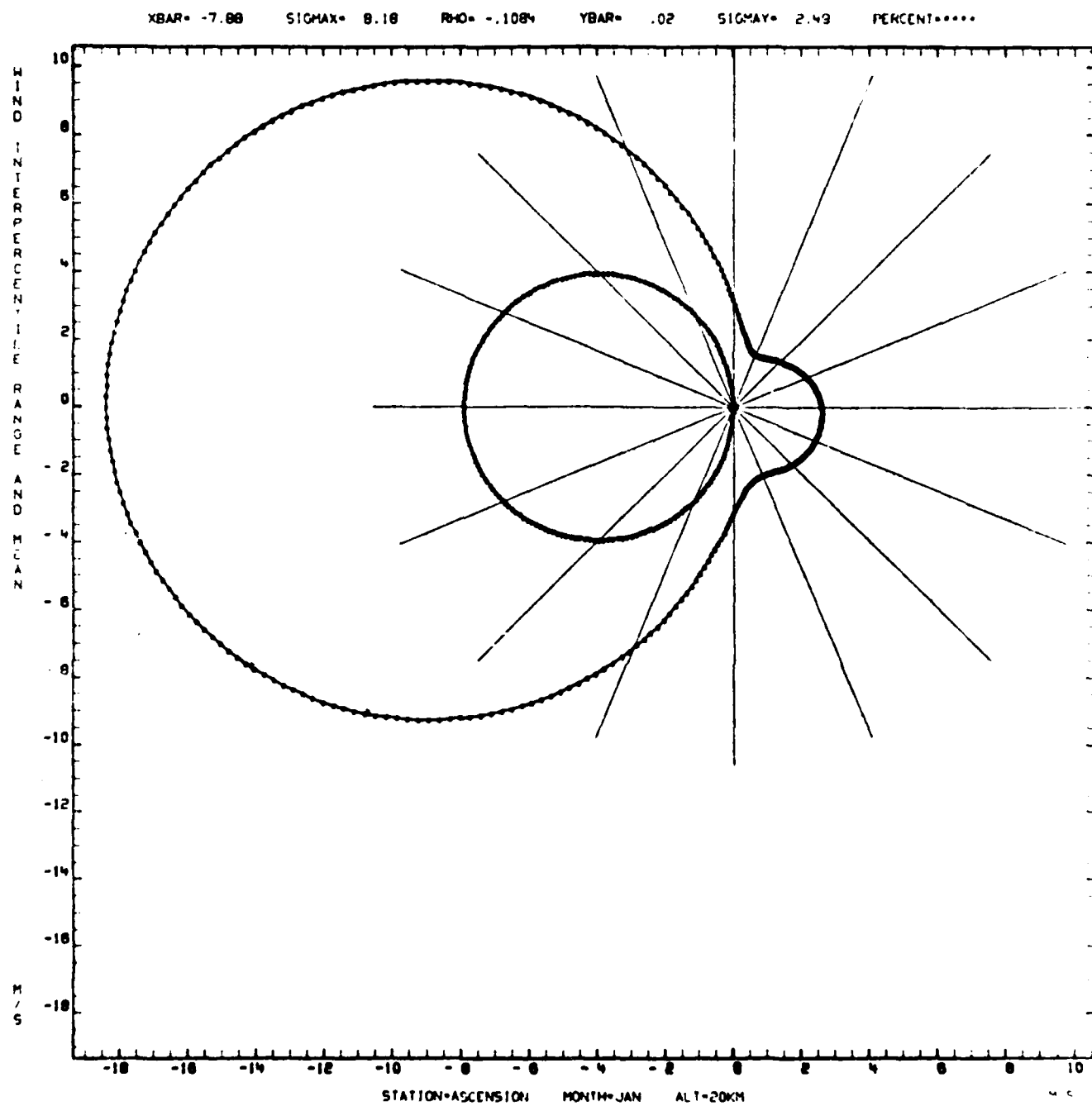


Figure A-19.

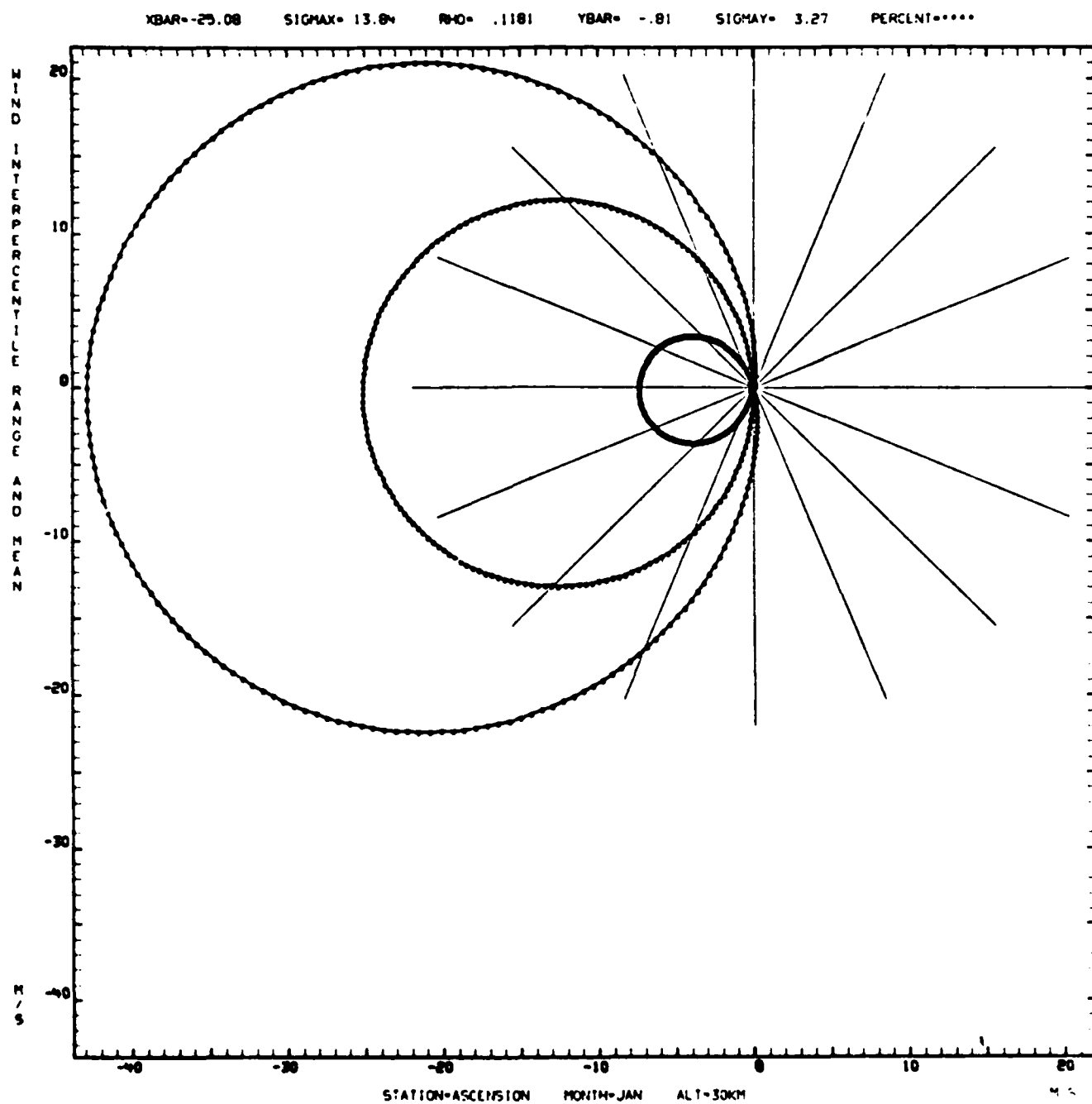


Figure A-20.

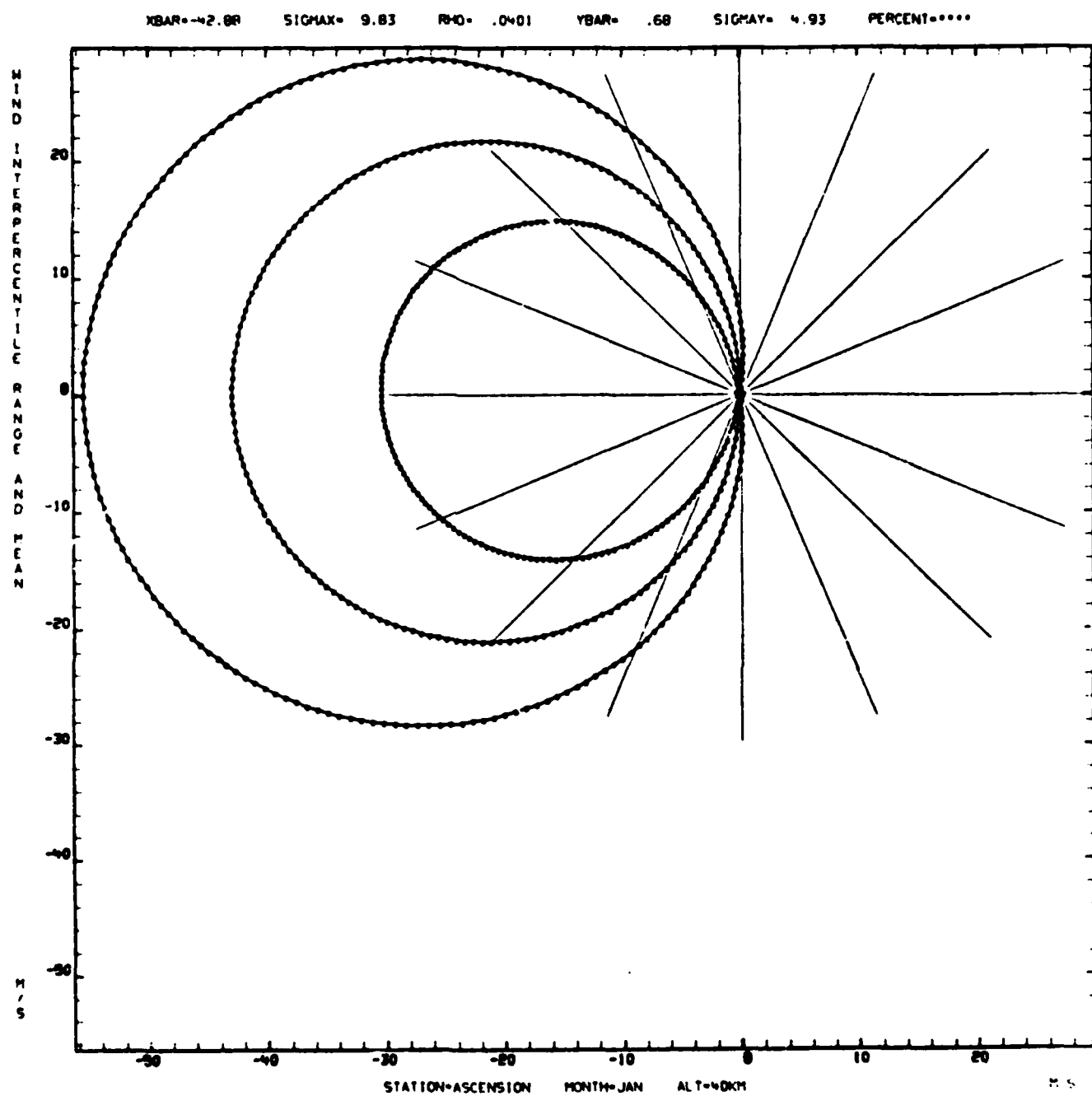


Figure A-21.

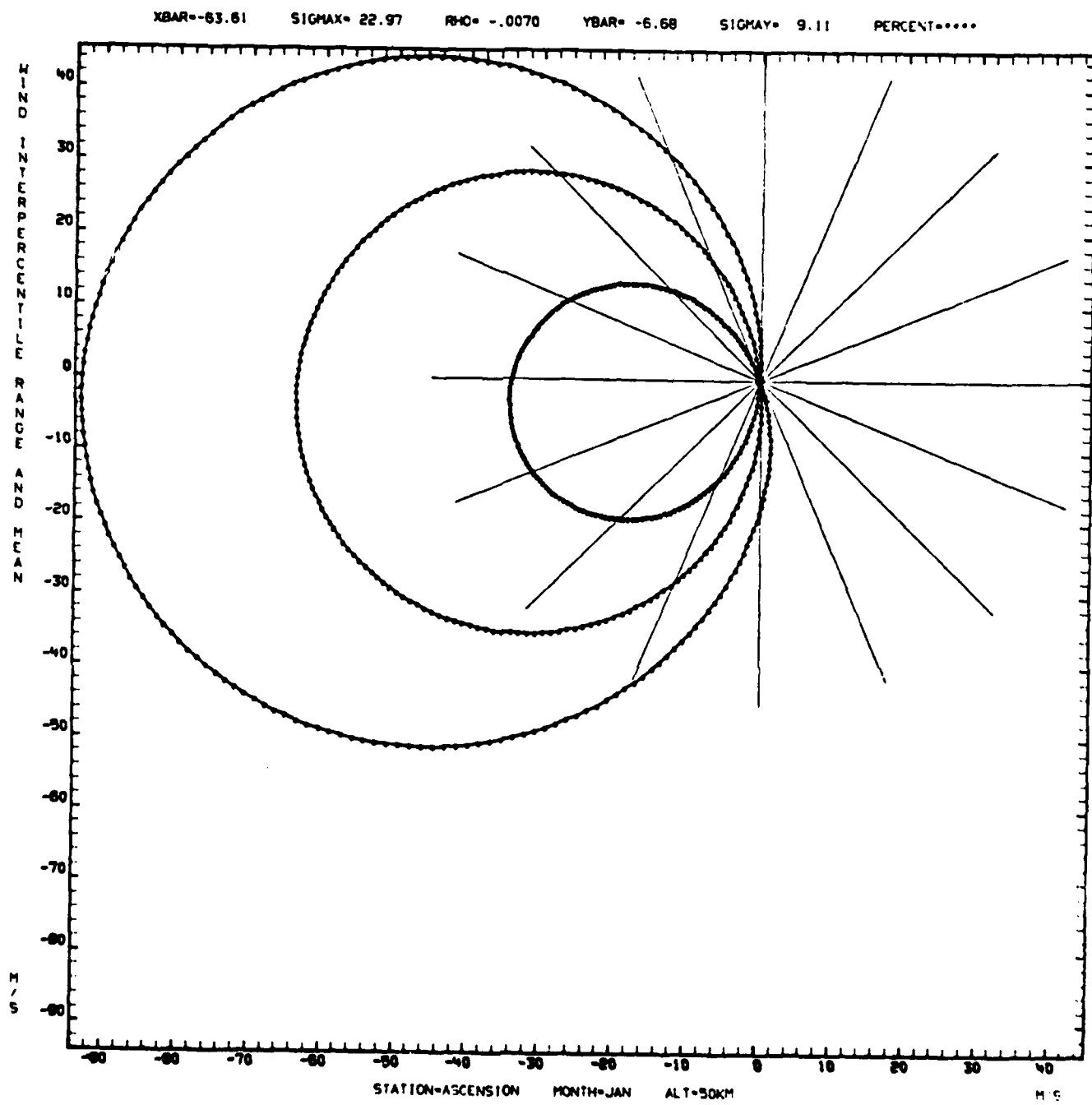


Figure A-22.

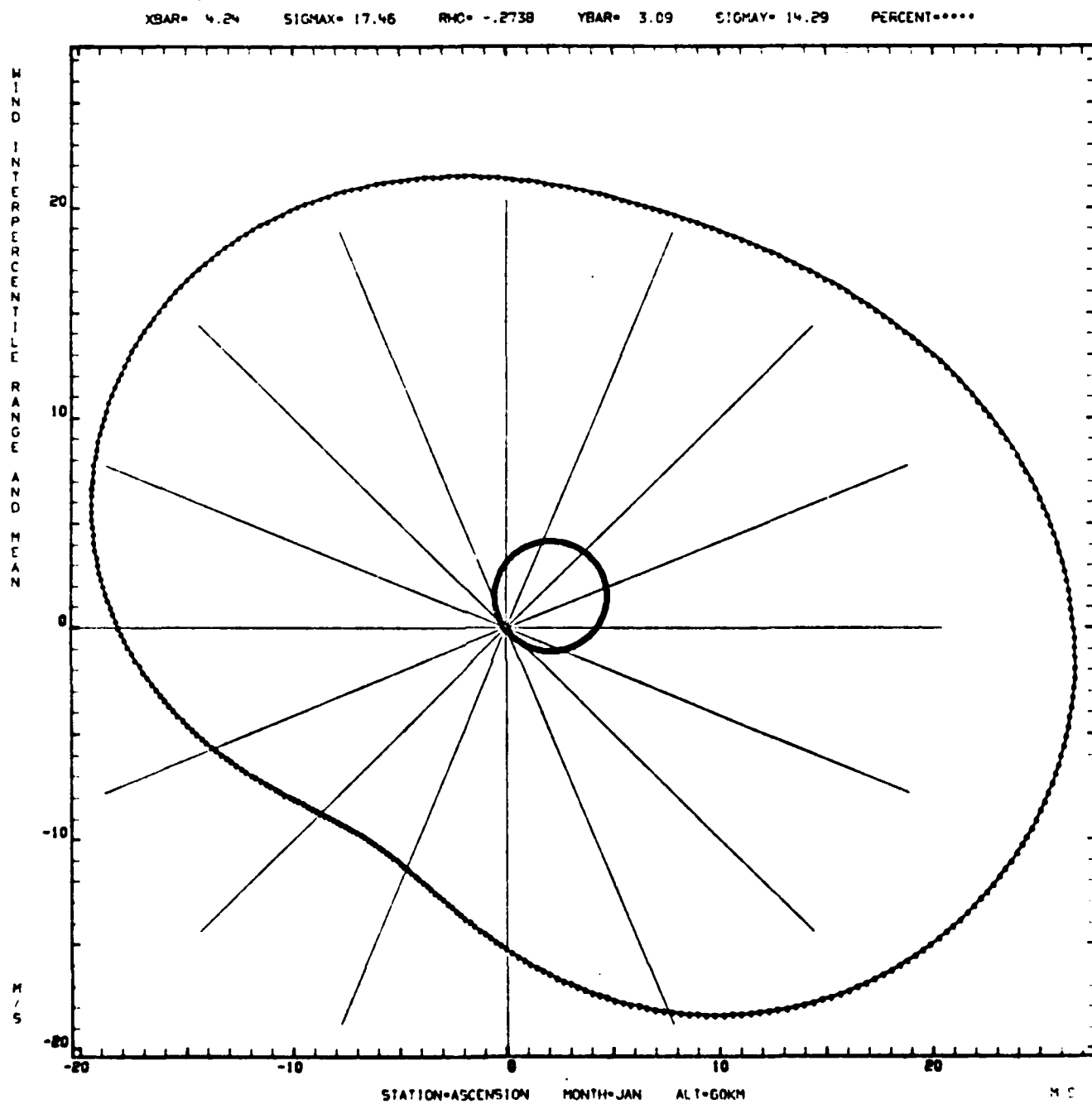


Figure A-23.

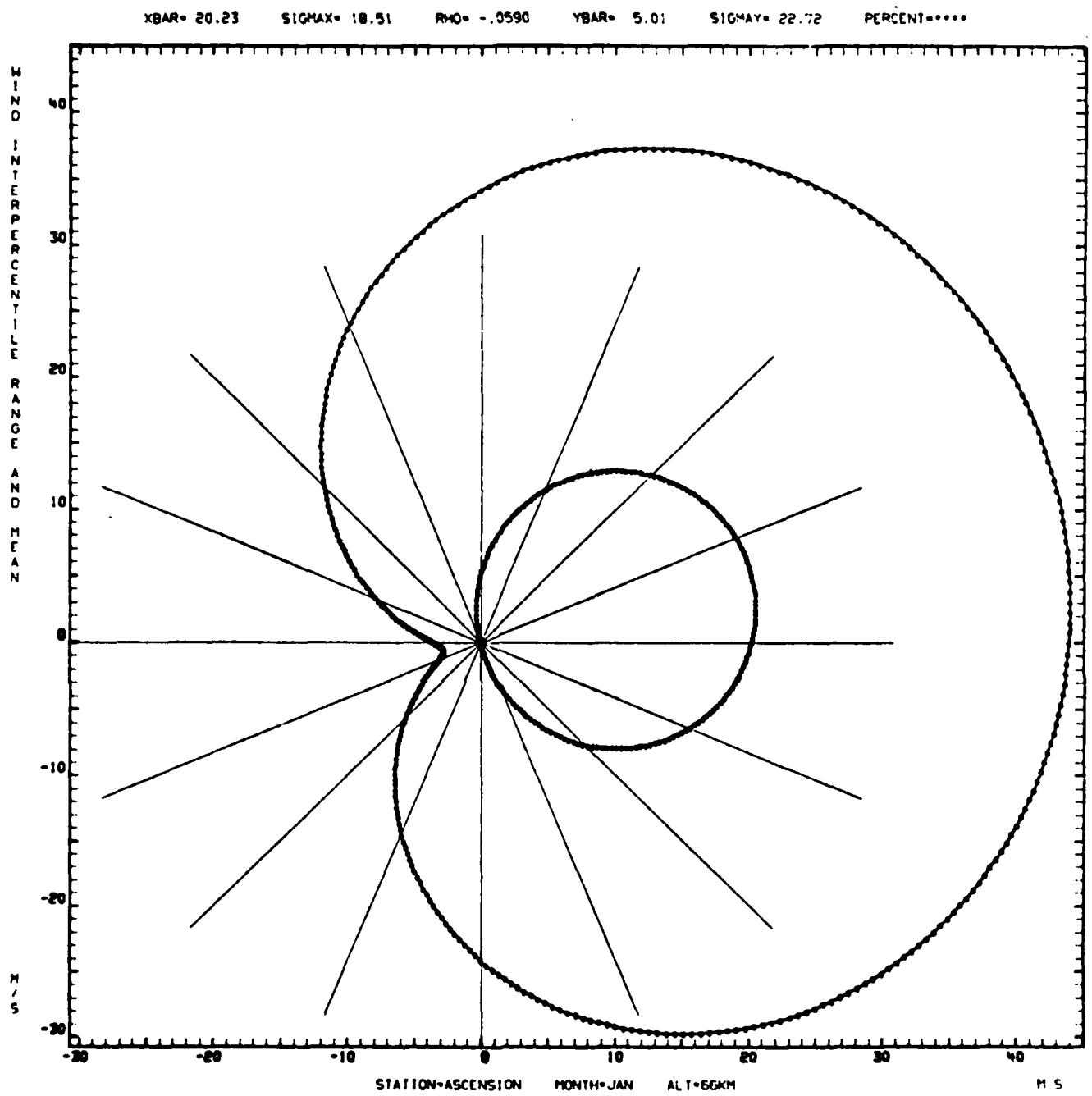


Figure A-24.

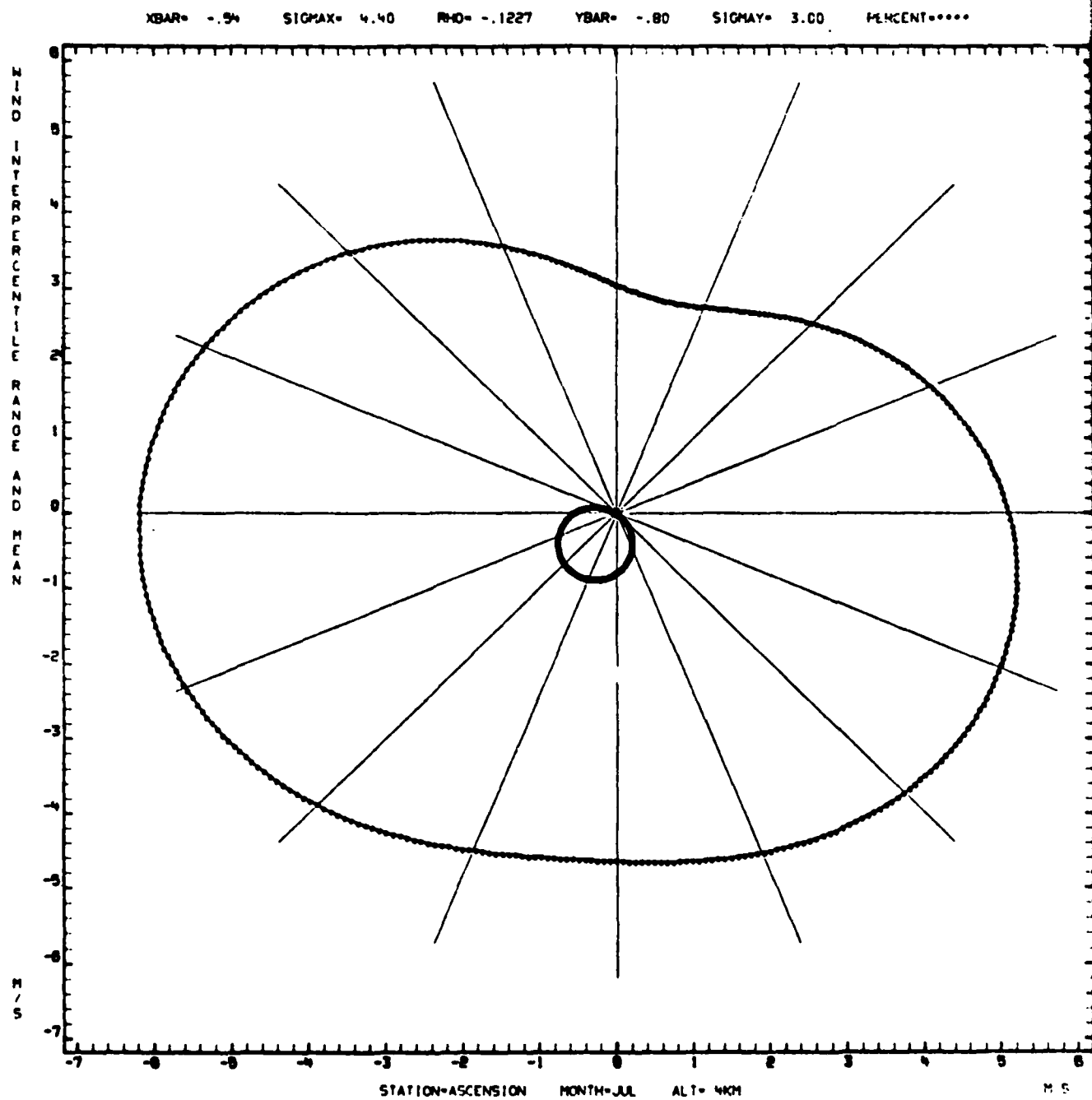


Figure A-25.

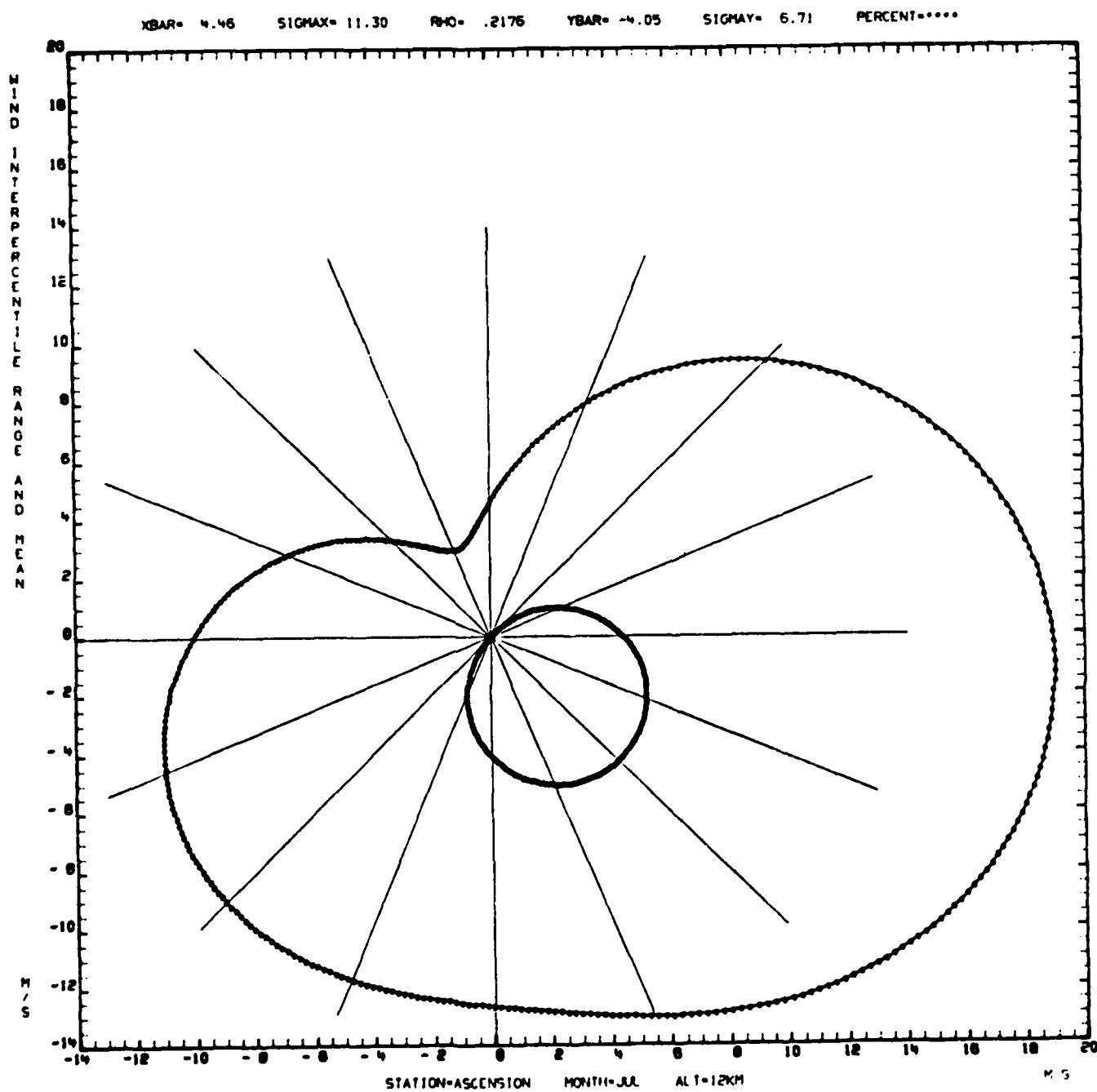


Figure A-26.



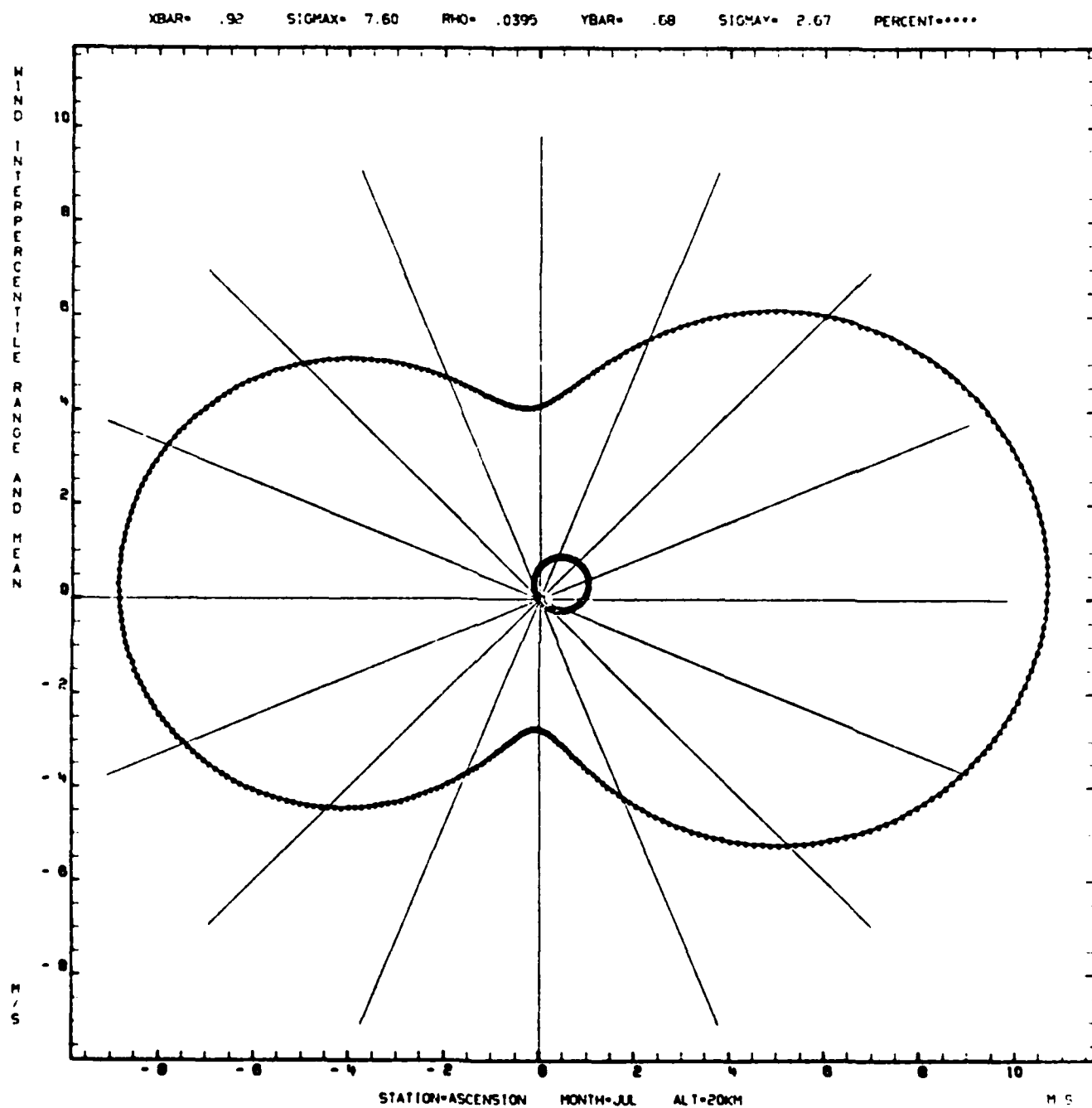


Figure A-27.

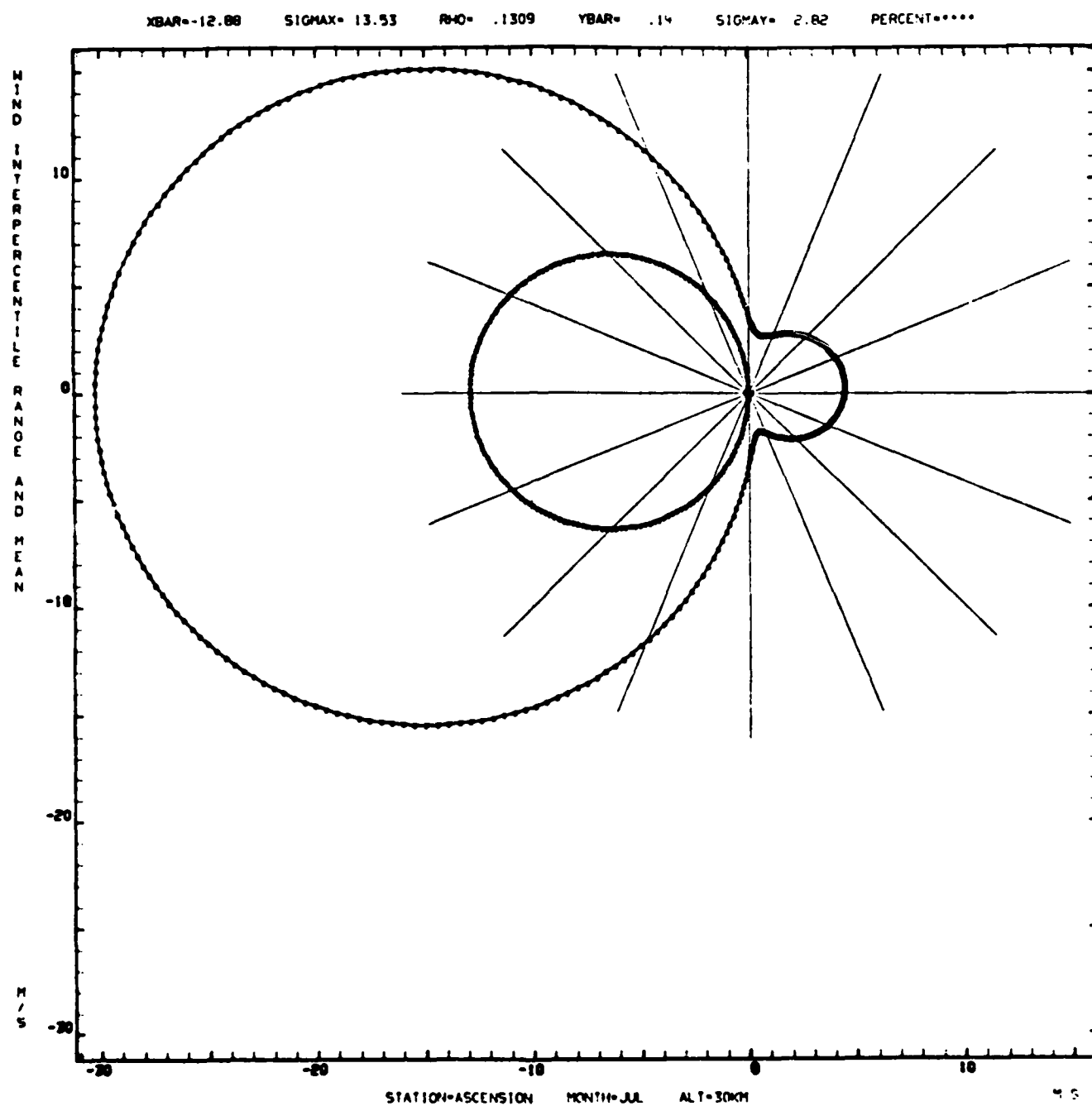


Figure A-28.

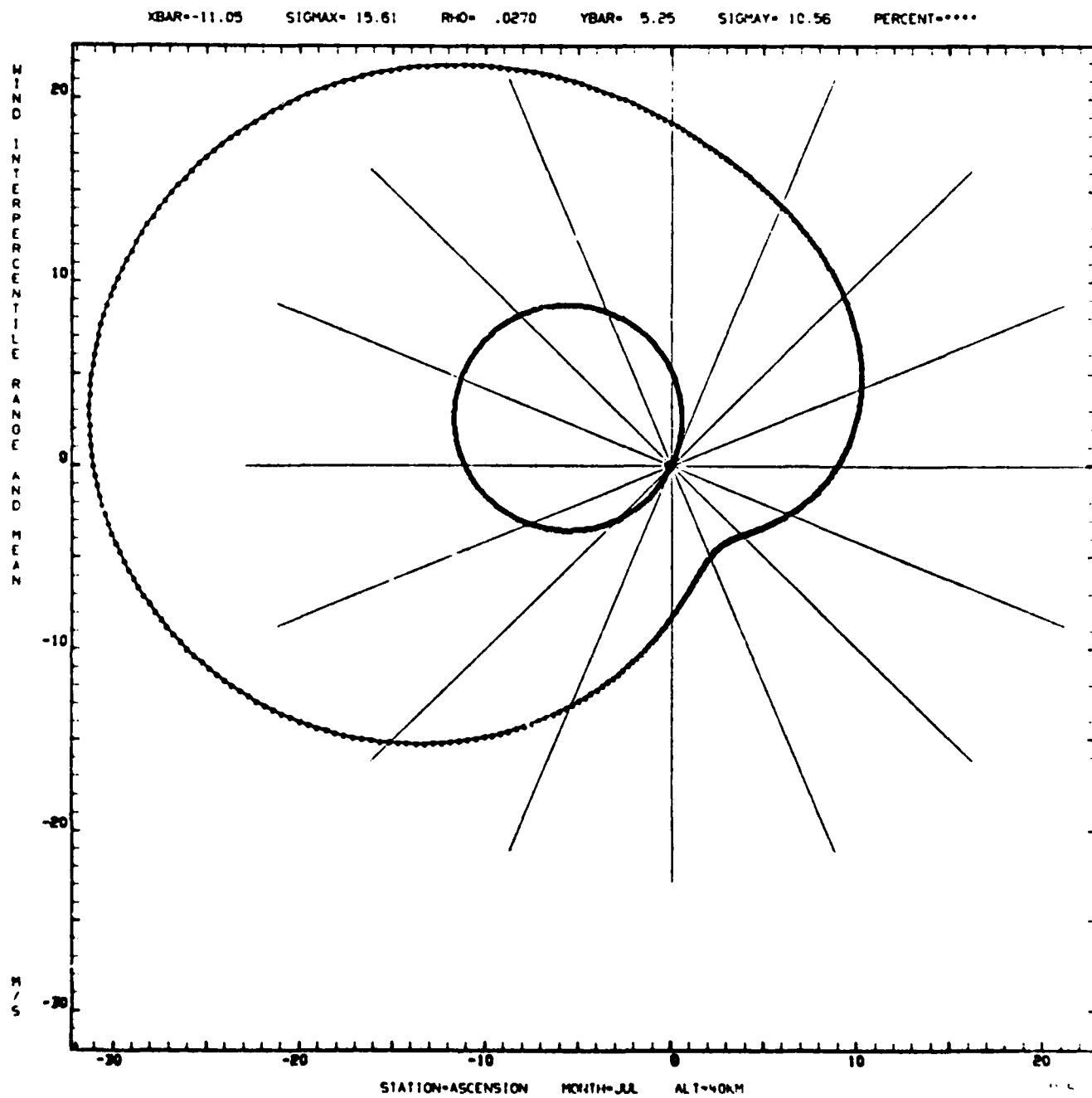


Figure A-29.

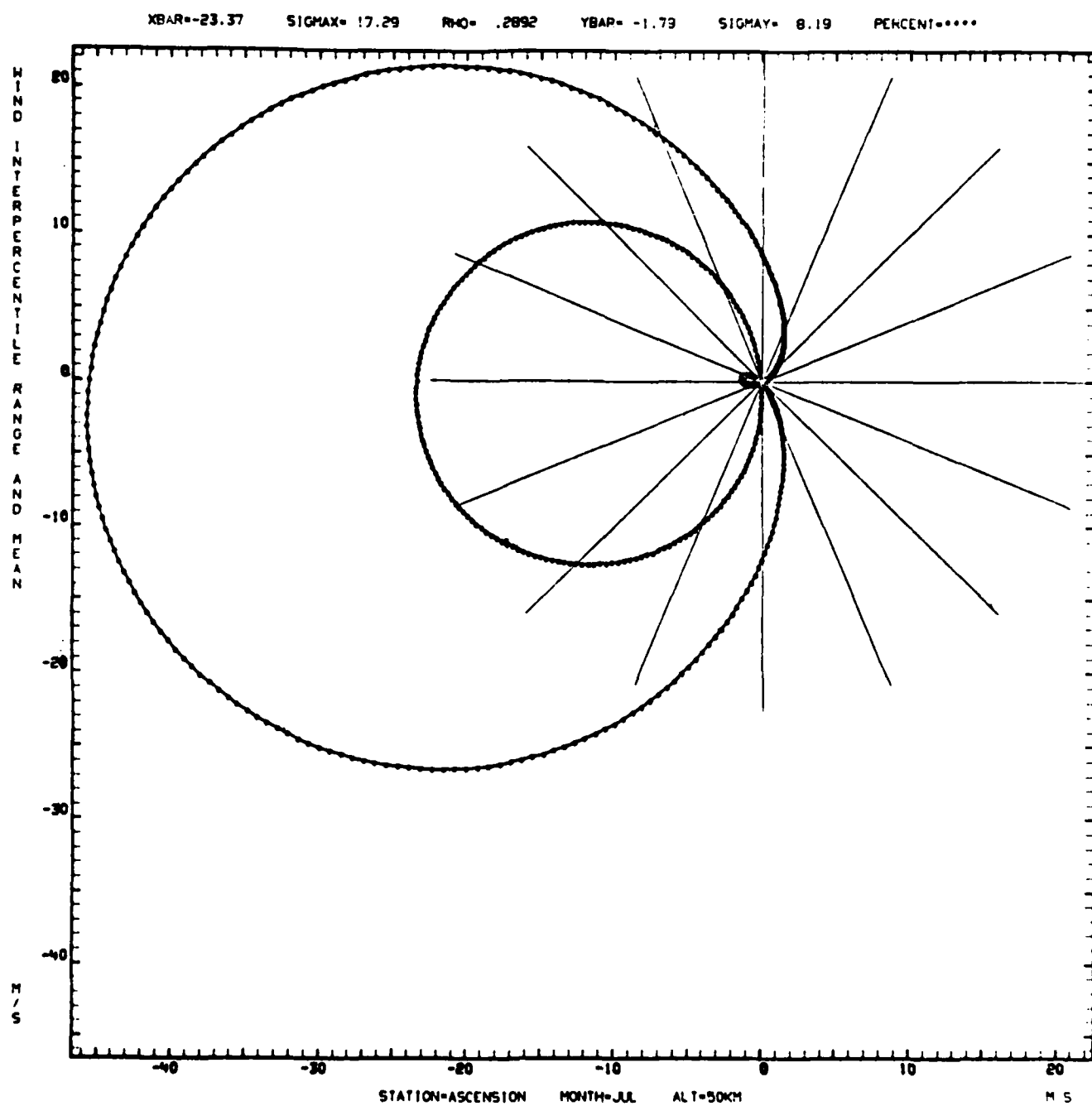


Figure A-30.

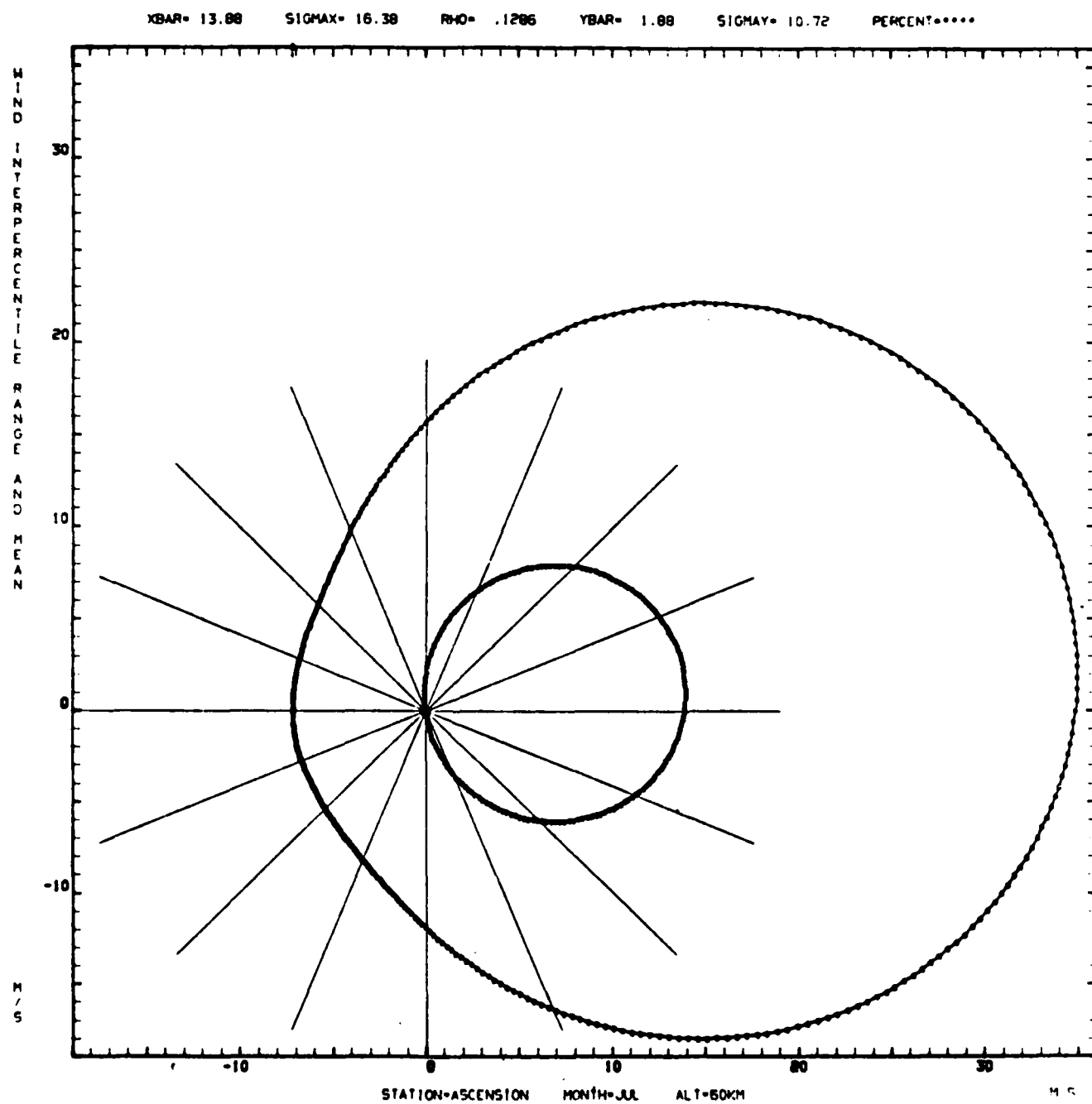


Figure A-31.

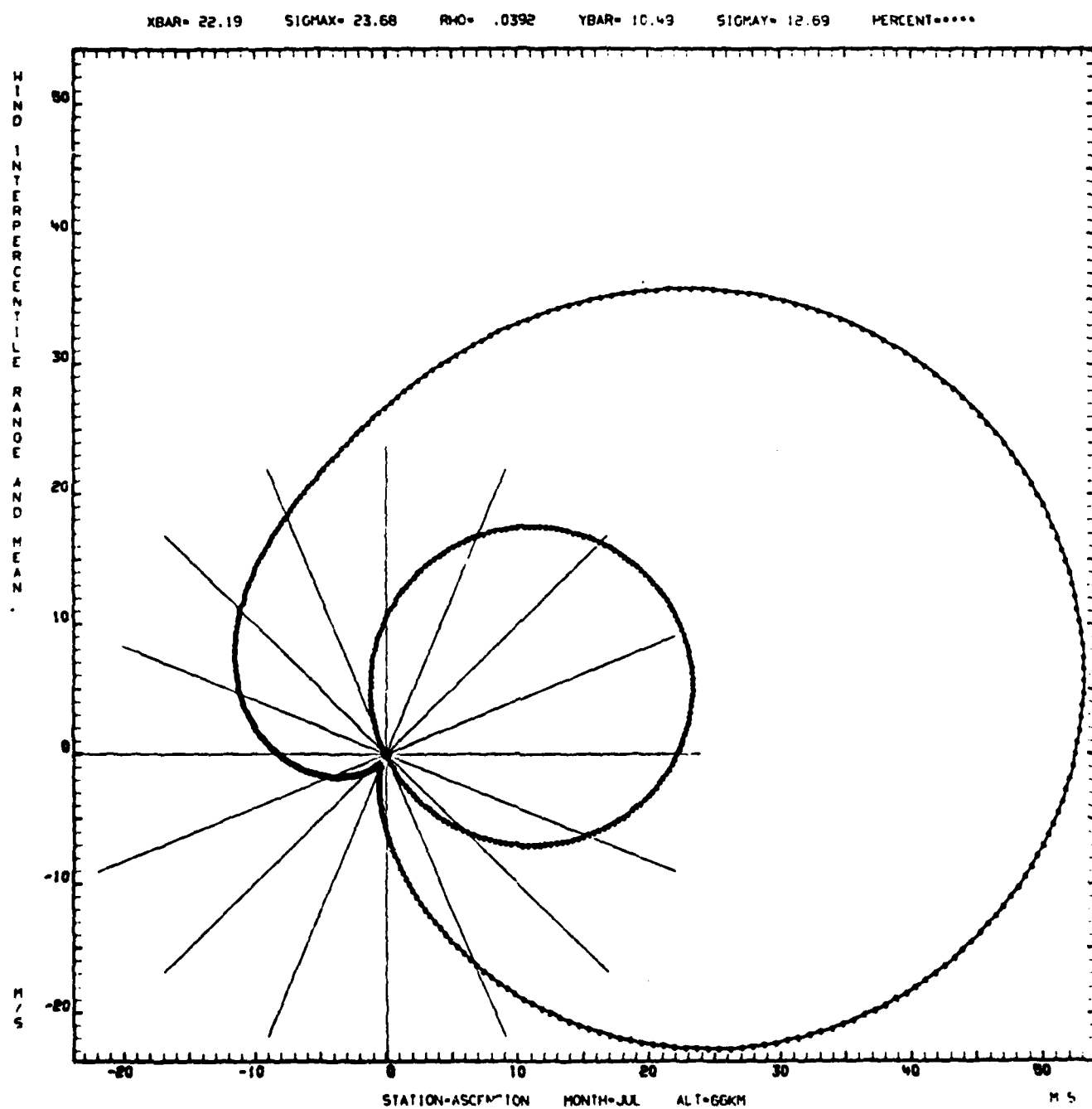


Figure A-32.

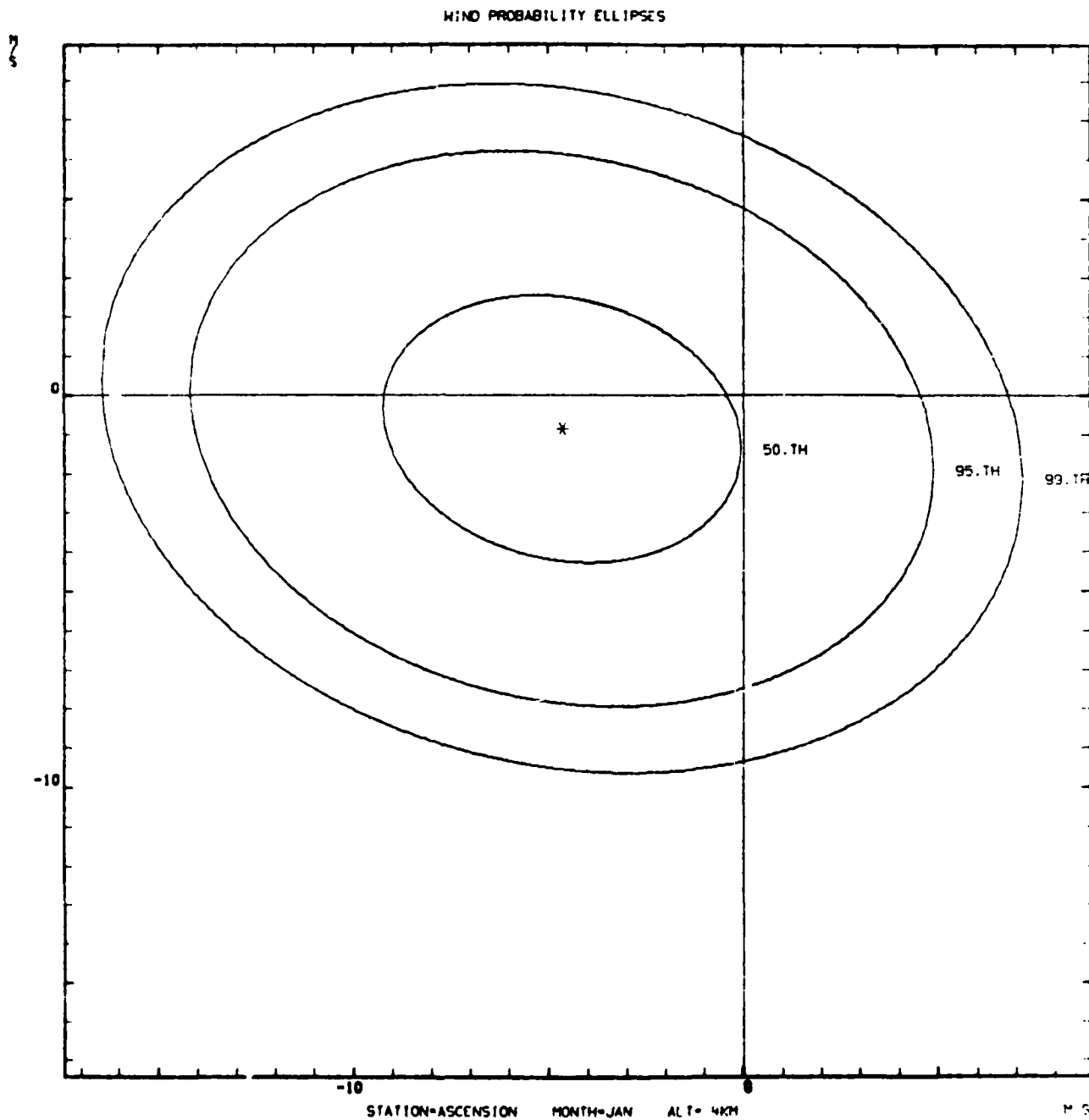


Figure A-33.

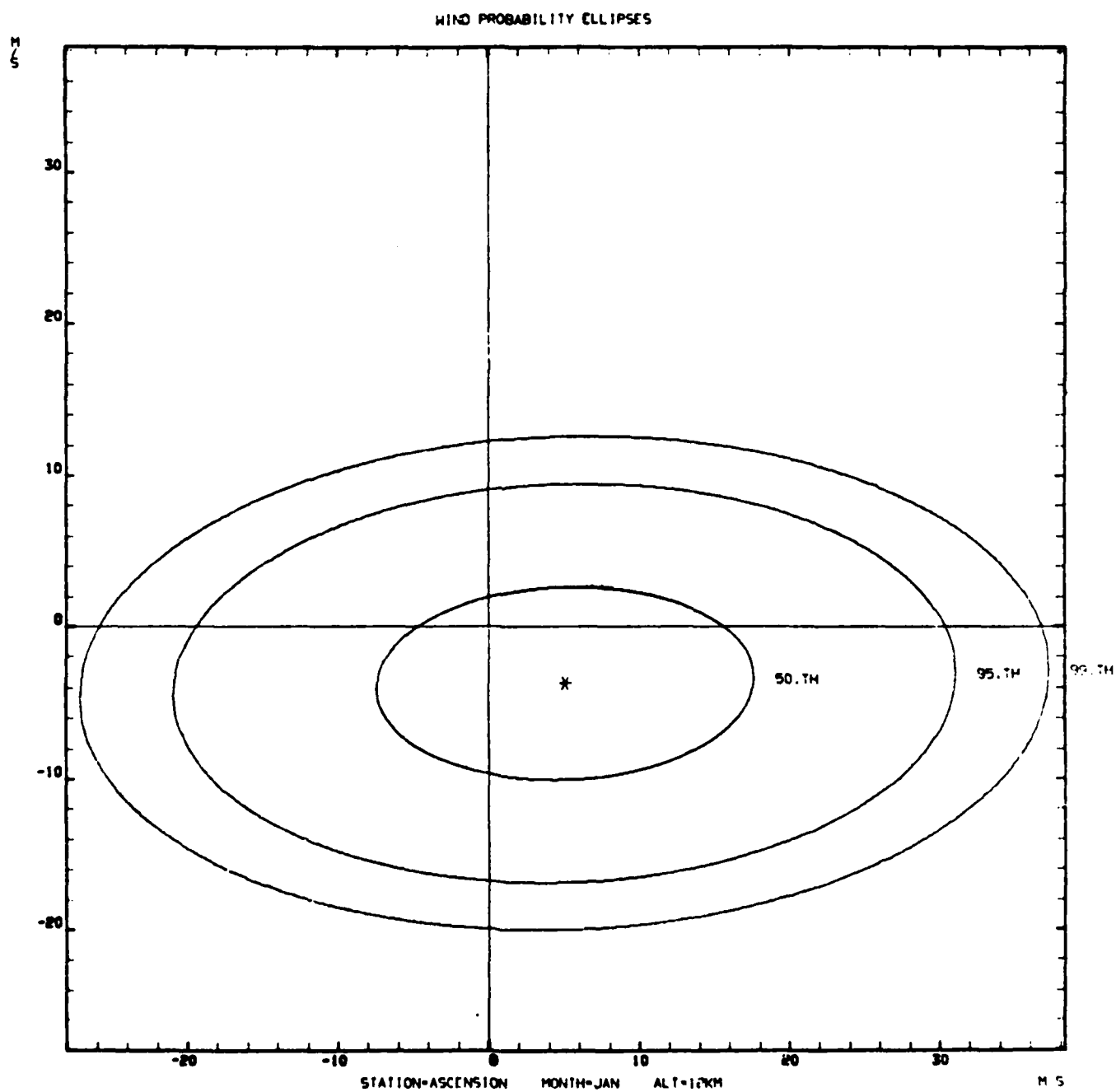


Figure A-34.



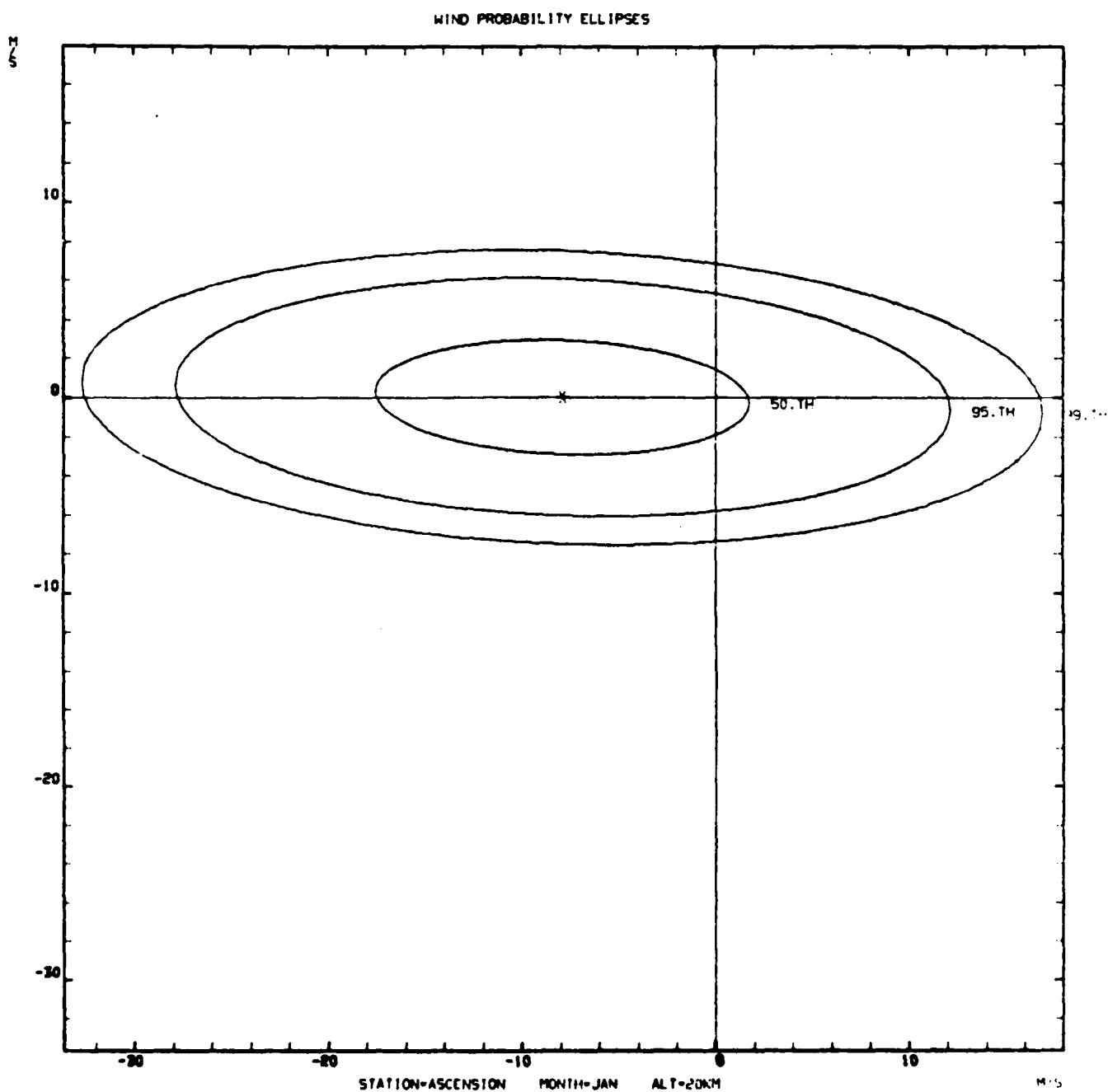


Figure A-35.

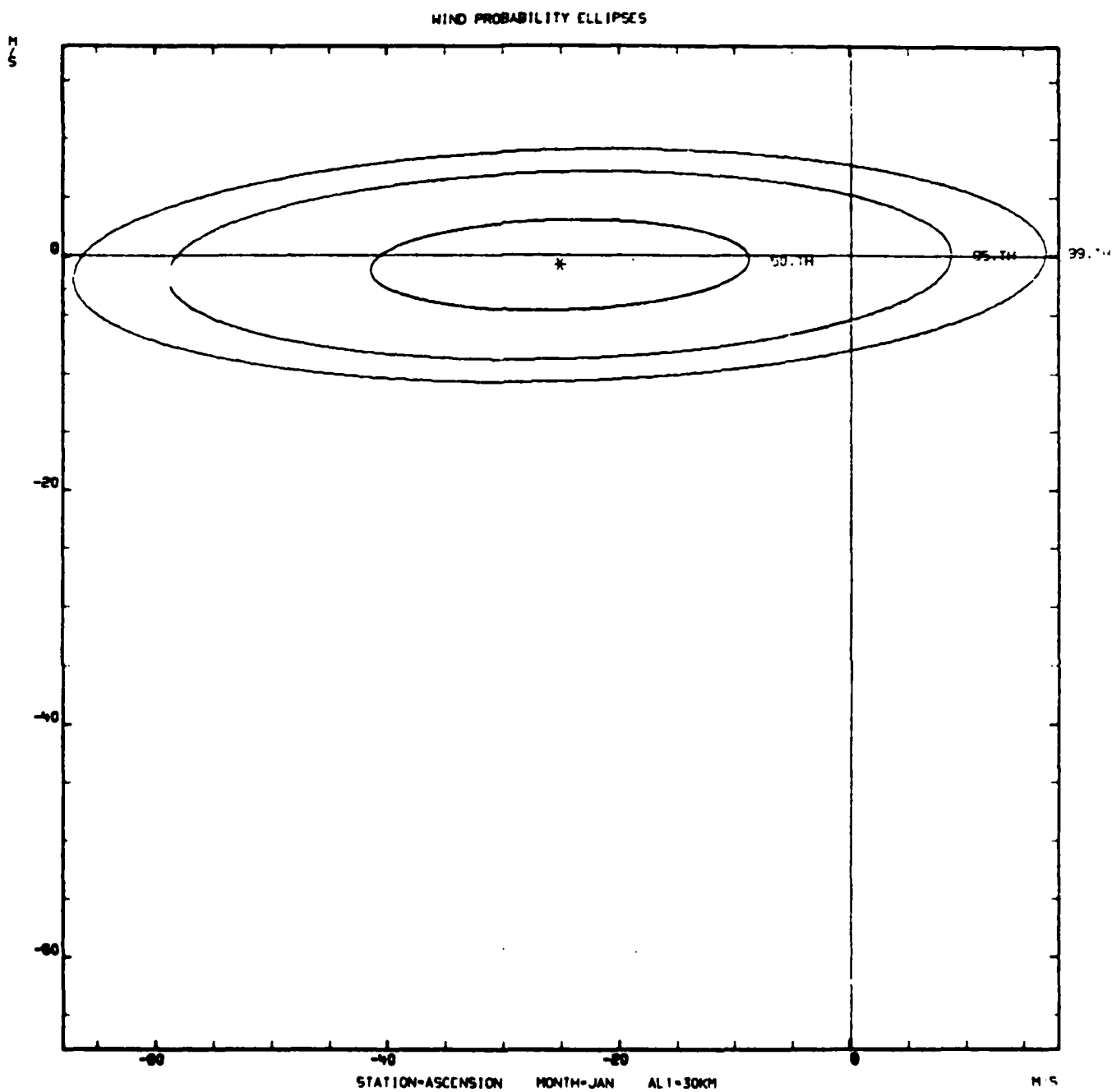


Figure A-36.

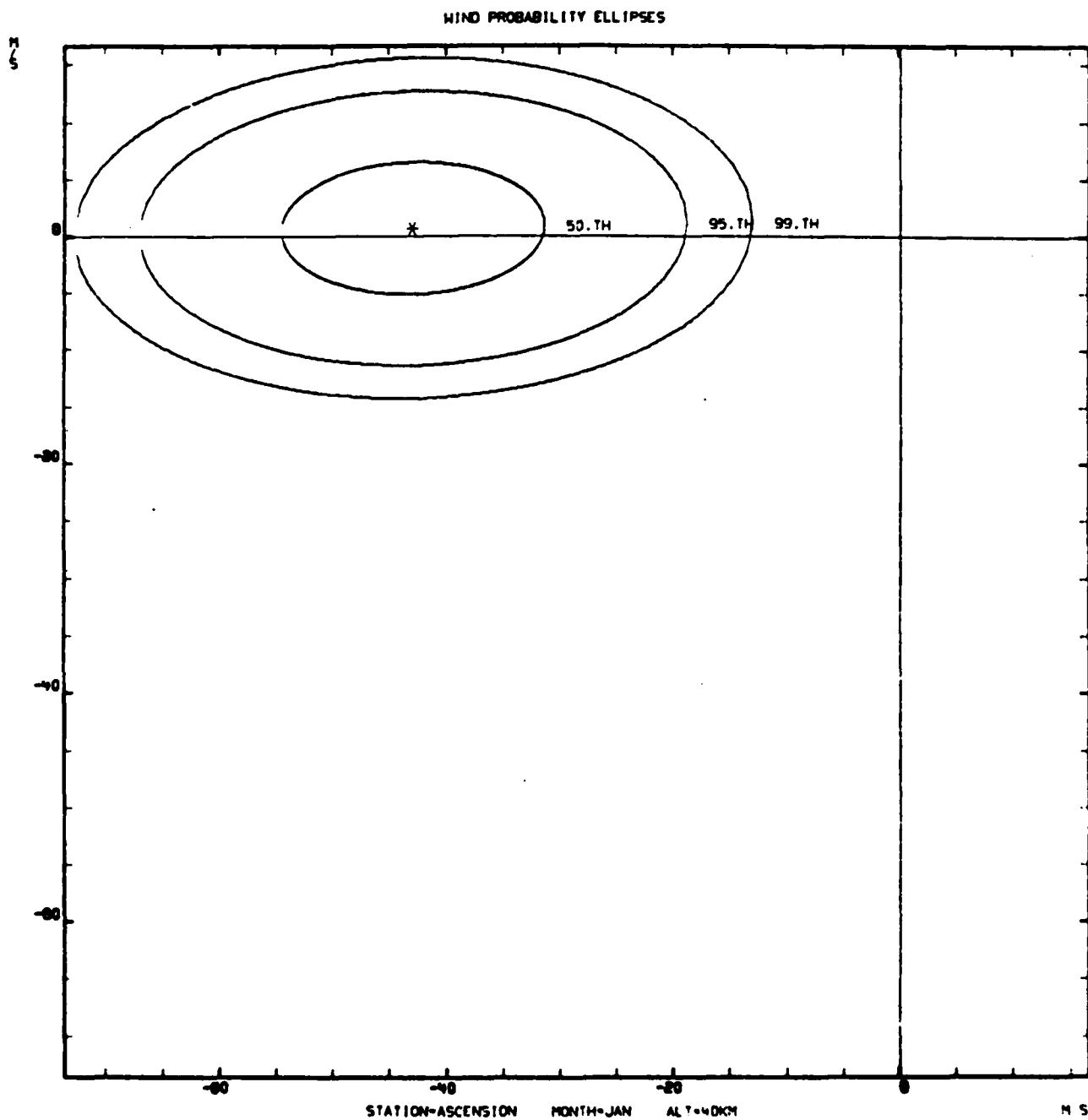


Figure A-37.

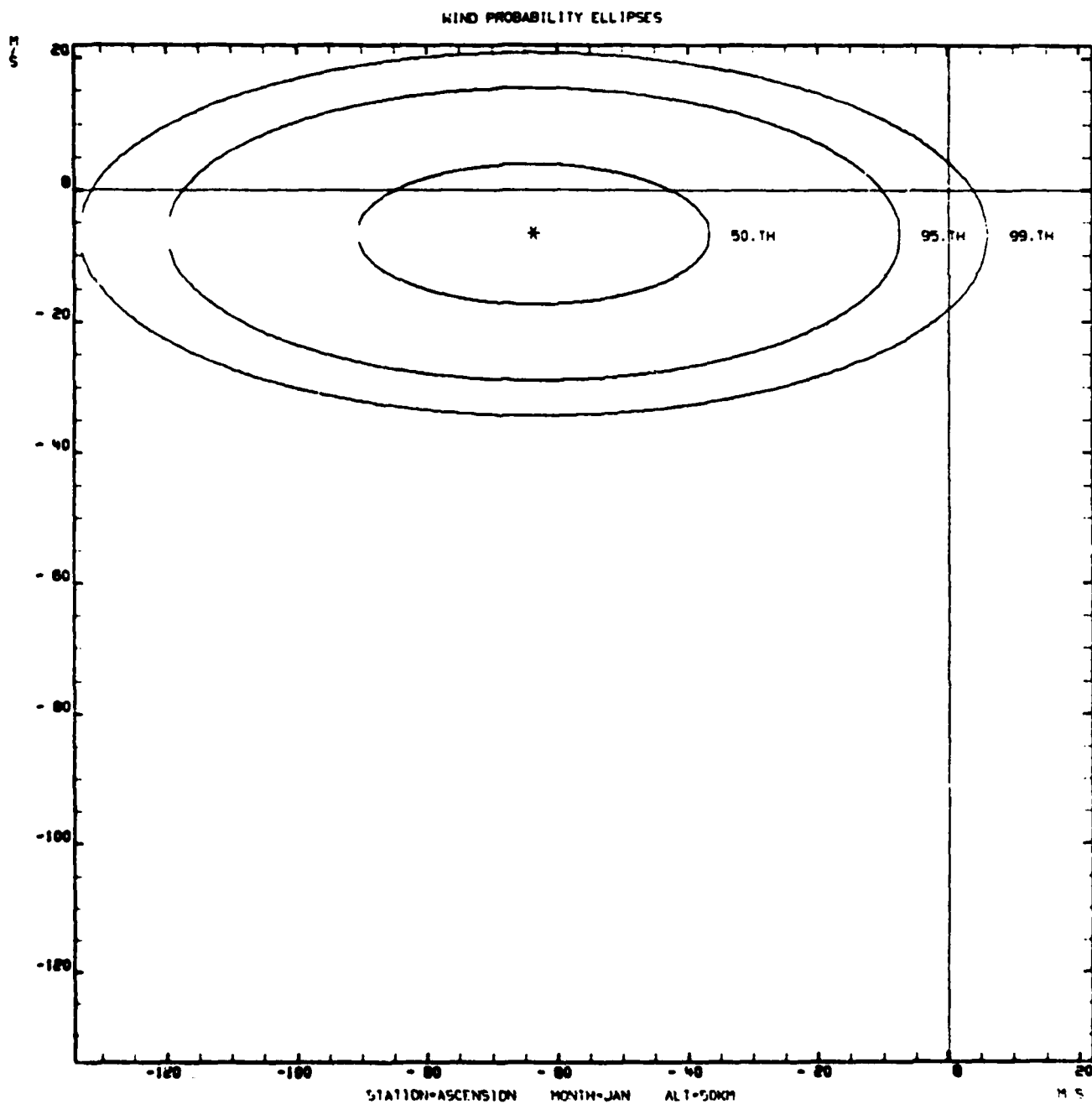


Figure A-38.

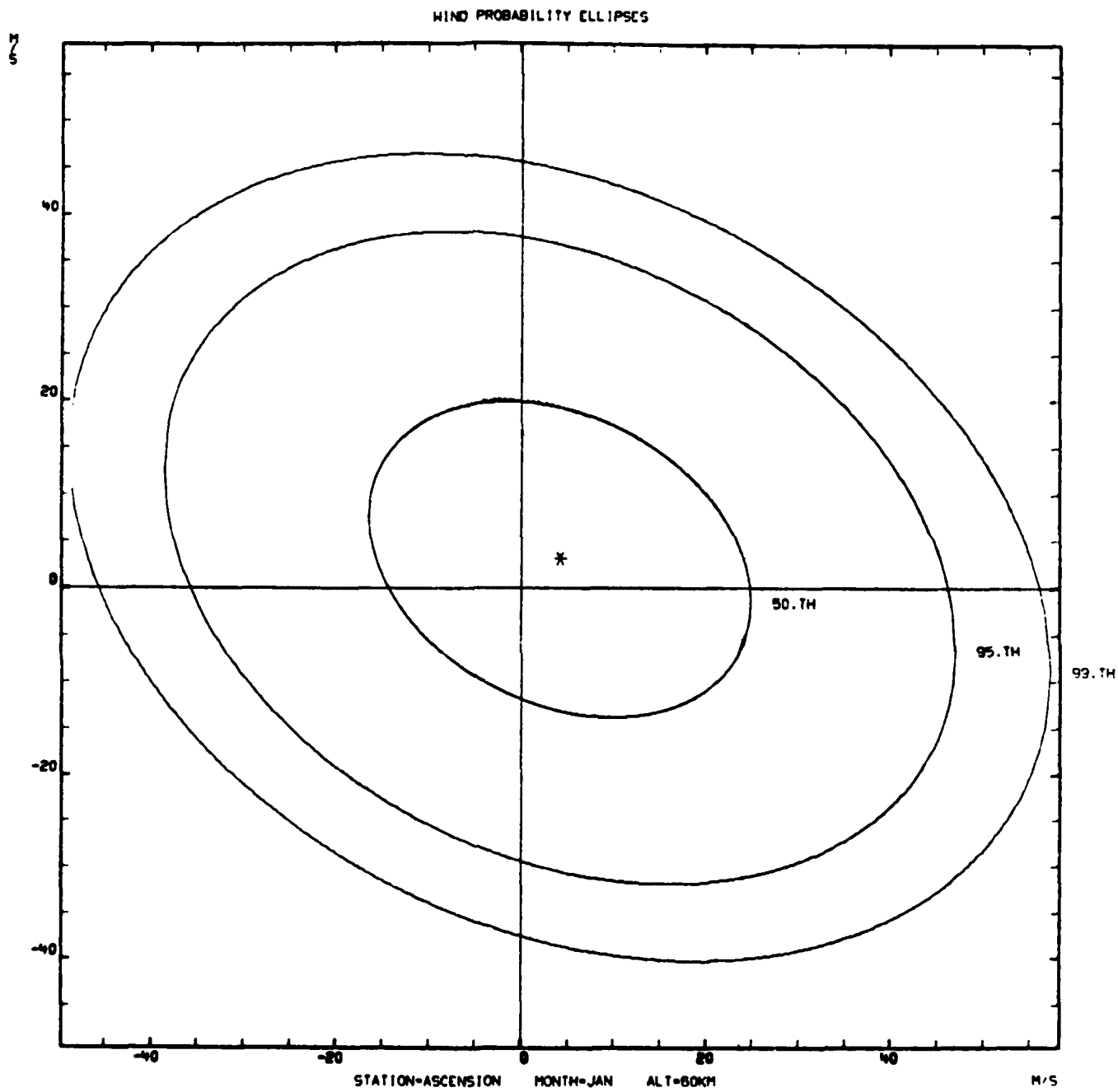


Figure A-39.

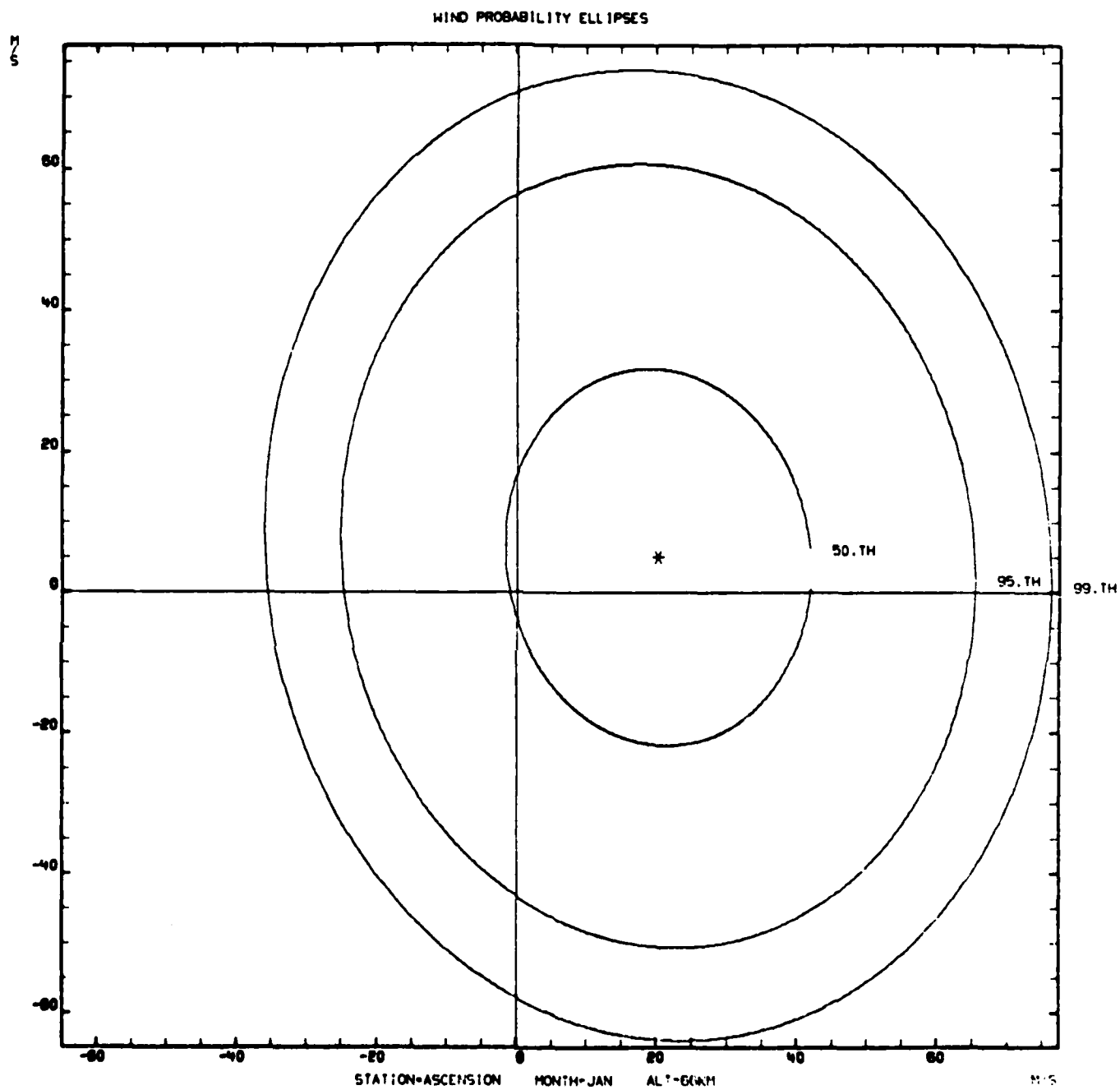


Figure A-40.

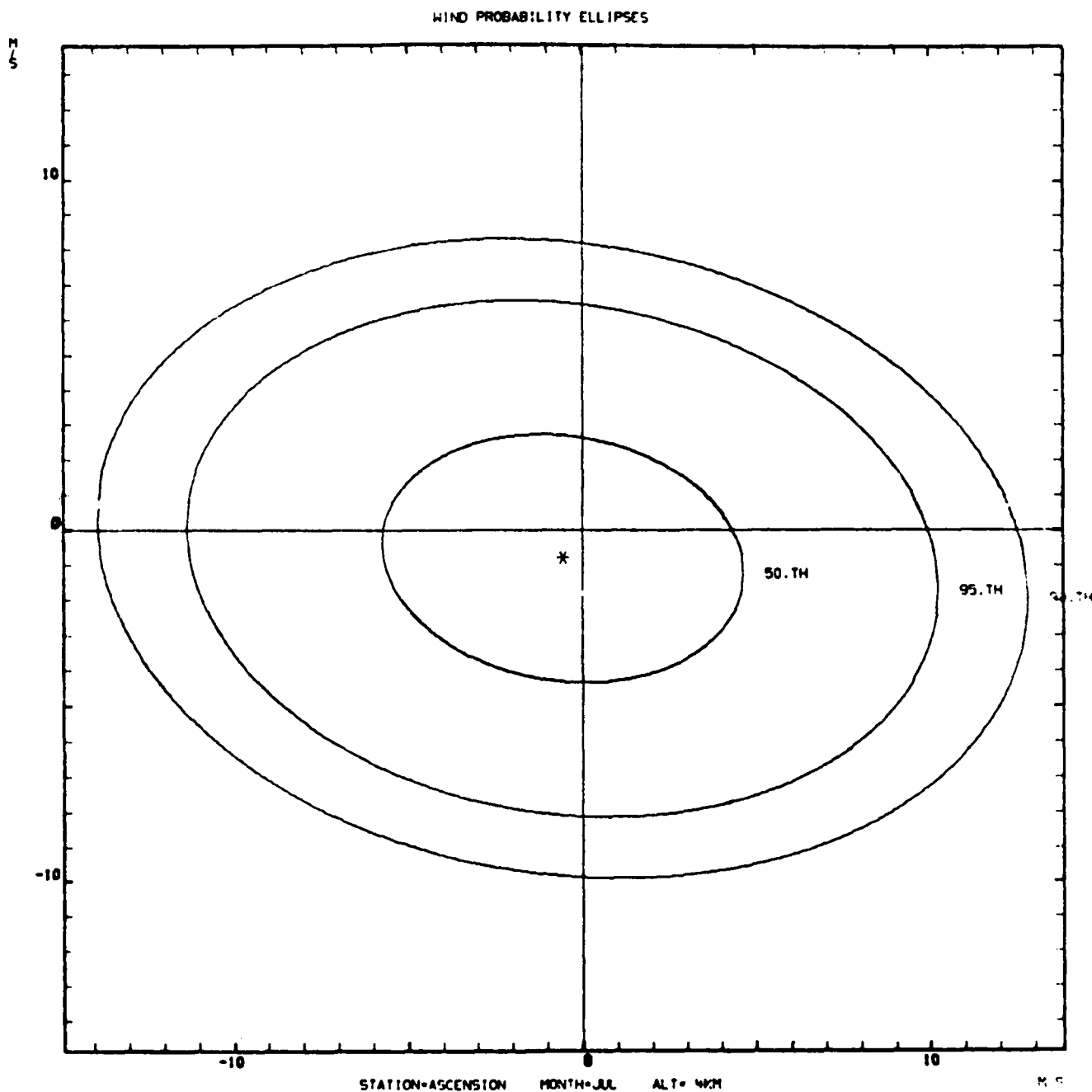


Figure A-41.

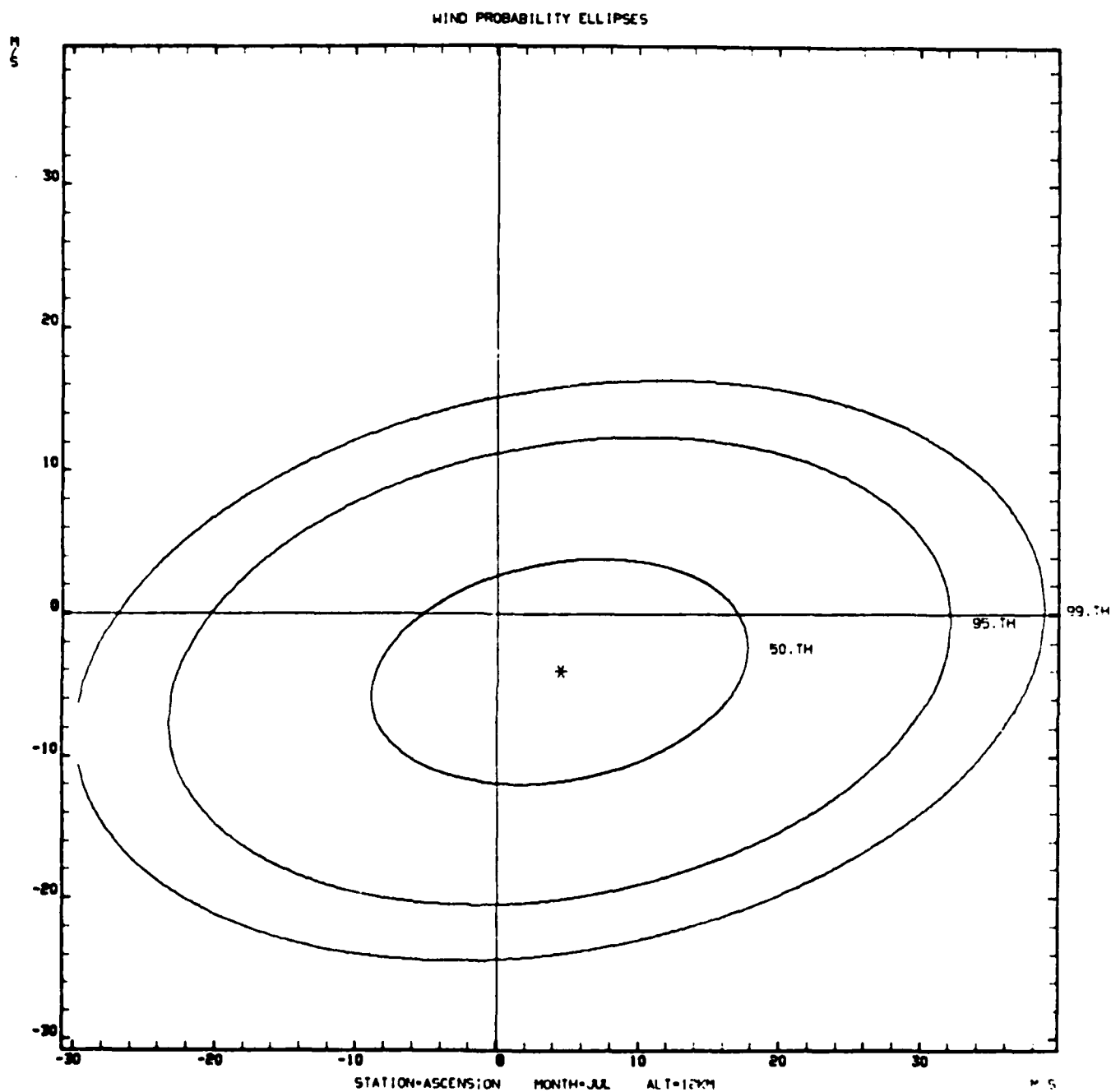


Figure A-42.



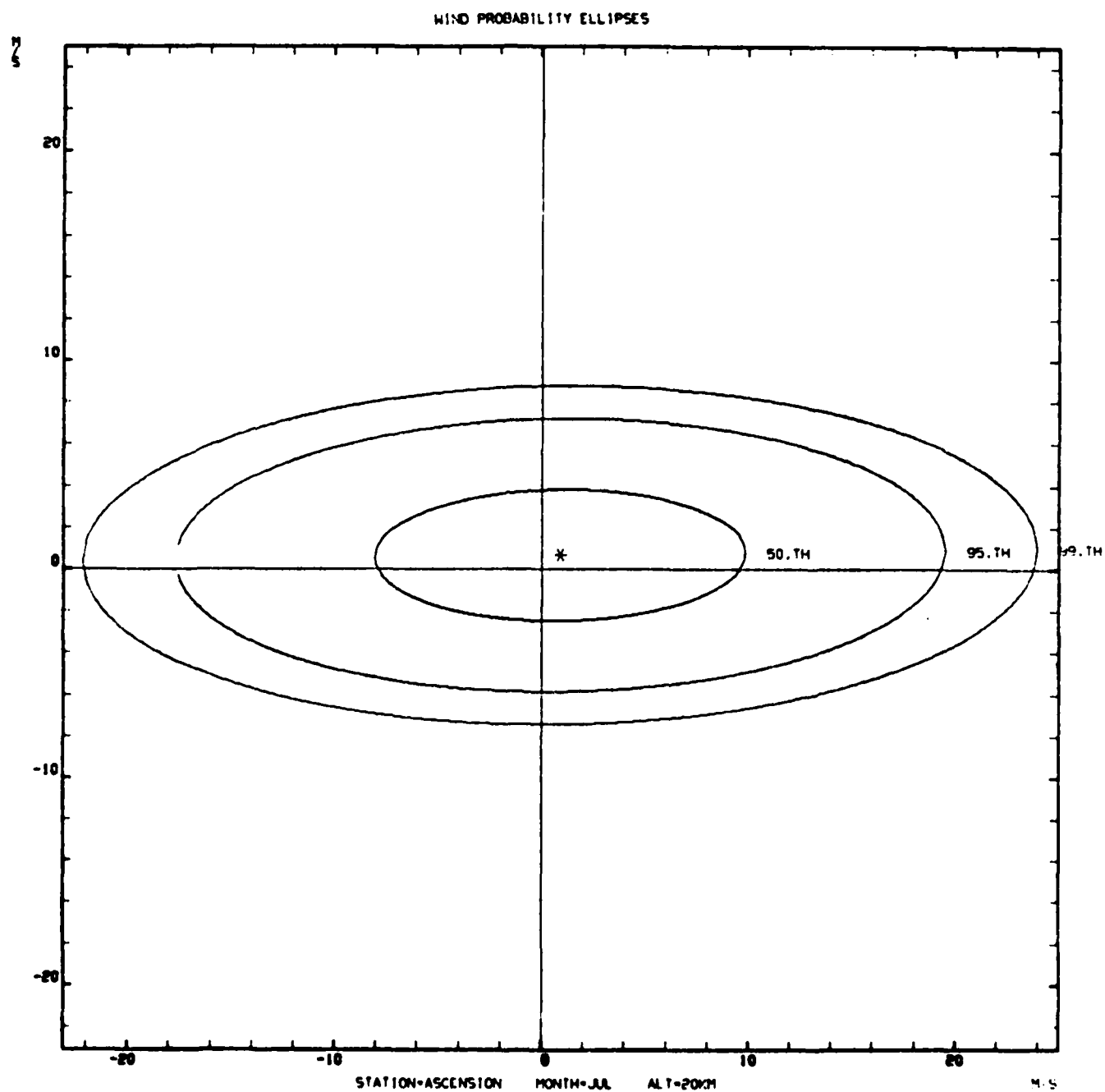


Figure A-43.

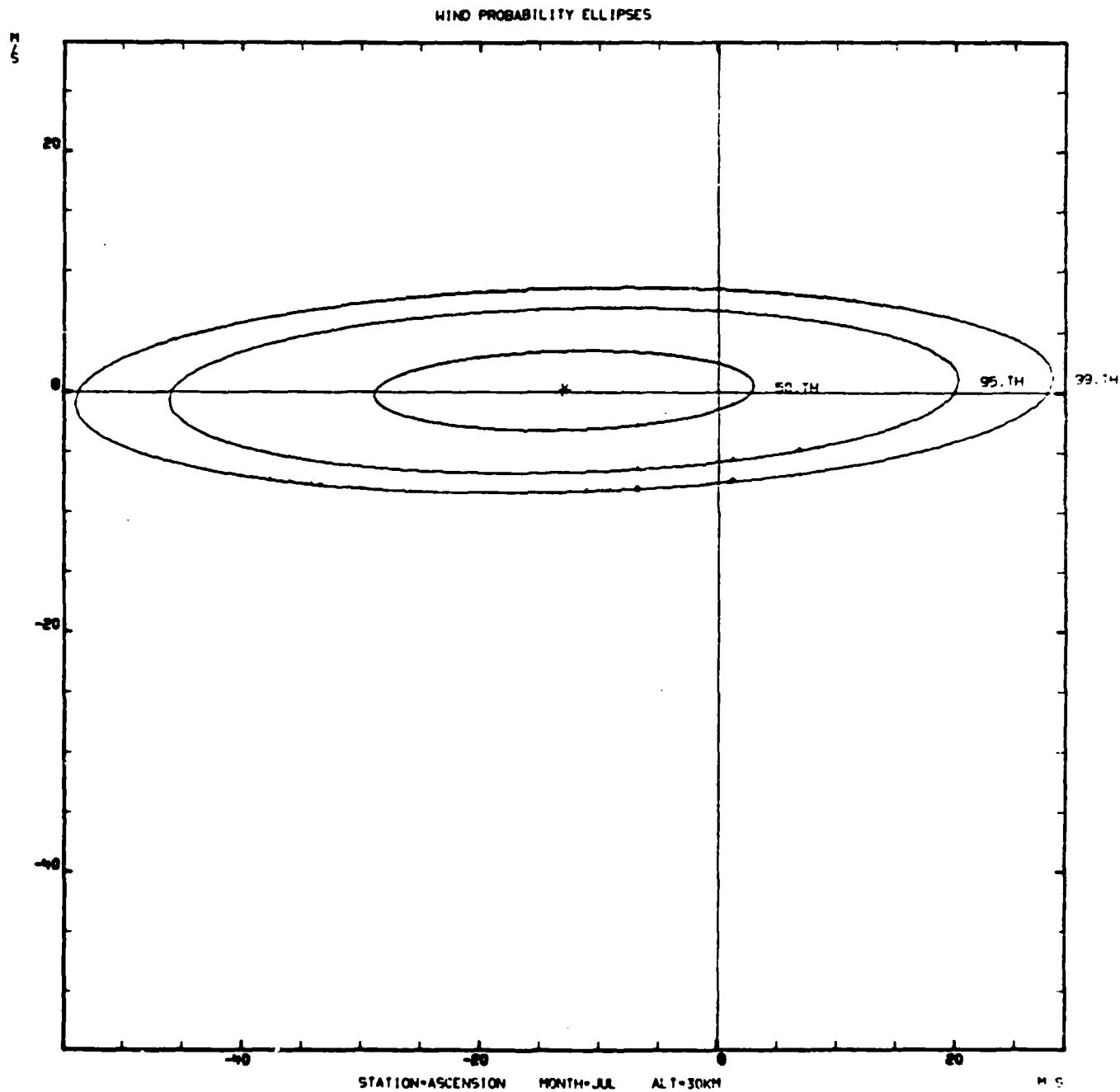


Figure A-44.

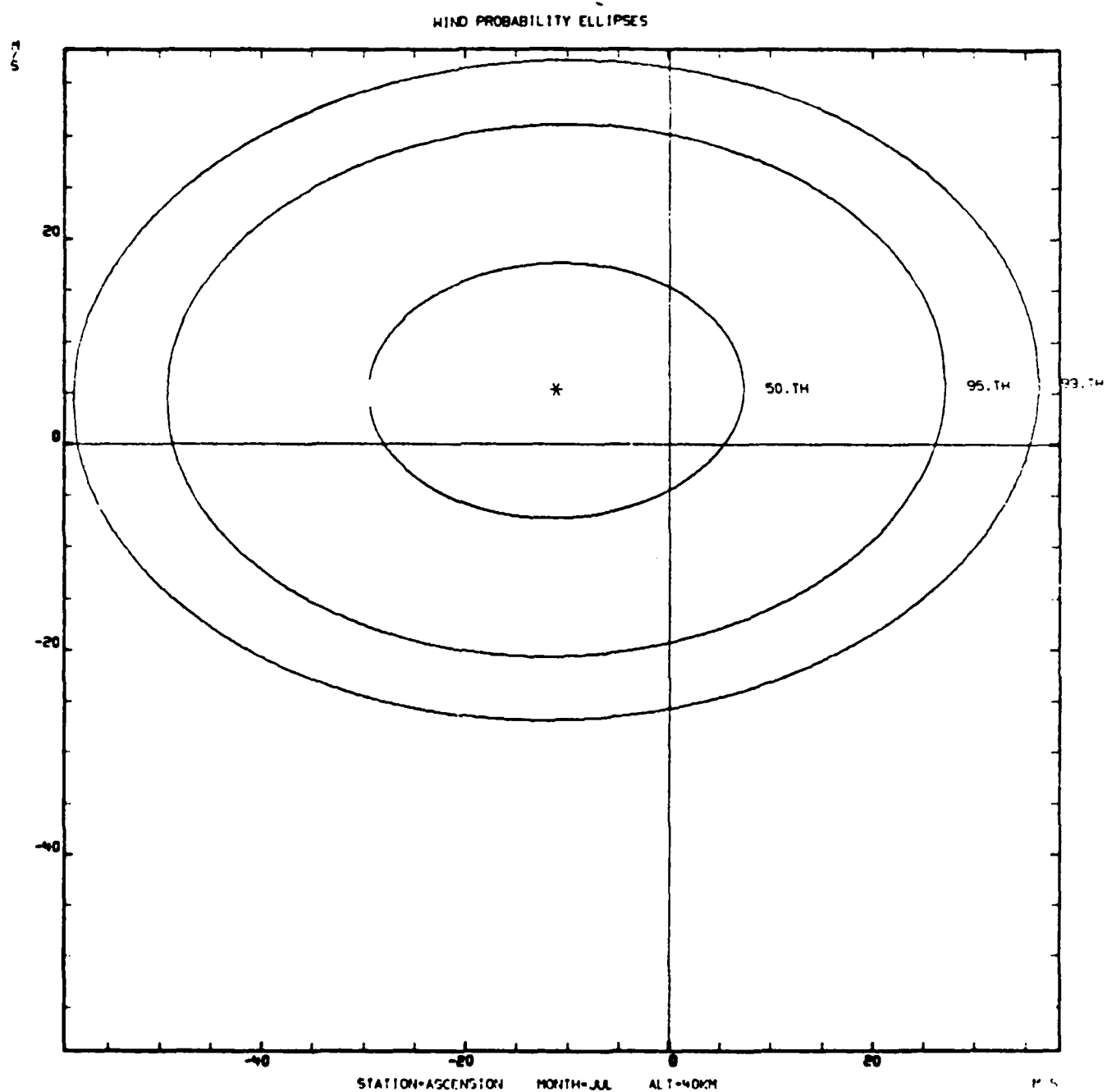


Figure A-45.

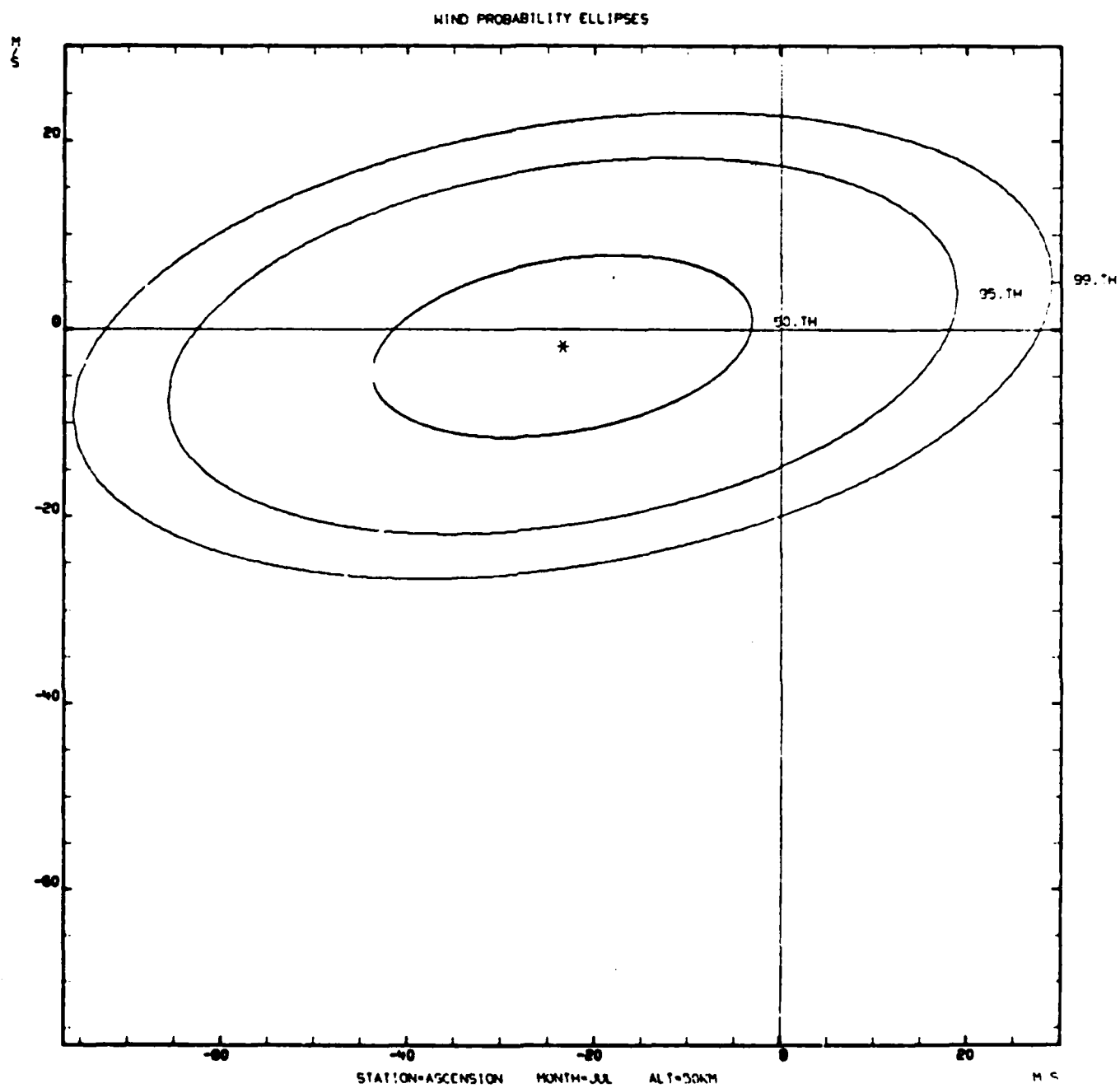


Figure A-46.

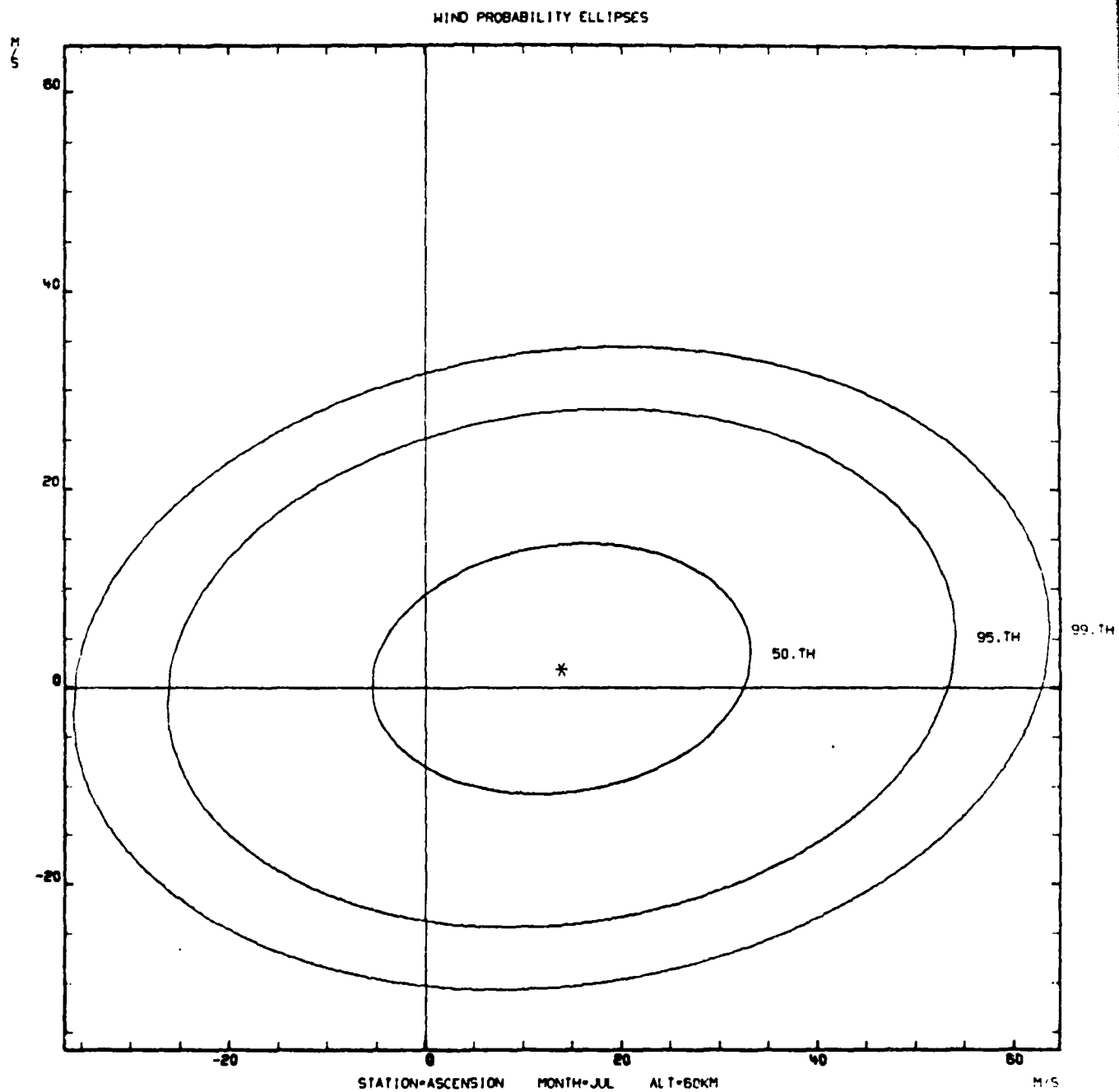


Figure A-47.

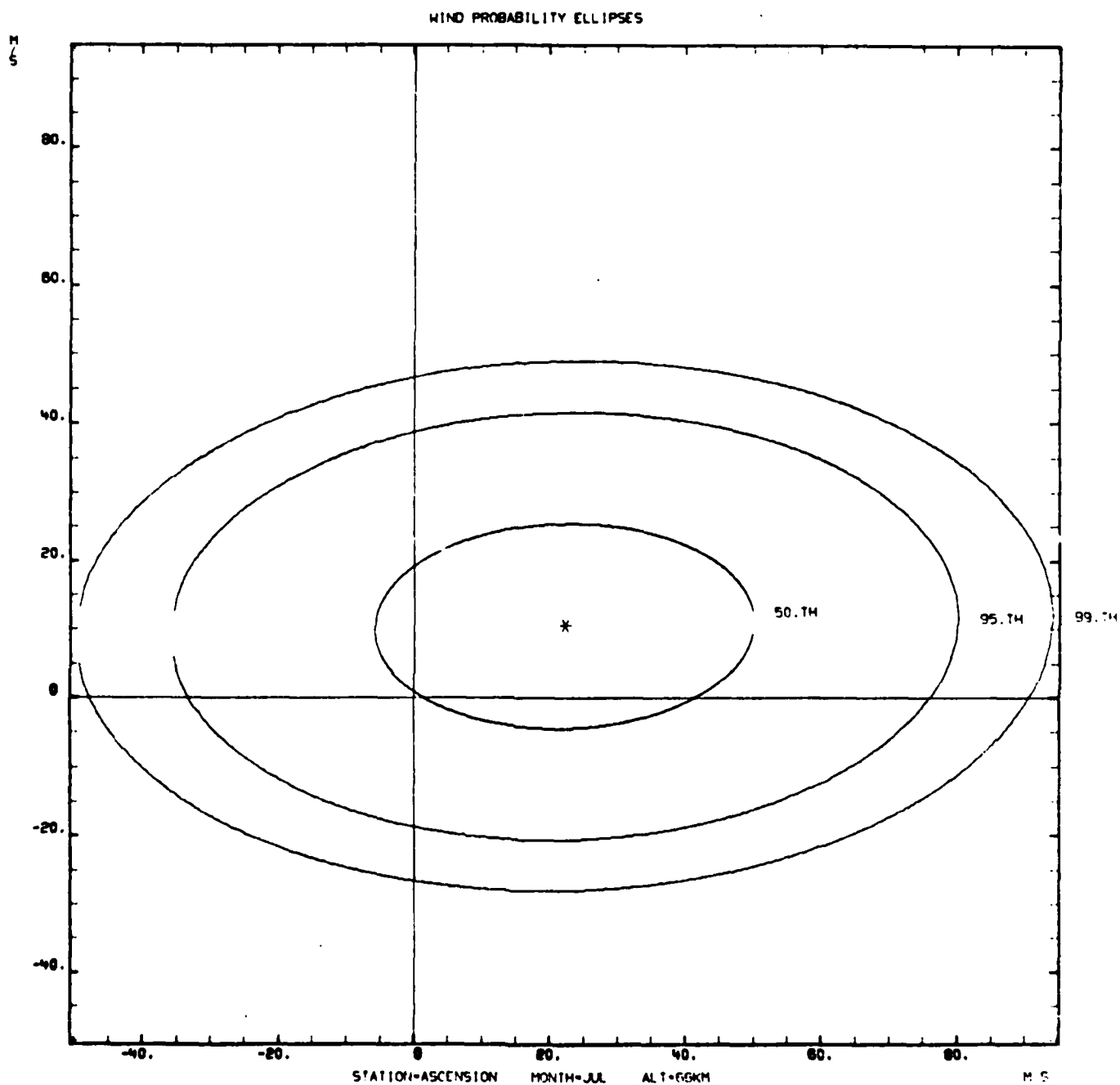


Figure A-48.

STATION-ASCENSION MONTH-JAN ALT= 4KM

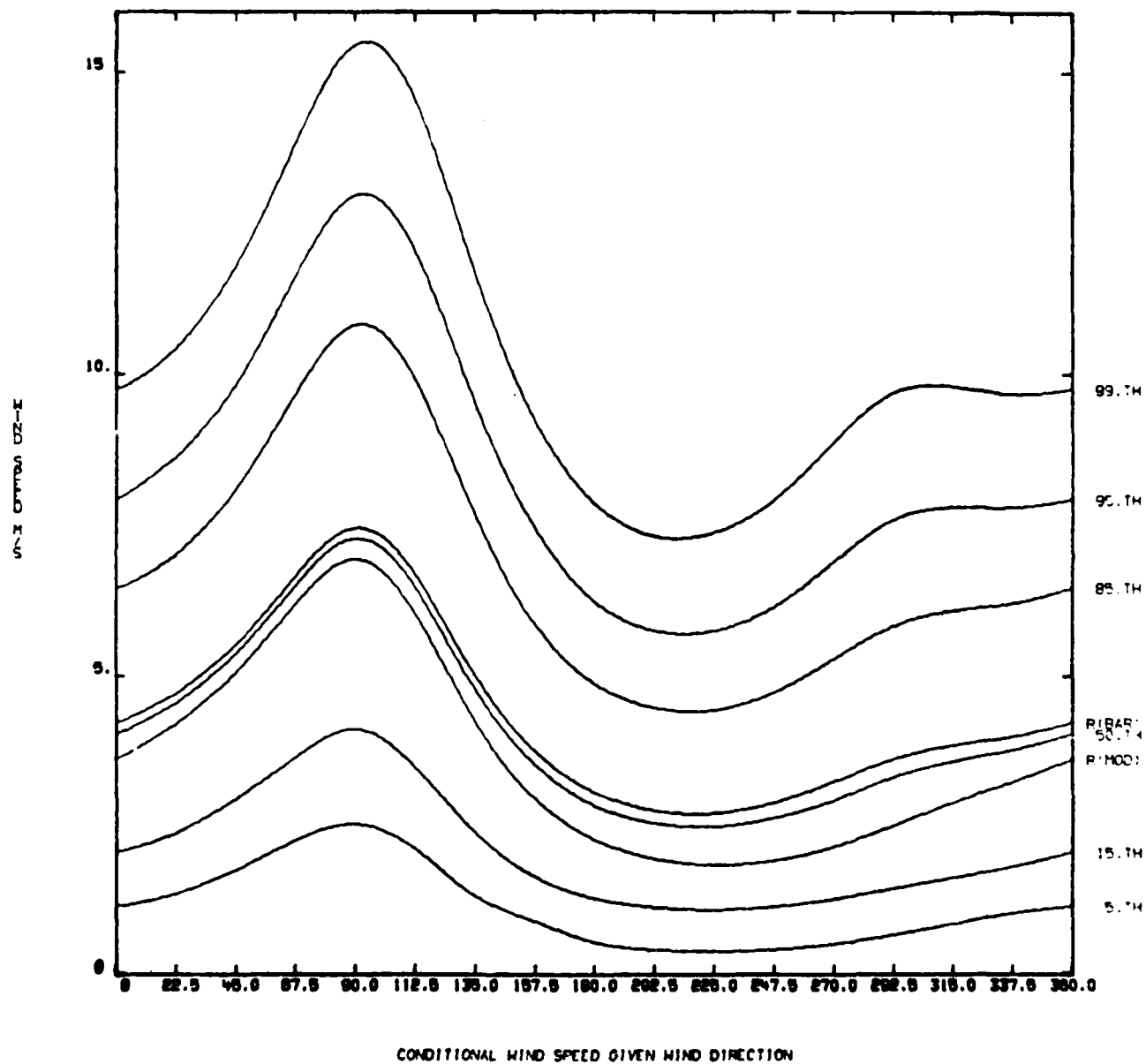


Figure A-49.

STATION-ASCENSION MONTH-JAN ALT-12KM

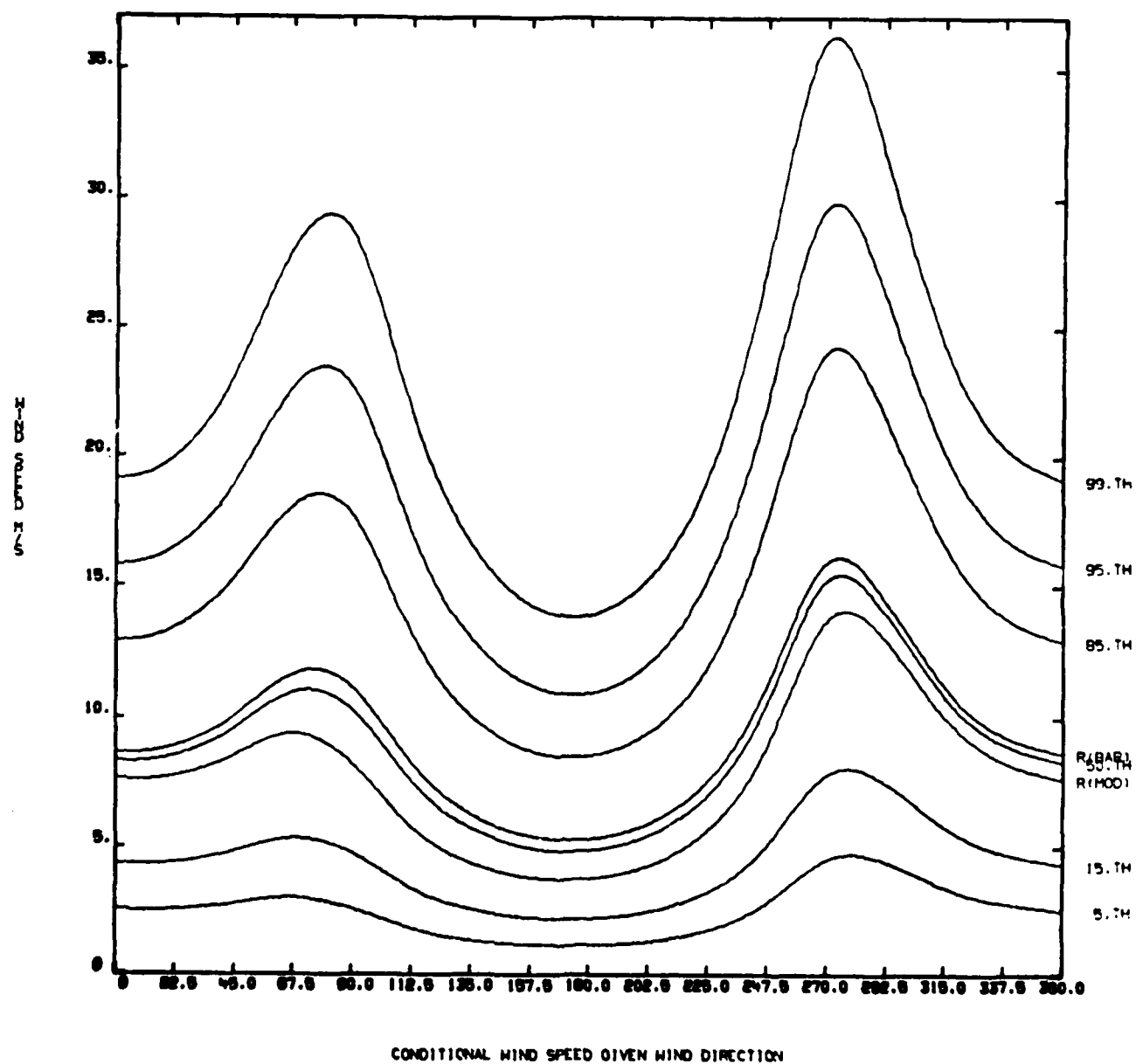


Figure A-50.



STATION=ASCENSION MONTH=JAN ALT=20KM

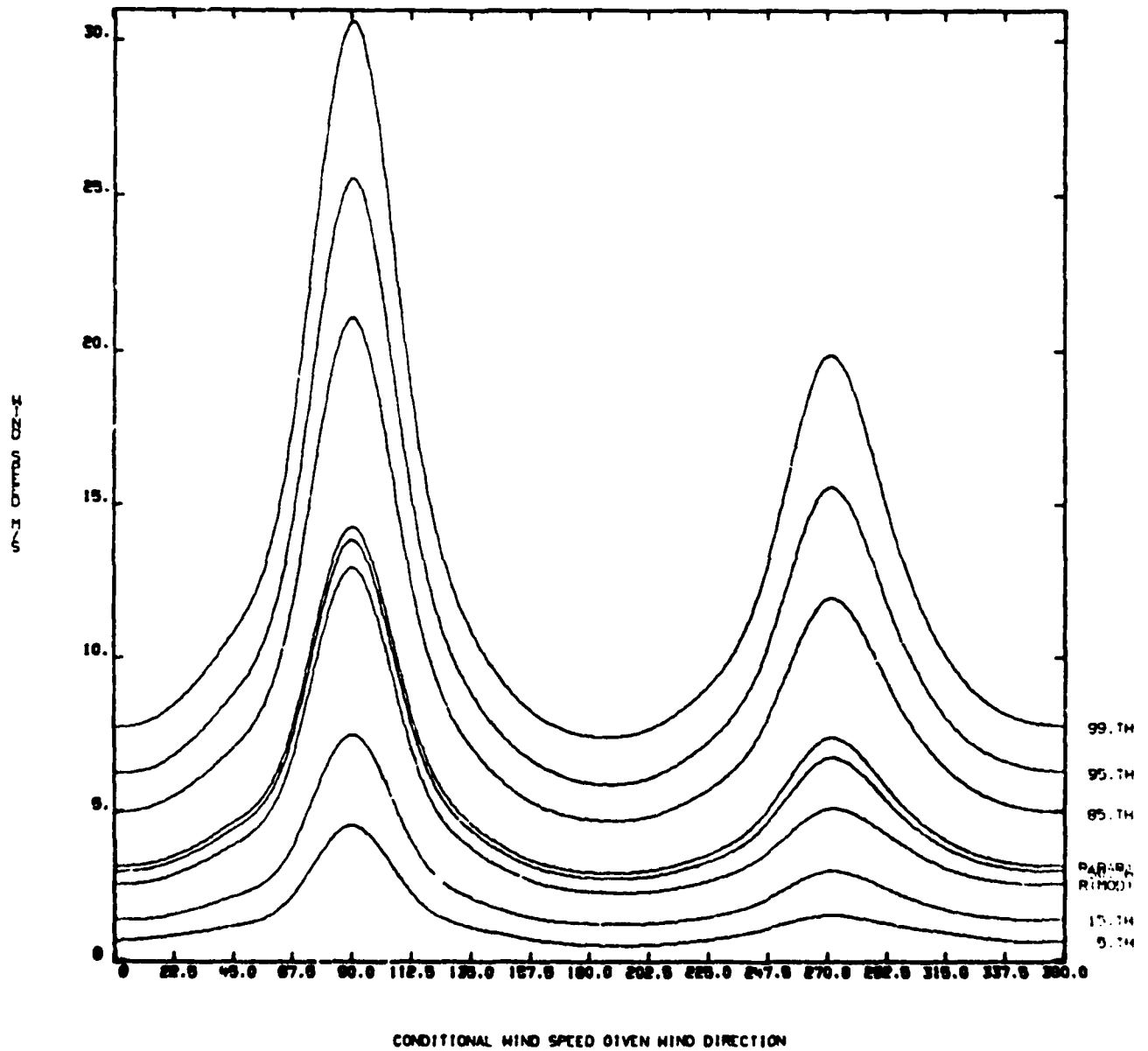


Figure A-51.

STATION=ASCENSION MONTH=JAN ALT=30KM

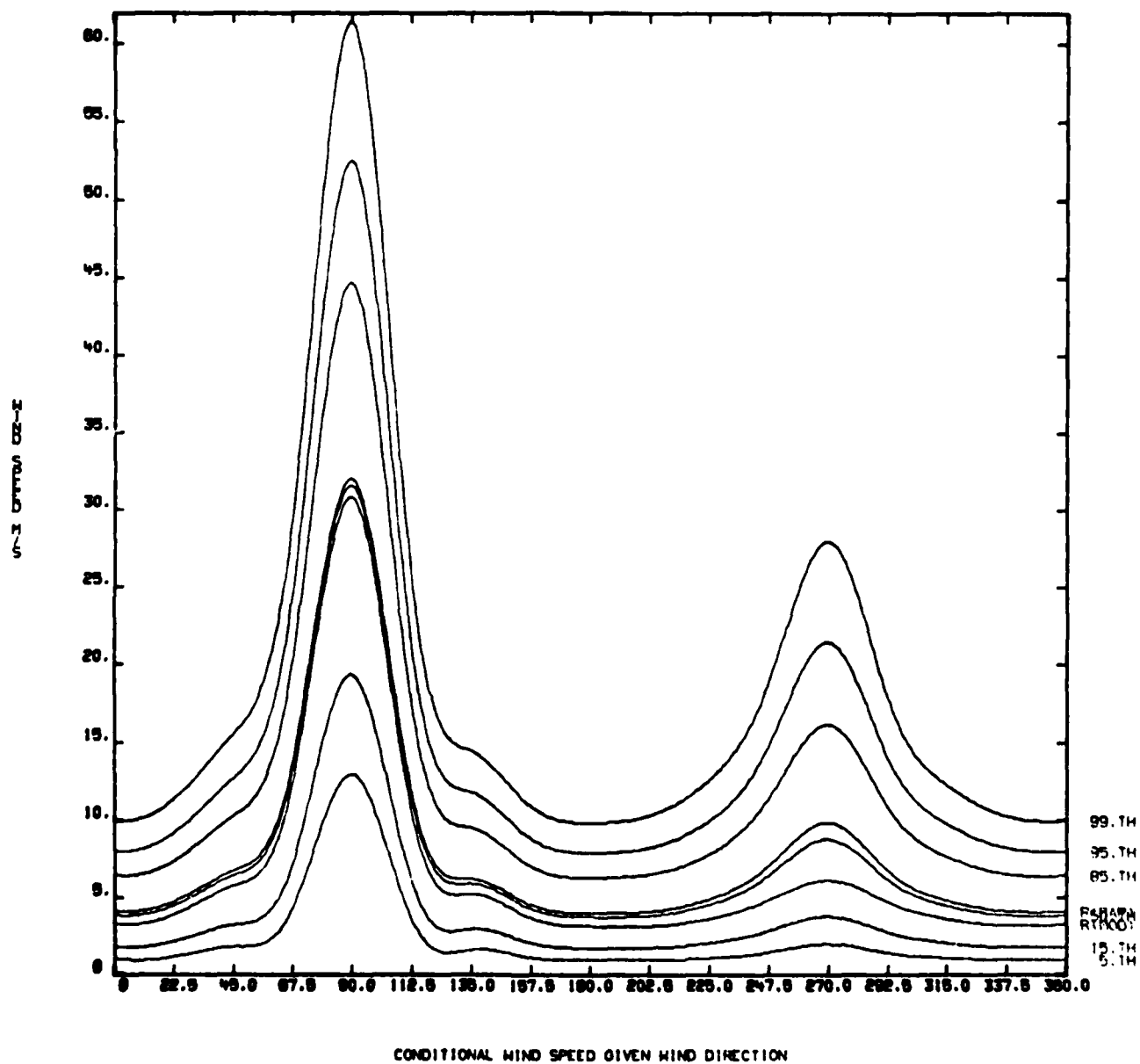


Figure A-52.

STATION=ASCENSION MONTH=JAN ALT=40KM

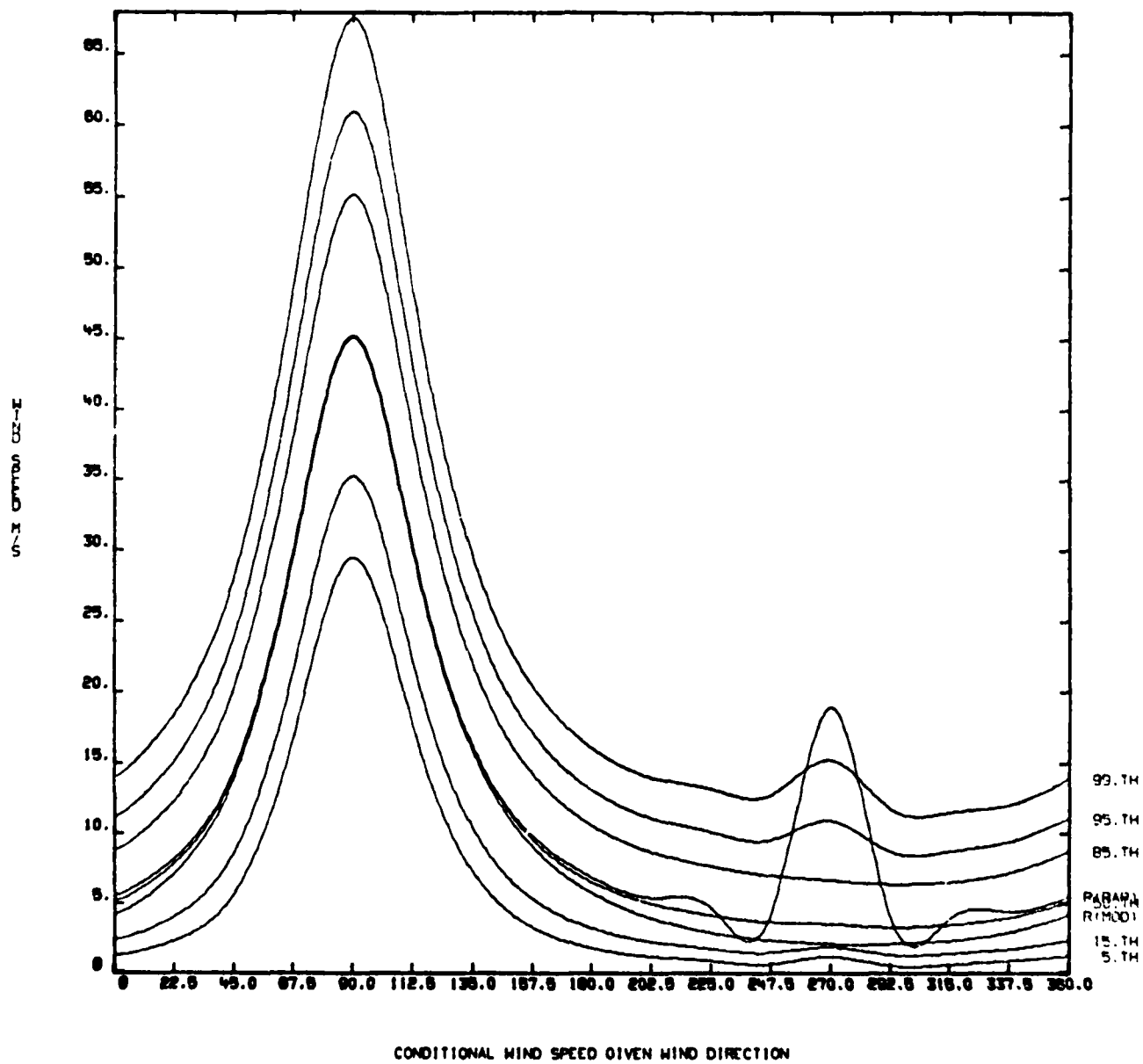


Figure A-53.

STATION=ASCENSION MONTH=JAN ALT=50KM

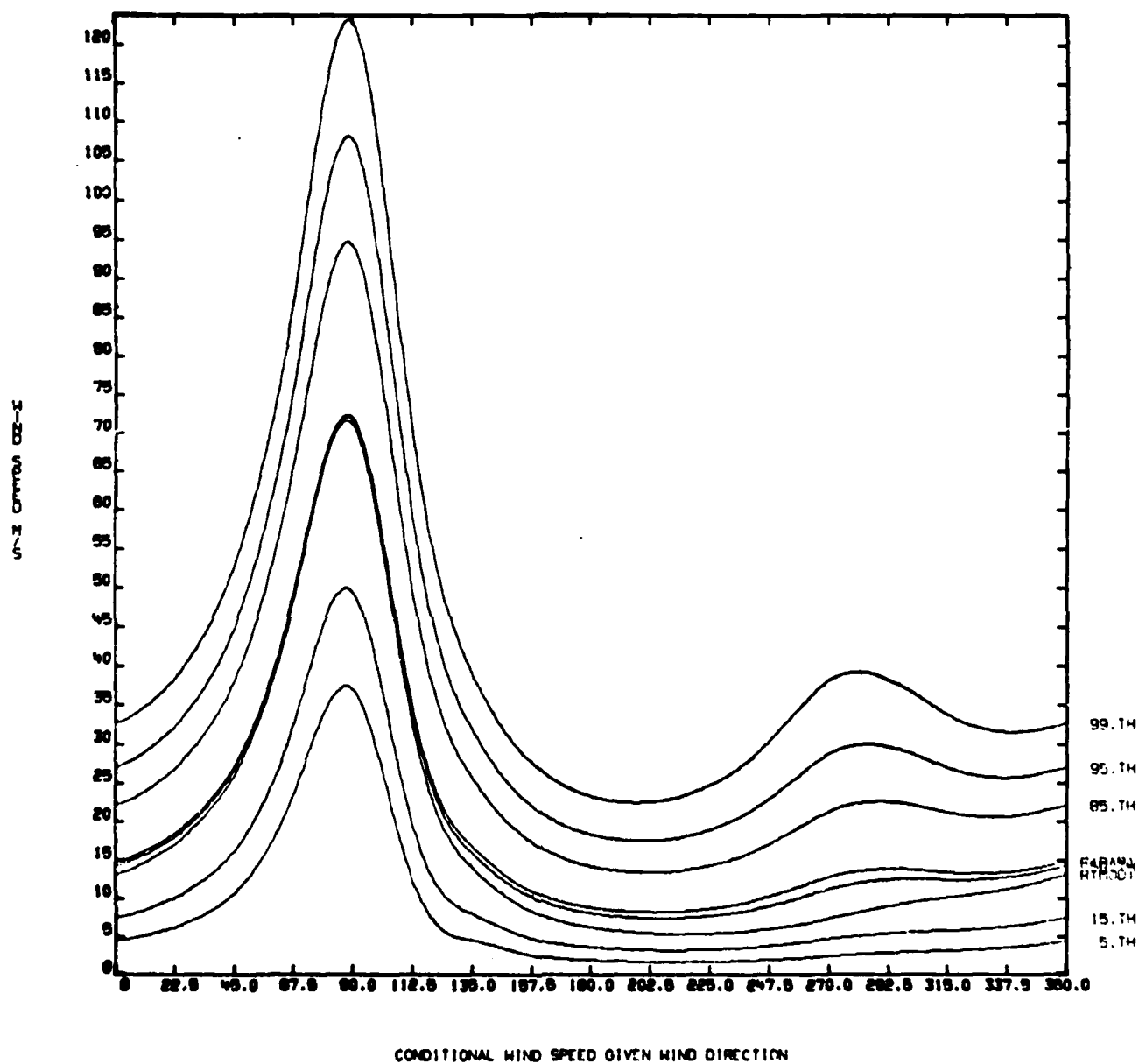


Figure A-54.

STATION=ASCENSION MONTH=JAN ALT=60KM

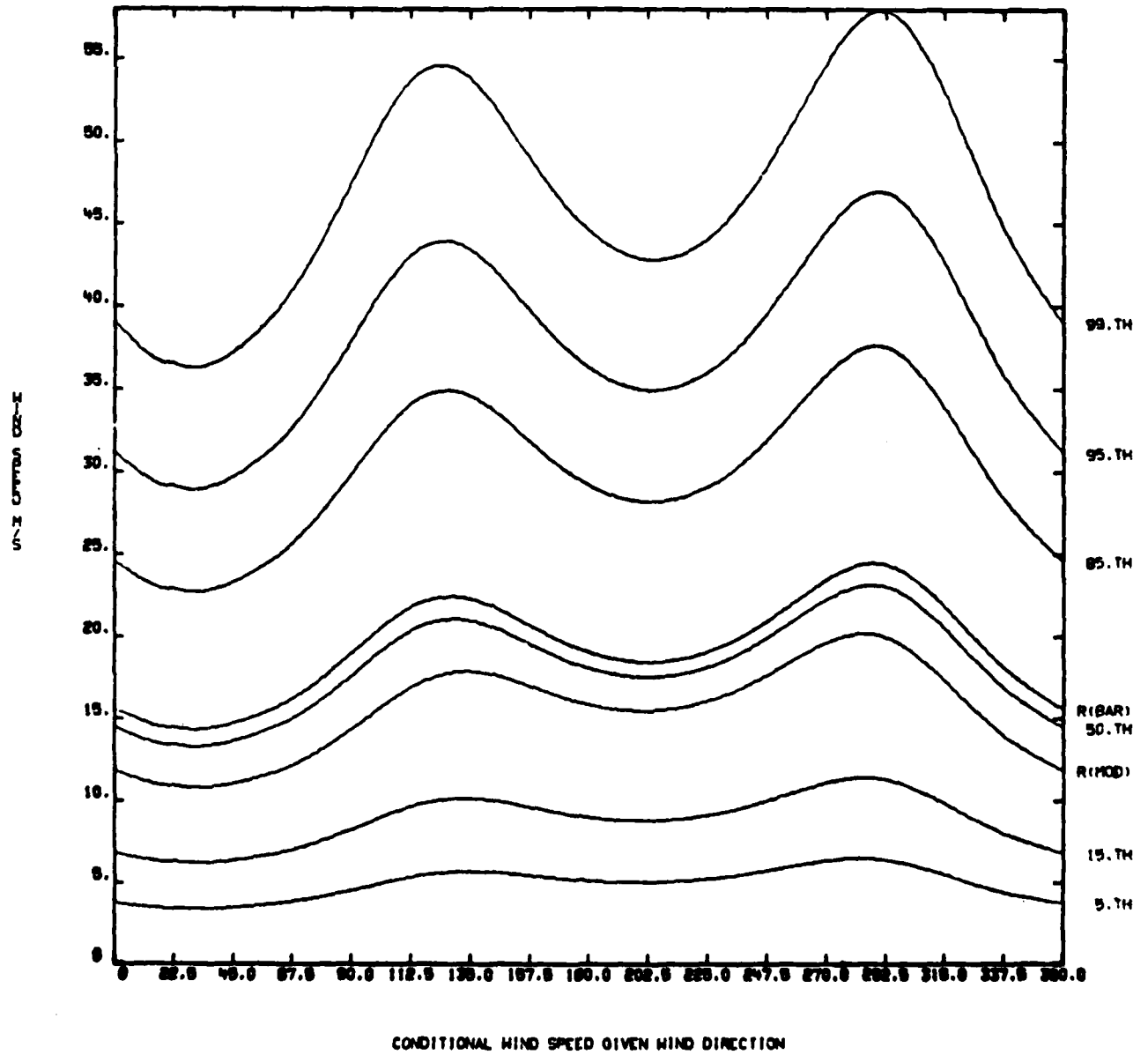


Figure A-55.

STATION=ASCENSION MONTH=JAN ALT=66KM

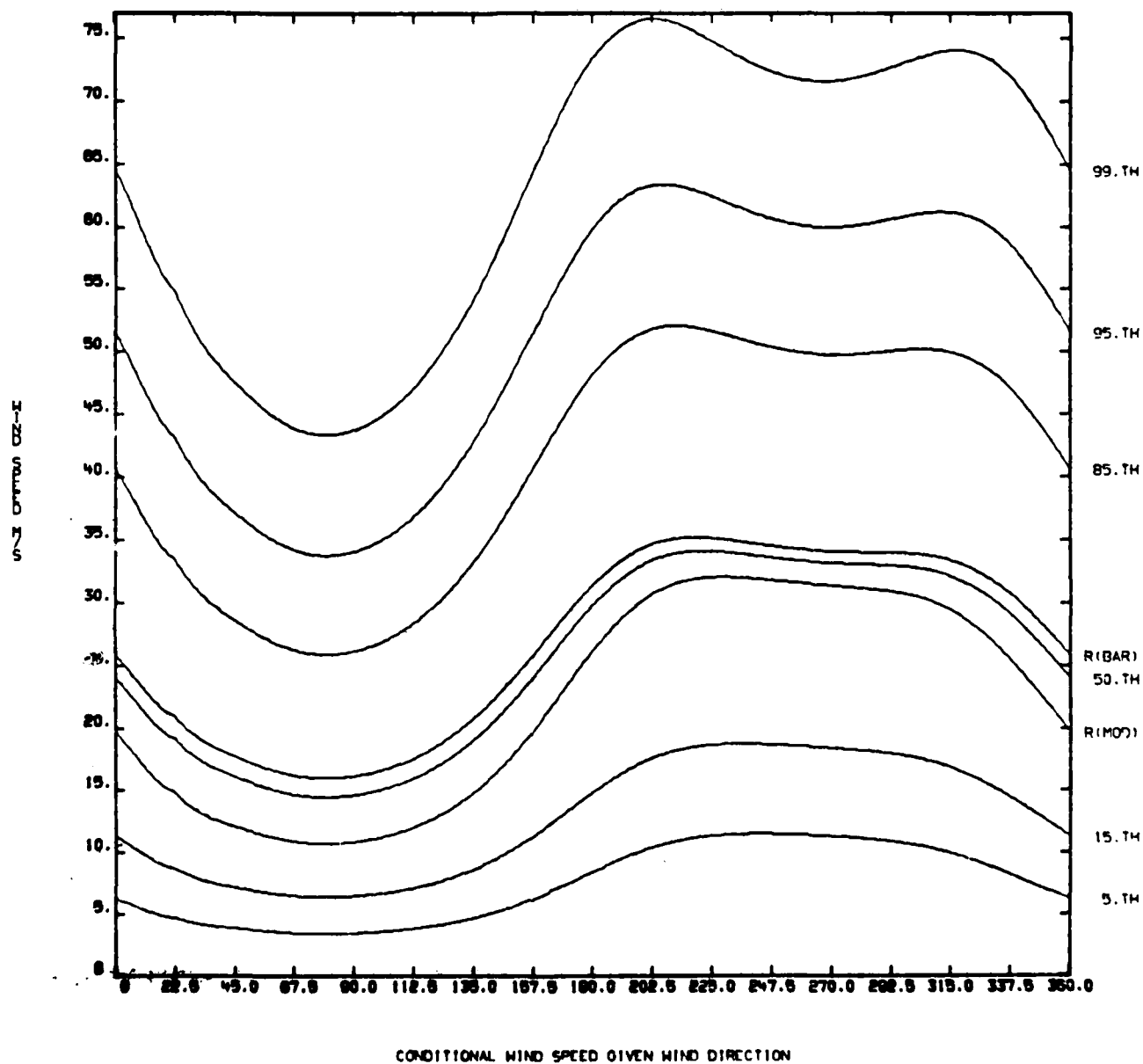


Figure A-56.

STATION=ASCENSION MONTH=JUL ALT= 40M

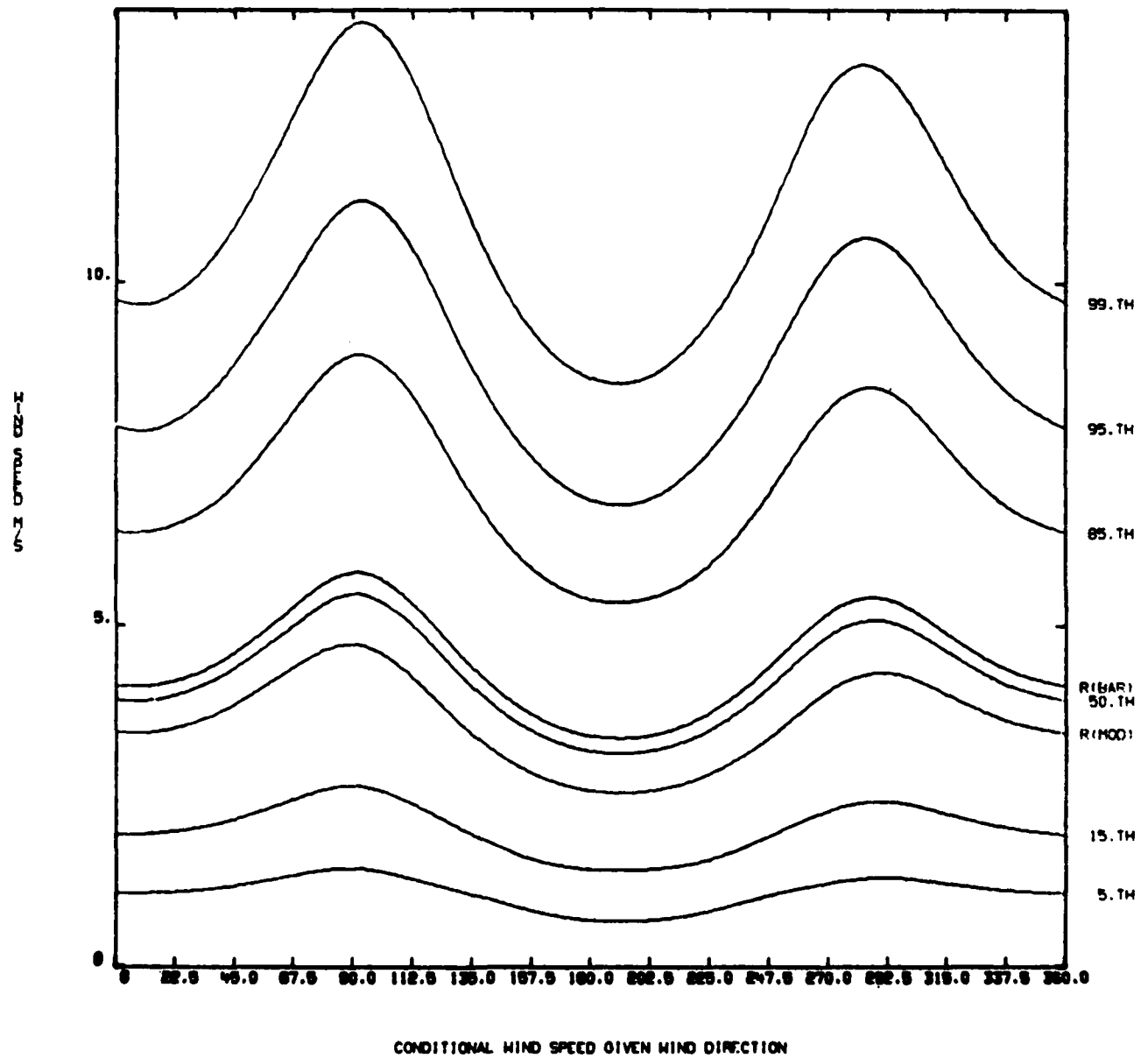


Figure A-57.

STATION=ASCENSION MONTH=JUL ALT=12KM

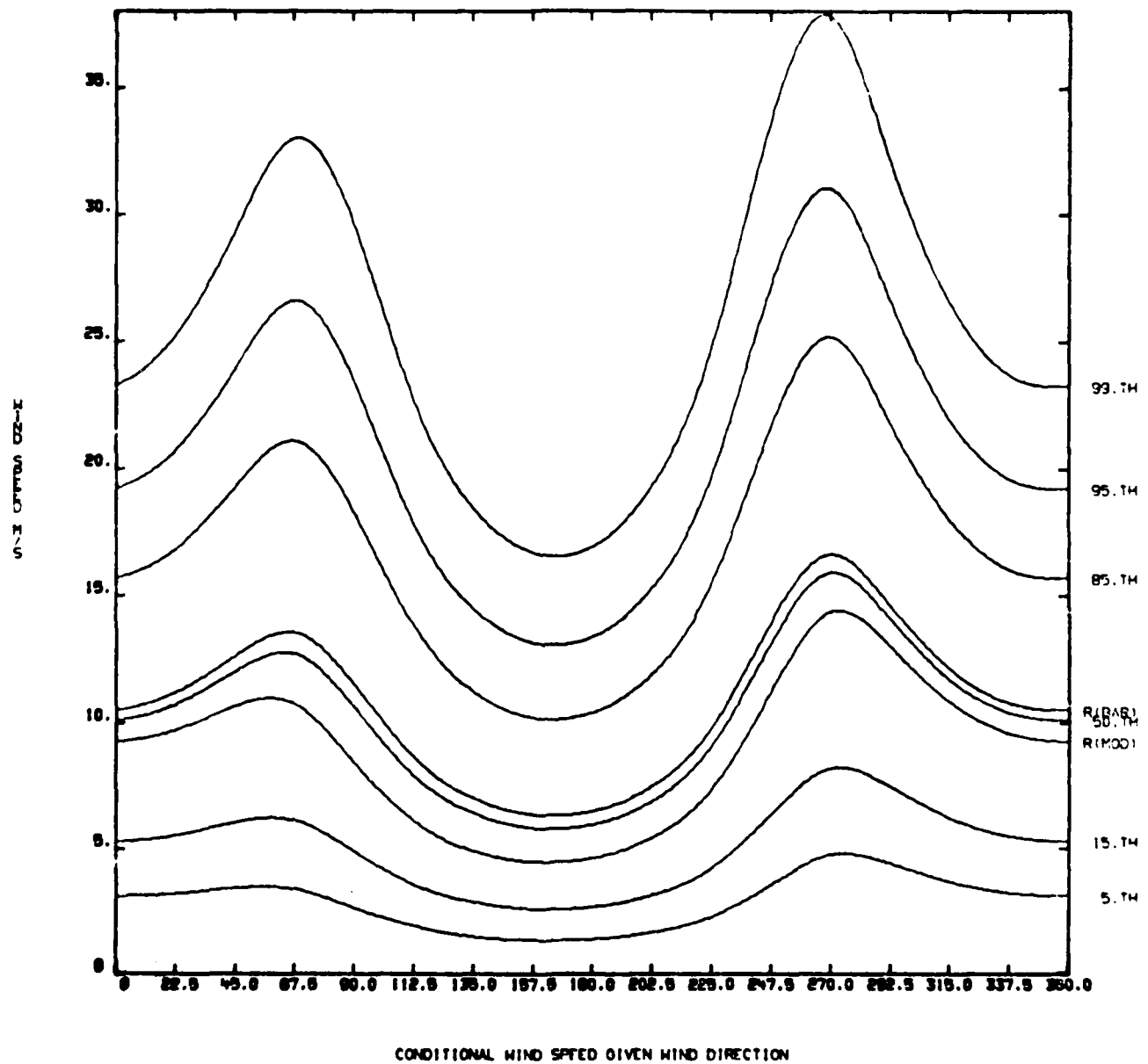


Figure A-58.



STATION=ASCENSION MONTH=JUL AL=20KM

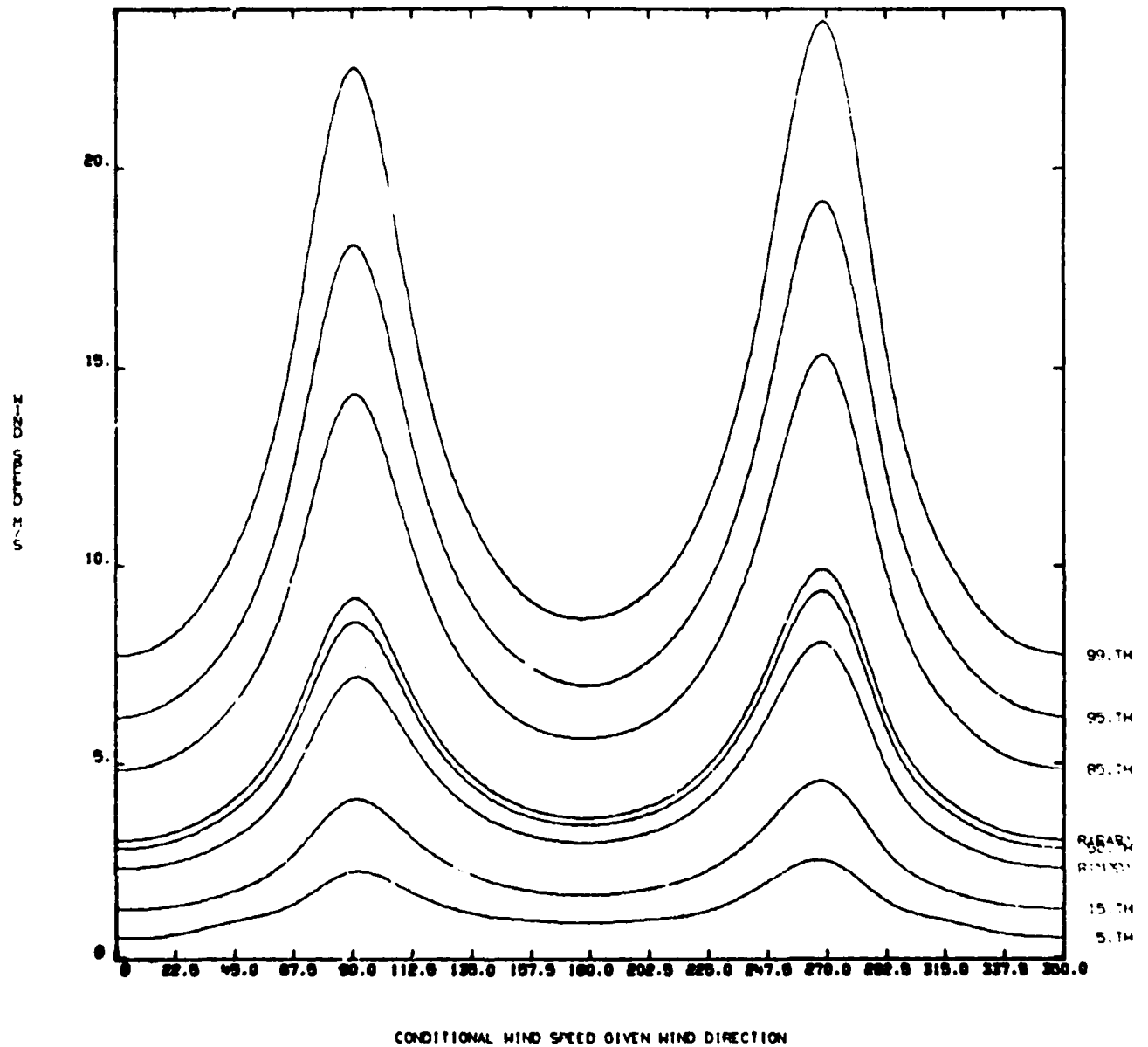


Figure A-59.

STATION=ASCENSION MONTH=JUL ALT=39KM

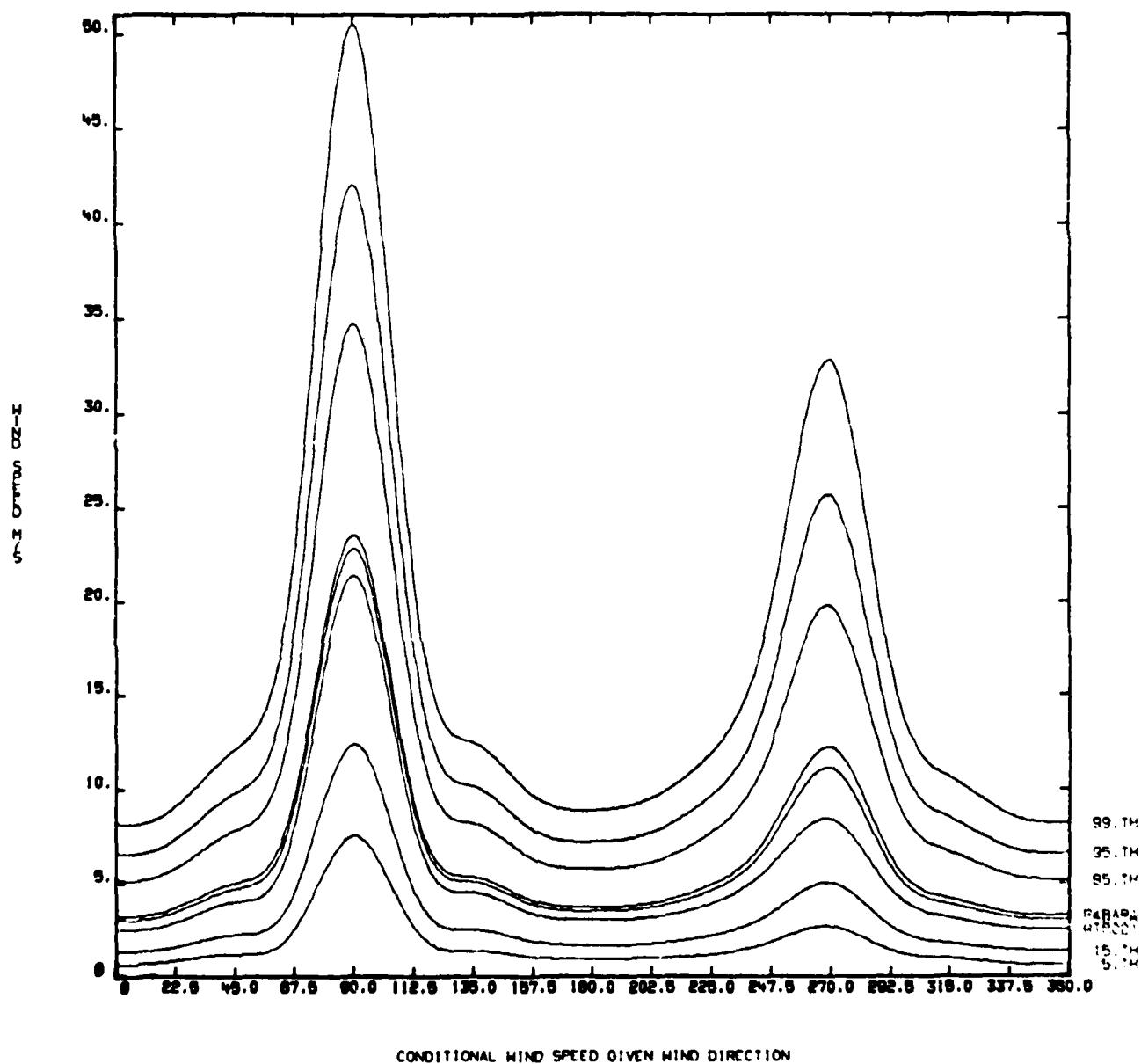


Figure A-60.

STATION=ASCENSION MONTH=JUL ALT=40KM

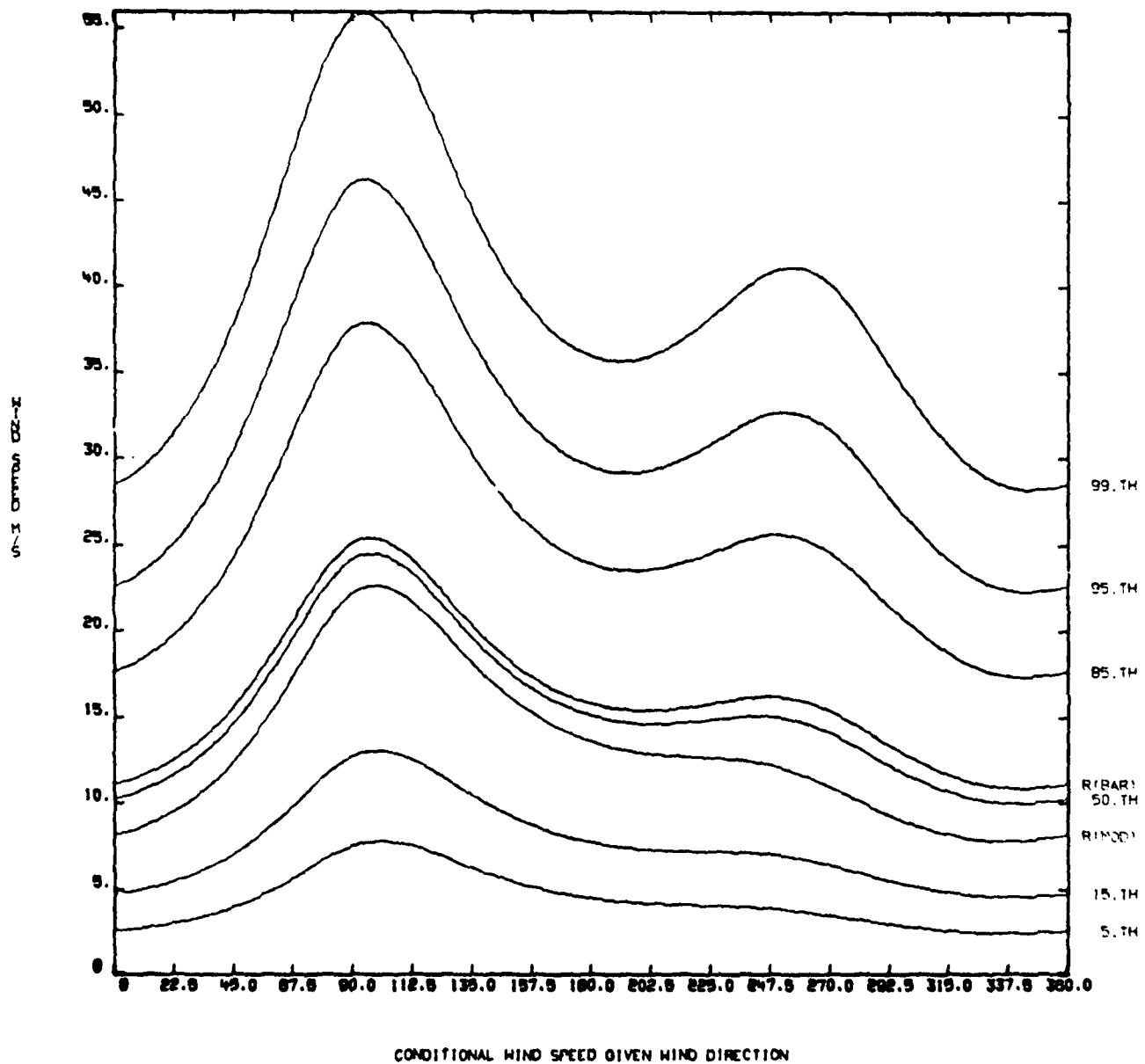


Figure A-61.

STATION=ASCENSION MONTH=JUL ALT=50KM

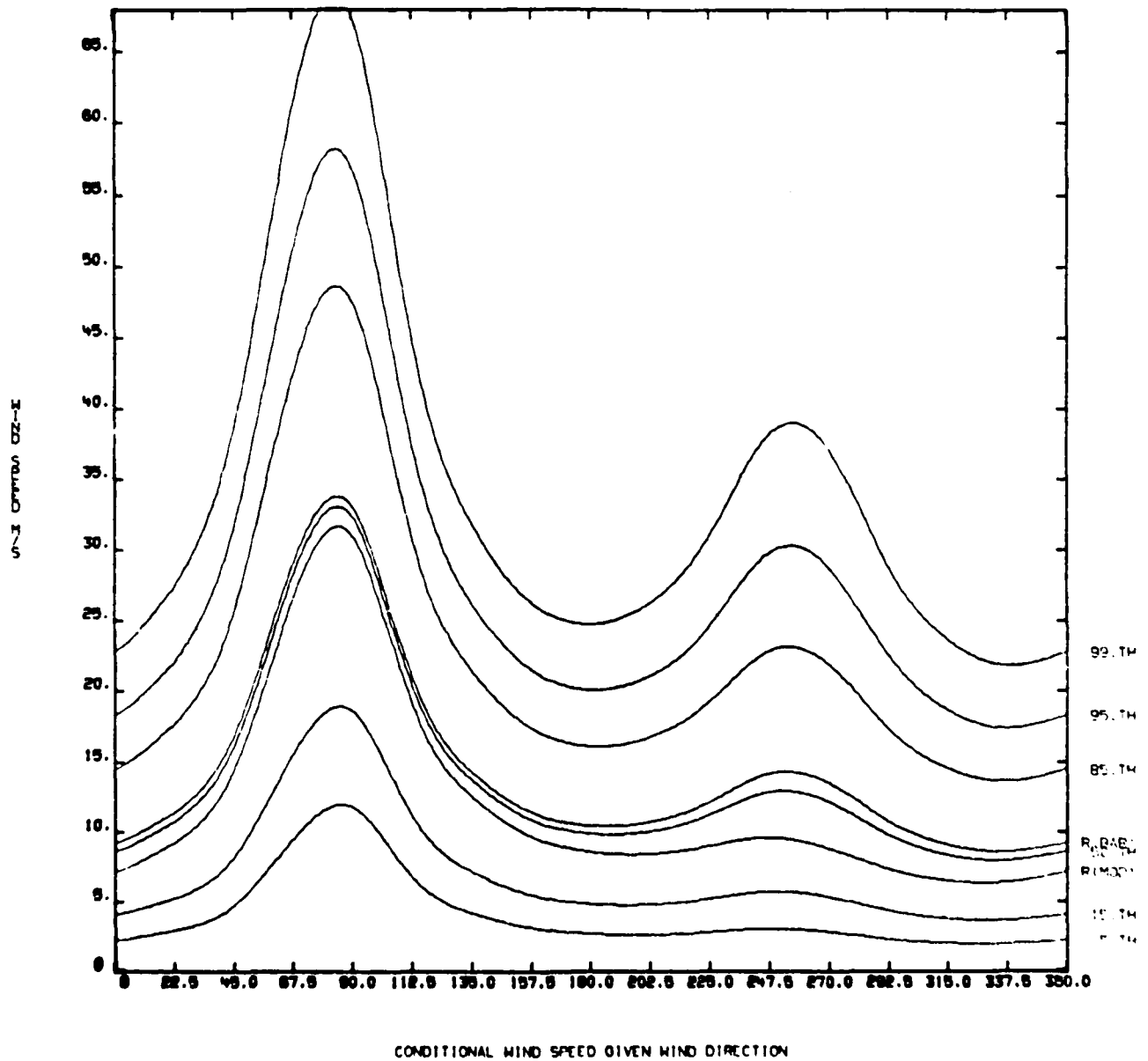


Figure A-62.

STATION=ASCENSION MONTH=JUL ALT=60KM

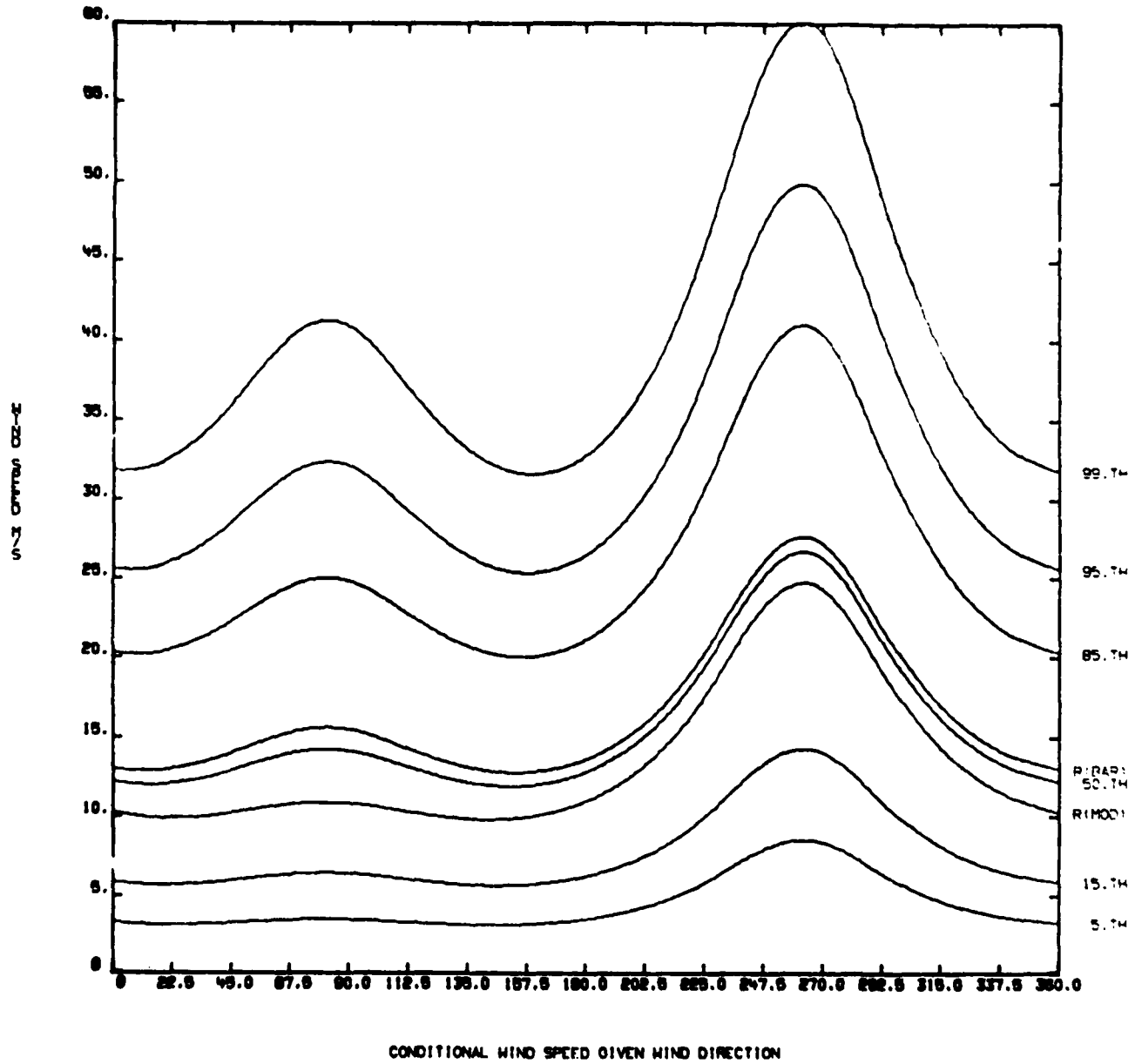
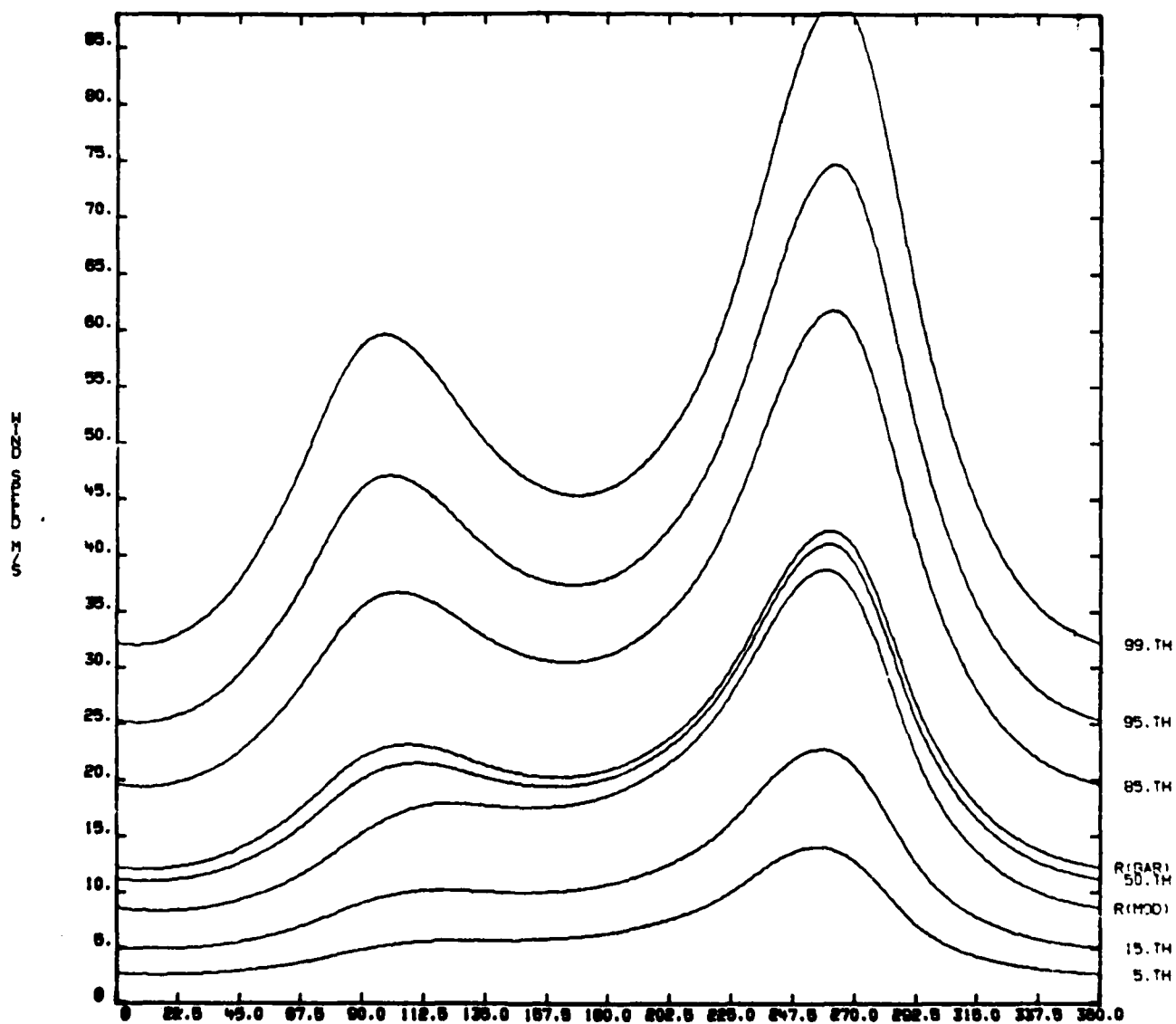


Figure A-63.

STATION=ASCENSION MONTH=JUL ALT=66KM



CONDITIONAL WIND SPEED GIVEN WIND DIRECTION

Figure A-64.

## APPENDIX B

### RANGE SPECIFIC INFORMATION AND THERMODYNAMIC QUANTITIES FOR ASCENSION ISLAND, SOUTH ATLANTIC

#### 1. Range Specific Information

To prevent further character size reduction for tables I through IV, certain range-specific information has been omitted. This important information is given in table B-1.

TABLE B-1

<u>Header Record 0-30 Km</u>	<u>Header Record 32-66 Km</u>
Table Number-----0	Table Number-----0
Data Source	Data Source
(1 = DATSAV, 2 = WDC-A)-----1	(1 = DATSAV, 2 = WDC-A)-----2
Call Letters-----FHAW	Call Letters-----FHAW
WMO Number-----61902	WMO Number-----61902
Latitude-----7°56'	Latitude-----7°56'
Direction (N or S)-----S	Direction (N or S)-----S
Longitude-----14°25'	Longitude-----14°25'
Direction (E or W)-----W	Direction (E or W)-----W
Elevation in Meters-----20	Elevation in Meters-----20
Start Period of Record	Start Period of Record
(Mo-Yr)-----160	(Mo-Yr)-----169
End Period of Record	End Period of Record
(Mo-Yr)-----1279	(Mo-Yr)-----1278
No. of Time Windows	No. of Time Windows
(0, 1 or 2)-----1	(0, 1 or 2)-----1
Start Time Window #1	Start Time Window #1
(Hr-MNZ)-----900	(Hr-MNZ)-----900
End Time Window #1-----1500	End Time Window #1-----1500
Start Time Window #2-----0	Start Time Window #2-----0
End Time Window #2-----0	End Time Window #2-----0
Date of RRA-----1180	Date of RRA-----1180
Altitude Range of RRA	Altitude Range of RRA
Low Level (Km)-----0	Low Level (Km)-----30
Altitude Range of RRA	Altitude Range of RRA
High Level (Km)-----30	High Level (Km)-----66
Standard Deviation of	Standard Deviation of
Thermodynamic Limits-----6.0	Thermodynamic Limits-----6.0
Wind Limits-----6.0	Wind Limits-----6.0

#### 2. Thermodynamic Quantities

This section presents examples of further computations and graphical displays of pressure, density, and virtual temperature statistics that can be derived from the data given in tables II, III, and IV. No attempt is made to

present complete nor exhaustive illustrations that can be made to aid in visualizing the relations that can be made from the data in tables II and IV. The choices are those that aided the committee to verify the reasonableness of the tabulations.

## 2.1 Monthly Mean from the Annual Mean

The hydrostatic model values in table IV are used to compute (1) the monthly mean differences relative to the annual mean values of pressure, density, and virtual temperature expressed in percent and (2) the monthly mean difference in virtual temperature for the annual mean virtual temperature expressed in degrees Kelvin. Examples of these four statistics are given in table B-2 for January and table B-3 for July. Graphical displays of the four statistics contained in tables B-2 and B-3 are shown in figures B-1 through B-8. Also, the relative differences between the monthly mean values from table IV-1 through IV-12 for all months from the annual mean values (table IV-13) are illustrated in figure B-9 for pressure, in figure B-10 for density, and in figure B-11 for virtual temperature. The monthly mean virtual temperature differences from the annual mean virtual temperature for all months are given in figure B-12. The simple sum of the monthly mean differences from the annual mean values of these quantities is not zero. This is because the annual mean statistical parameters are computed (see section III. C.3) by weighting the monthly means by the number of observations in each month.

## 2.2 Coefficients of Variation and Derived Correlation Coefficients

The coefficient of variation,  $C_V$ , is defined by the standard deviation with respect to the mean divided by the mean. The coefficients of variation for pressure,  $C_{VP}$ , and density,  $C_{VD}$ , were computed using the standard deviations from table II and the hydrostatic mean values from table IV. The coefficient of variation for temperature uses the standard deviations of virtual temperature from table III to the altitude where virtual temperature exists. Above this altitude, the standard deviations of temperature are from table II. The mean values for temperature (virtual temperature to the altitude where it exists) are taken from table IV. No distinction is made in the table headings in table B-4 (January) and table B-5 (July) and all related figures between virtual temperature and temperature.

From the coefficients of variation for pressure, density, and temperature (virtual temperature to the altitude where it exists), the correlation coefficients between these quantities are derived using Buell's method (see reference in text). The equations for these derived correlation coefficients are

$$r(P,T) = \frac{(C_{VT})^2 + (C_{VP})^2 - (C_{VD})^2}{2 [C_{VT} \cdot C_{VP}]} \quad (B-1)$$

$$r(P,D) = \frac{(C_{VD})^2 - (C_{VT})^2 + (C_{VP})^2}{2 [C_{VP} \cdot C_{VD}]} \quad (B-2)$$



$$r(T,D) = \frac{(C_{VP})^2 - (C_{VD})^2 - (C_{VT})^2}{2 [C_{VT} \cdot C_{VD}]} \quad (B-3)$$

The correlation coefficients in tables B-4 and B-5 are derived from the above equations.

A test for the validity of the derived correlation coefficient is that all three of the following inequalities be satisfied.

$$\left. \begin{aligned} C_{VP} - [C_{VD} + C_{VT}] &< 0 \\ C_{VD} - [C_{VT} + C_{VP}] &< 0 \\ C_{VT} - [C_{VP} + C_{VD}] &< 0 \end{aligned} \right\} \quad (B-4)$$

In these examples (tables B-4 and B-5) the numerical values from equation (B-4) are all negative; hence, the derived correlation test is considered valid. The rare exceptions to this test for several RRAs occur at the extreme highest altitudes, where sample sizes for the statistical sample are small.

The statistical parameters from table B-4 (January) and table B-5 (July) are illustrated in figures B-13 through B-16.

For all months the  $C_{VP}$  values are shown in figure B-17, the  $C_{VD}$  values are shown in figure B-18, and  $C_{VT}$  values are shown in figure B-19. If the abscissa on the figures for the coefficient of variation were multiplied by 100, these figures would show the percentage of random dispersion of these qualities over the month with respect to the monthly mean for these thermodynamic quantities.

The derived correlation coefficients for all months are illustrated in the following figures:

- a) Figure B-20 gives  $r(P,D)$ .
- b) Figure B-21 gives  $r(P,T)$ .
- c) Figure B-22 gives  $r(T,D)$ .

Table B-2.

STATION 619020 MONTH 1  
 DELTAS IN PERCENT RELATIVE TO ANNUAL

LEVEL	PRESSURE	DENSITY	TEMP.	THO-TANN( DEG. K)
.000	-.15	-.26	.07	.20
.020	-.14	-.17	.09	.23
1.000	-.13	-.37	.20	.59
2.000	-.10	-.42	.32	.62
3.000	-.07	-.20	.13	.37
4.000	-.07	-.01	-.06	-.18
5.000	-.08	.03	-.11	-.31
6.000	-.09	-.02	-.07	-.20
7.000	-.11	.05	-.18	-.43
8.000	-.14	.12	-.24	-.61
9.000	-.17	.11	-.28	-.70
10.000	-.21	.05	-.25	-.53
11.000	-.24	-.05	-.20	-.45
12.000	-.26	-.15	-.10	-.23
13.000	-.27	-.30	.03	.07
14.000	-.26	-.38	.15	.31
15.000	-.24	-.31	.07	.14
16.000	-.24	-.10	-.15	-.30
17.000	-.31	.30	-.61	-1.20
18.000	-.47	.60	-1.30	-2.58
19.000	-.69	.61	-1.32	-2.68
20.000	-.69	.21	-1.10	-2.29
21.000	-1.06	-.08	-.98	-2.07
22.000	-1.21	-.27	-.94	-2.01
23.000	-1.37	-.34	-1.04	-2.26
24.000	-1.54	-.36	-1.18	-2.56
25.000	-1.72	-.49	-1.23	-2.72
26.000	-1.90	-.61	-1.11	-2.49
27.000	-2.05	-1.12	-.94	-2.12
28.000	-2.18	-1.43	-.77	-1.76
29.000	-2.28	-1.72	-.56	-1.29
30.000	-2.36	-1.85	-.51	-1.19
32.000	-2.58	-1.25	-1.04	-2.46
34.000	-2.93	-1.17	-1.48	-3.55
36.000	-3.37	-1.36	-1.74	-4.27
38.000	-3.86	-1.68	-1.91	-4.79
40.000	-4.33	-2.29	-1.78	-4.59
42.000	-4.67	-3.47	-.92	-2.43
44.000	-4.87	-3.84	-.76	-2.04
46.000	-5.09	-3.64	-1.03	-2.78
48.000	-5.30	-4.24	-.78	-2.10
50.000	-5.39	-5.15	.07	.18
52.000	-5.27	-5.89	.97	2.60
54.000	-4.86	-6.16	1.59	4.22
55.000	-4.50	-6.35	2.28	6.00
58.000	-3.94	-5.89	2.37	6.12
60.000	-3.36	-5.25	2.32	5.23
62.000	-2.72	-5.04	2.76	6.63
64.000	-1.95	-4.70	3.22	7.81
66.000	-1.24	-2.89	2.03	4.78

Table B-3.

STATION 619020 MONTH 7  
 DELTAS IN PERCENT RELATIVE TO ANNUAL

LEVEL	PRESSURE	DENSITY	TEMP.	TMO-TANP DEG. K1
.000	.24	.52	-.28	-.66
.020	.24	.52	-.27	-.81
1.000	.20	.56	-.34	-1.00
2.000	.14	.92	-.78	-2.26
3.000	.07	.34	-.26	-.75
4.000	.05	.14	-.10	-.27
5.000	.04	.11	-.07	-.20
6.000	.03	.13	-.09	-.25
7.000	.01	.17	-.16	-.42
8.000	-.01	.25	-.26	-.65
9.000	-.05	.28	-.35	-.85
10.000	-.11	.29	-.40	-.95
11.000	-.17	.24	-.43	-.98
12.000	-.23	.18	-.39	-.86
13.000	-.28	.00	-.29	-.62
14.000	-.31	-.23	-.05	-.11
15.000	-.29	-.57	.30	.60
16.000	-.21	-.92	.70	1.38
17.000	-.03	-1.45	1.39	2.73
18.000	.25	-1.59	1.90	3.73
19.000	.54	-1.05	1.65	3.25
20.000	.79	-.61	1.42	2.96
21.000	1.00	-.16	1.17	2.47
22.000	1.16	.31	.84	1.00
23.000	1.28	.58	.68	1.48
24.000	1.37	.90	.47	1.04
25.000	1.44	1.01	.43	.96
26.000	1.50	1.16	.33	.74
27.000	1.54	1.33	.19	.43
28.000	1.55	1.71	-.15	-.34
29.000	1.49	2.00	-.50	-1.14
30.000	1.41	2.01	-.58	-1.35
32.000	1.25	1.62	-.50	-1.17
34.000	1.11	1.50	-.43	-1.15
36.000	.92	1.66	-.84	-2.06
38.000	.67	1.55	-.98	-2.46
40.000	.37	1.54	-1.26	-3.24
42.000	-.01	1.56	-1.65	-4.35
44.000	-.42	1.04	-1.57	-4.20
46.000	-.74	.05	-.93	-2.52
48.000	-.95	-.28	-.75	-2.02
50.000	-1.10	-.80	-.46	-1.24
52.000	-1.14	-1.32	.07	.60
54.000	-1.14	-1.24	-.00	-.01
56.000	-1.15	-1.14	-.12	-.32
58.000	-1.21	-.96	-.37	-.95
60.000	-1.33	-.90	-.55	-1.40
62.000	-1.64	.04	-1.78	-4.41
64.000	-2.29	.59	-2.96	-7.17
66.000	-2.99	-1.07	-2.03	-4.77

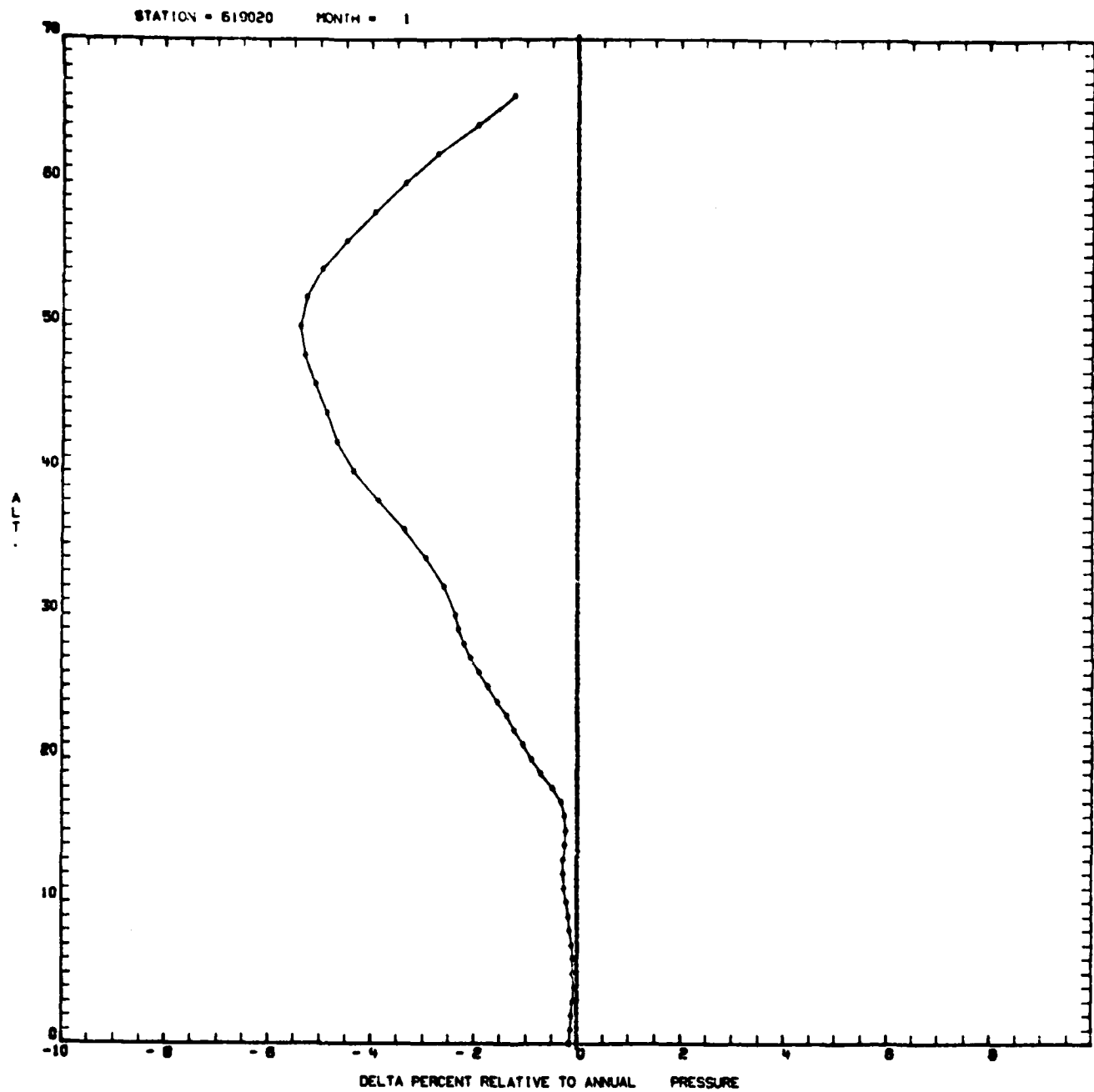


Figure B-1.

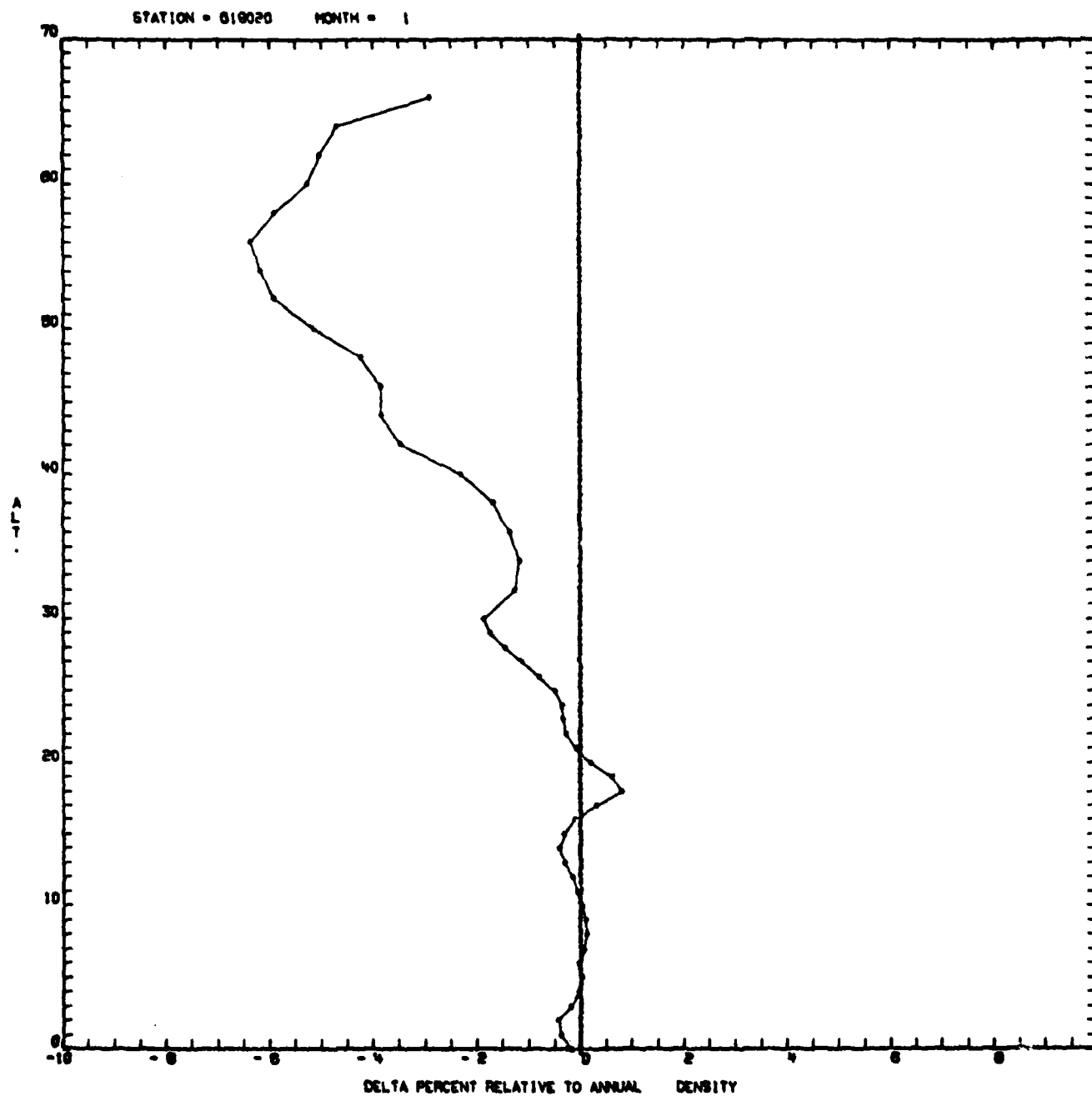


Figure B-2.

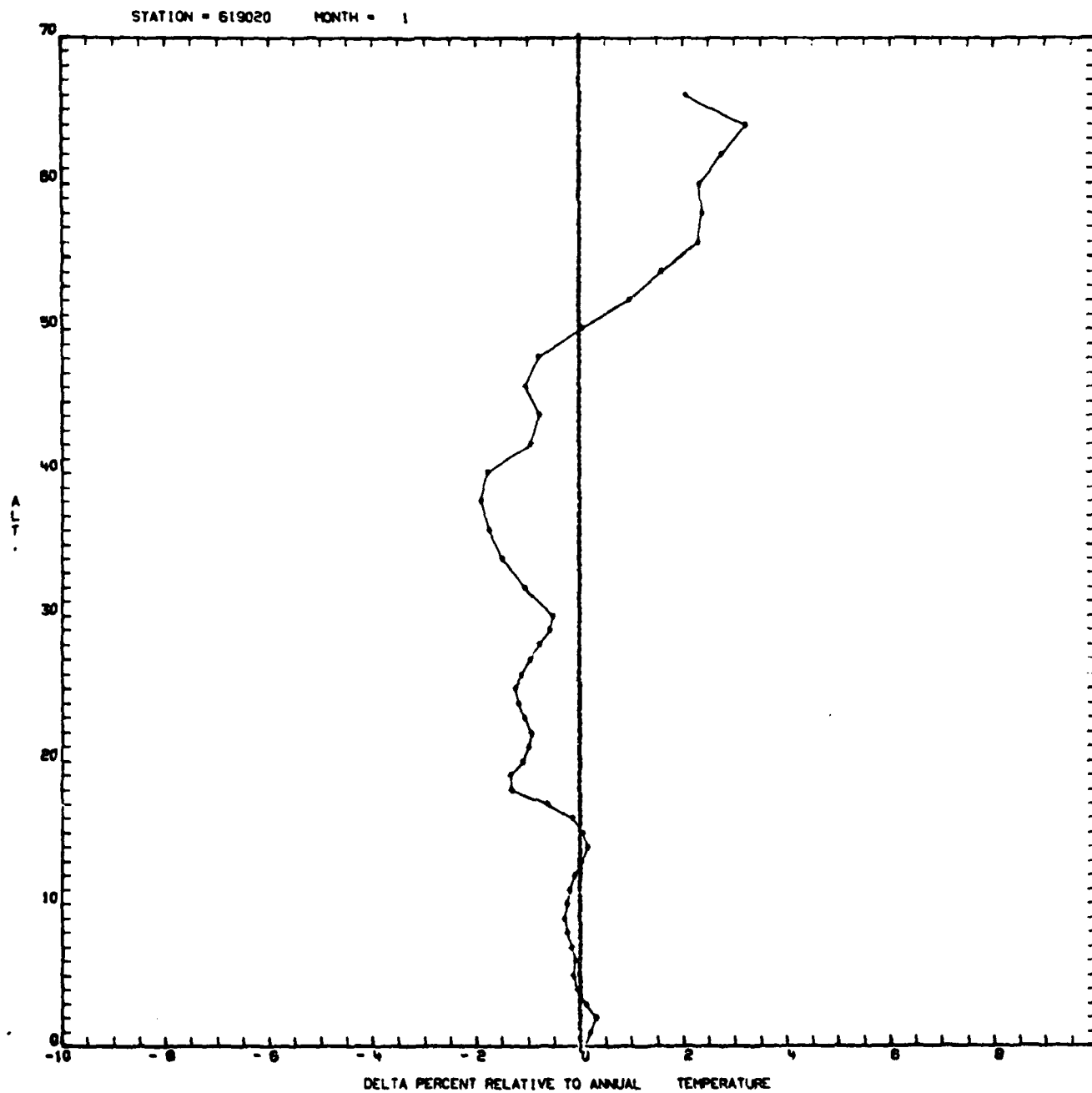


Figure B-3.

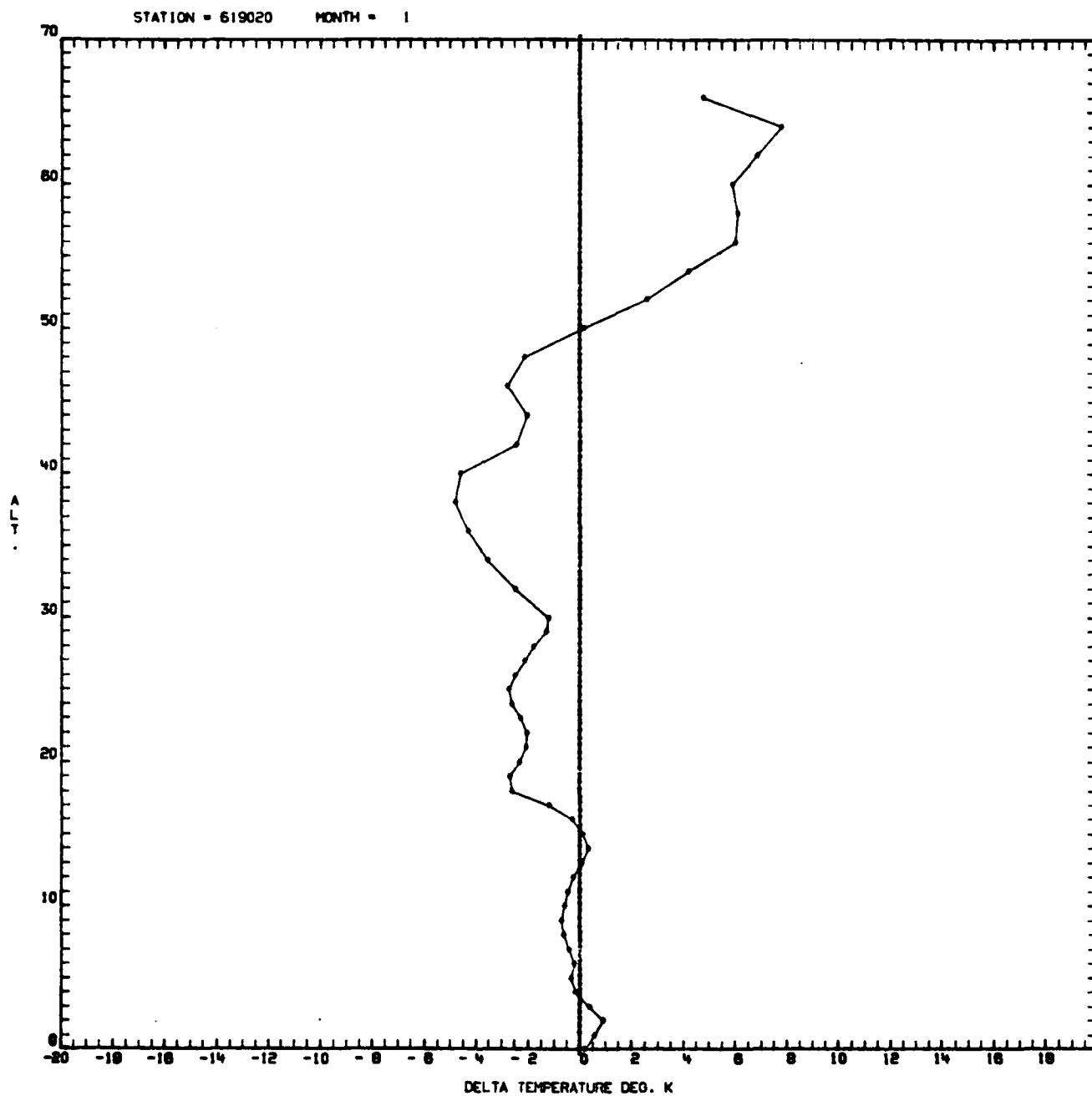


Figure B-4.

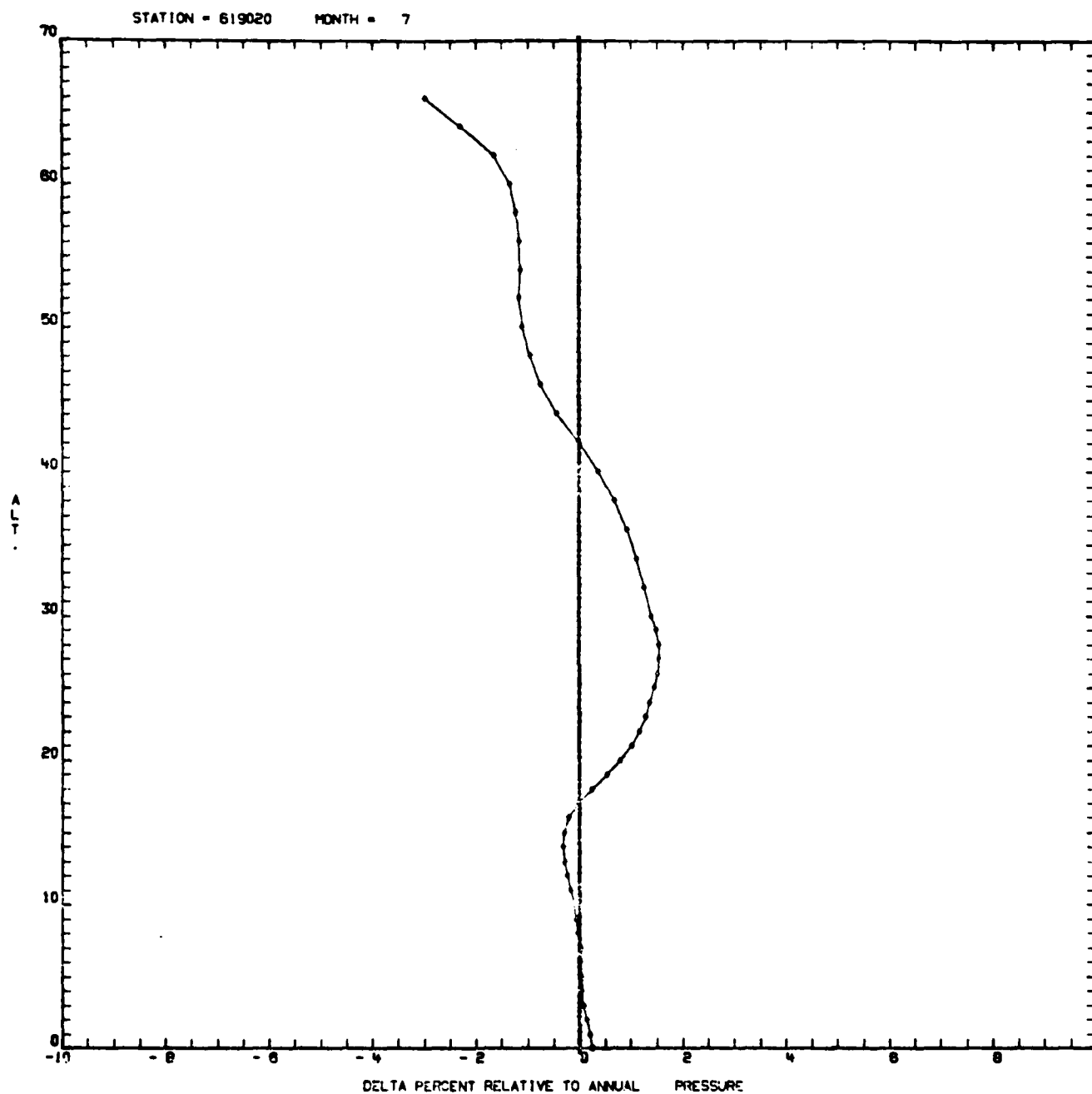


Figure B-5.



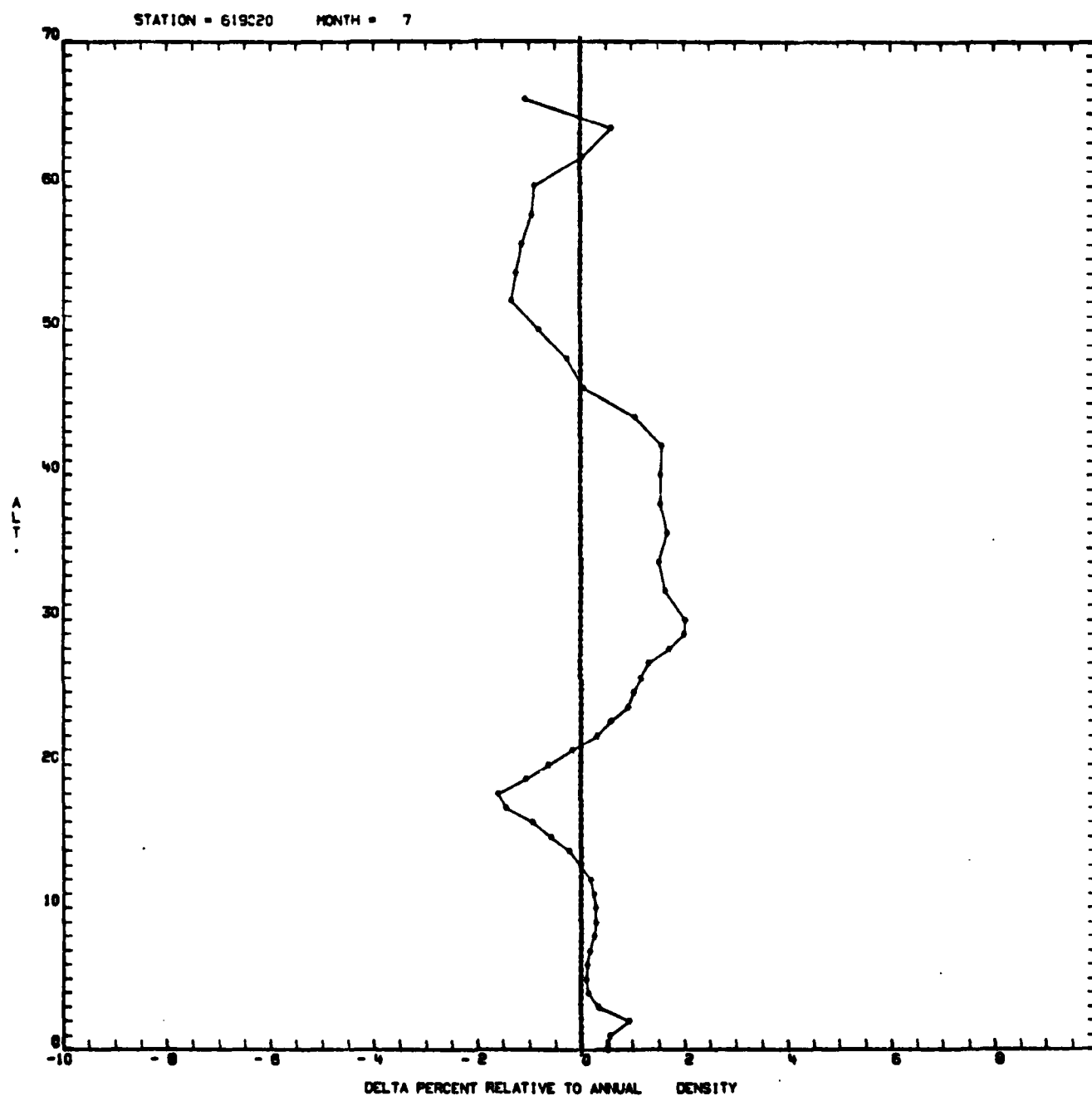


Figure B-6.

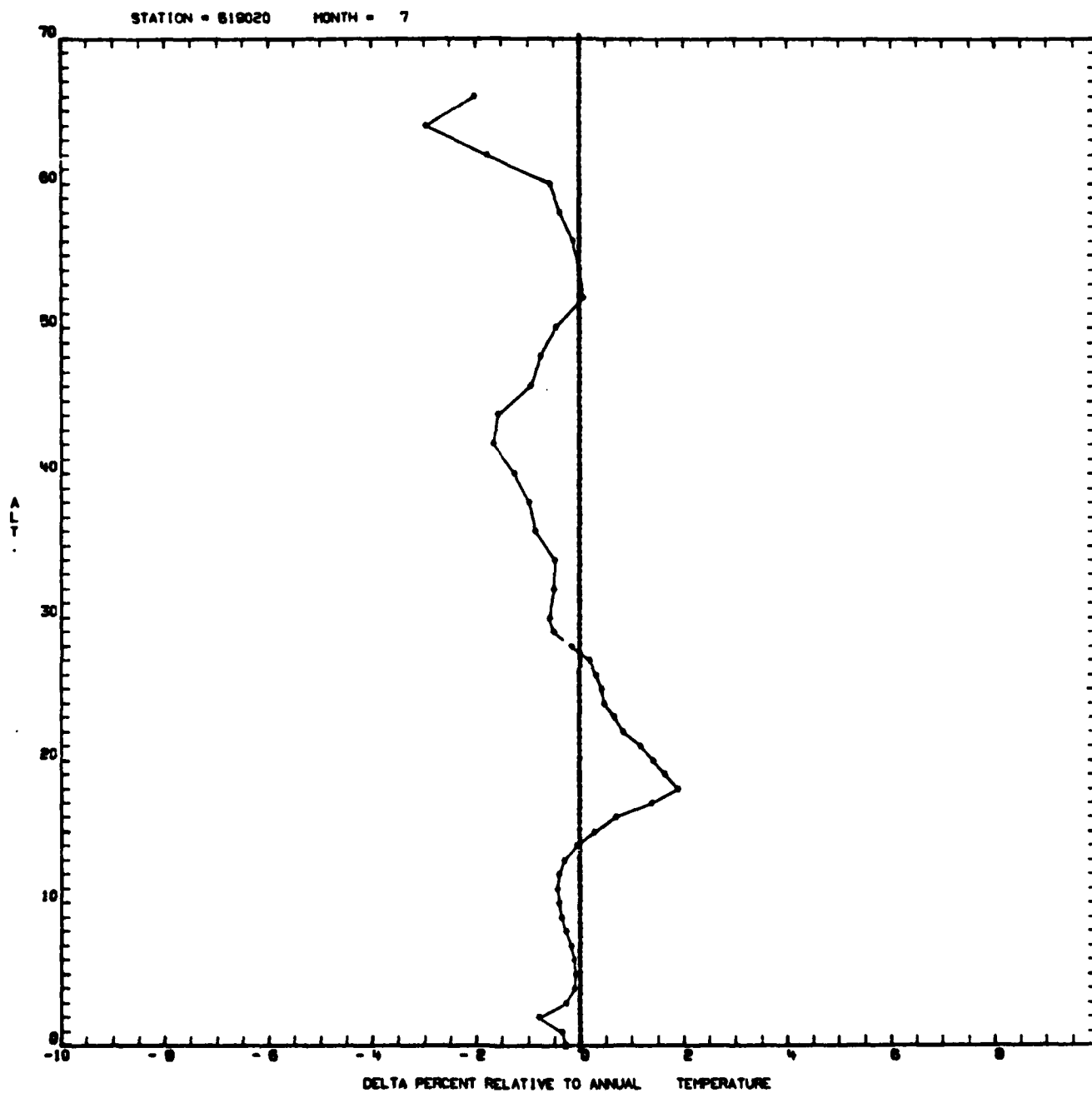


Figure B-7.

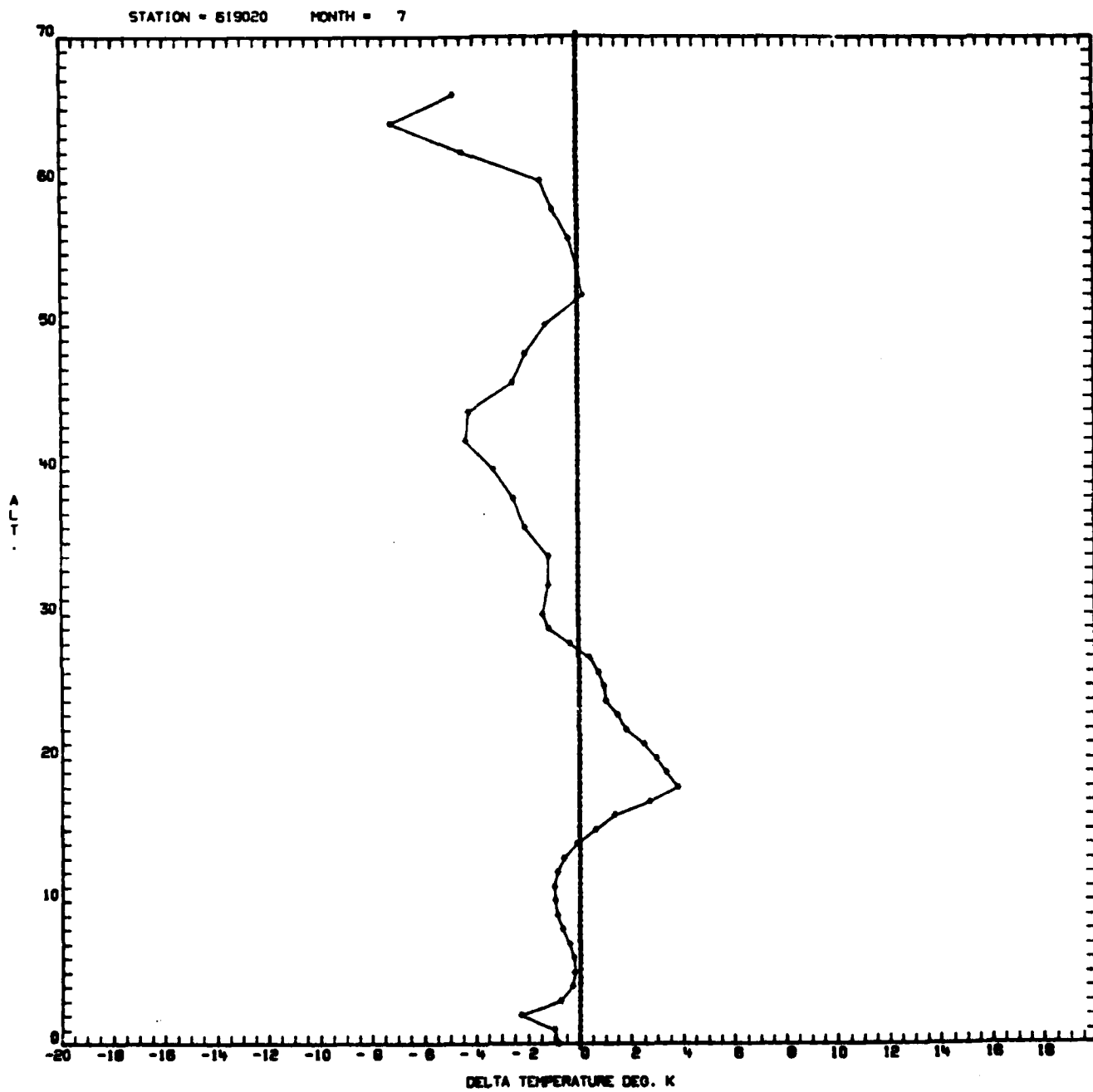


Figure B-8.

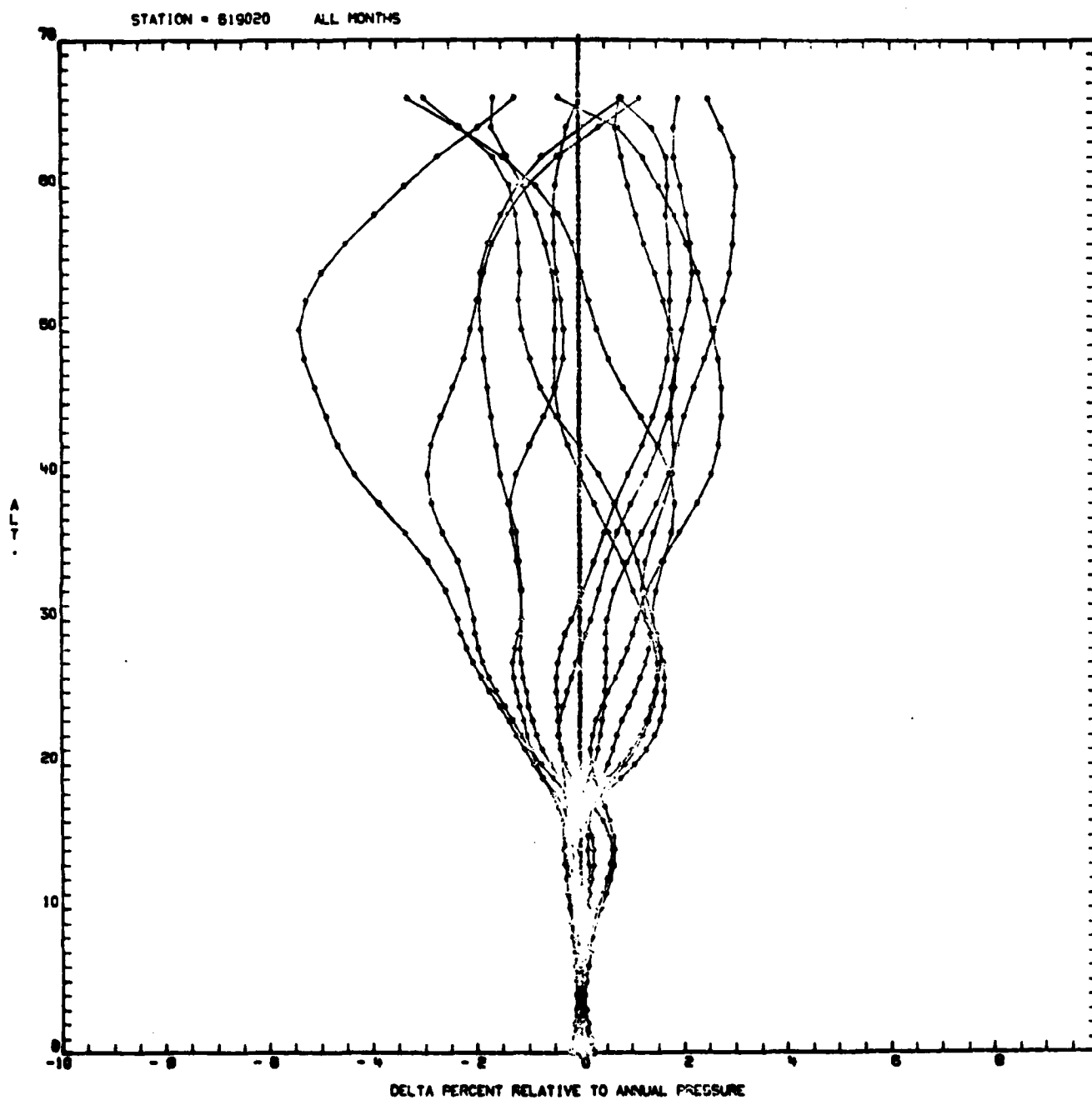


Figure B-9.

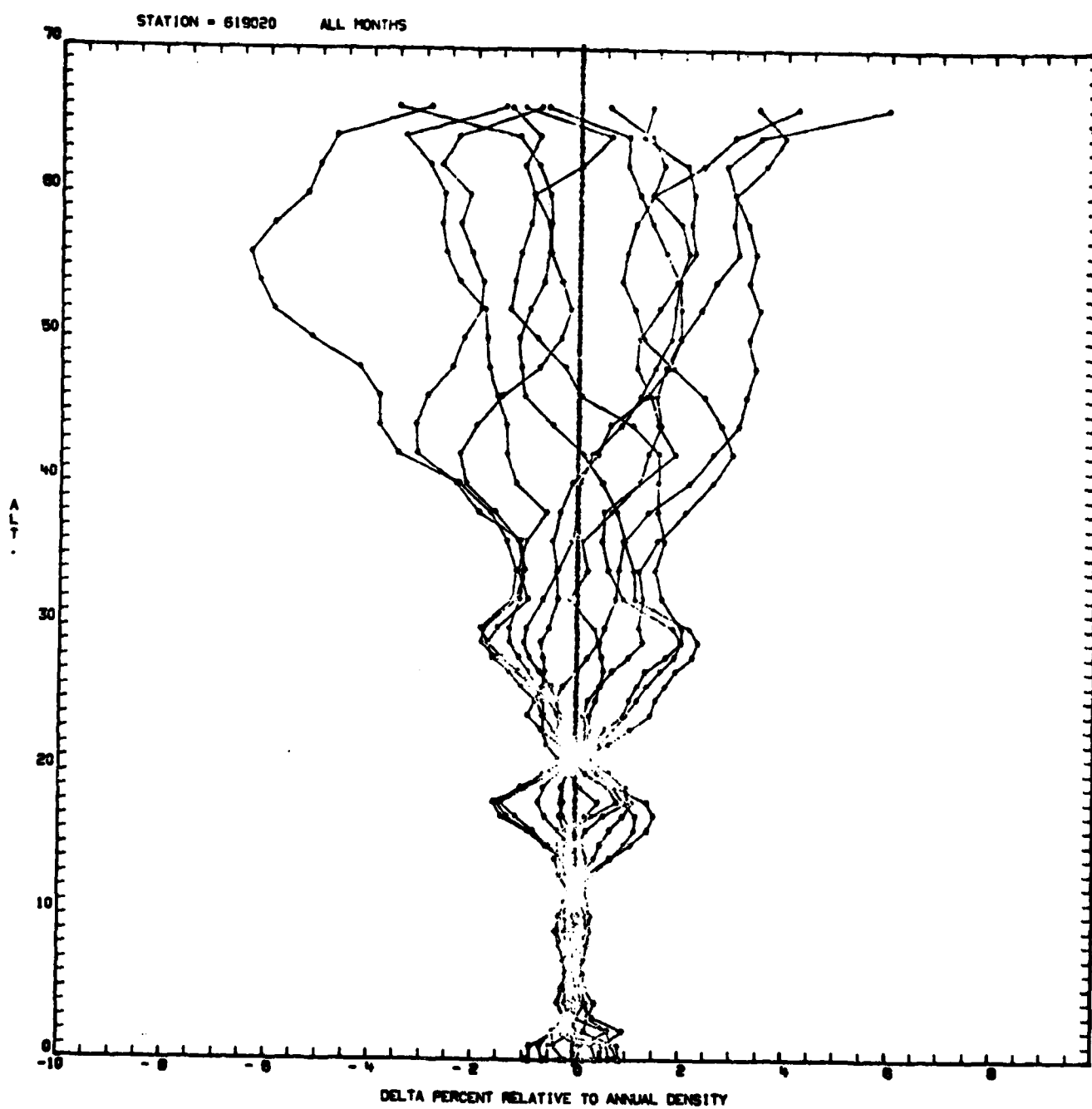


Figure 8-10.

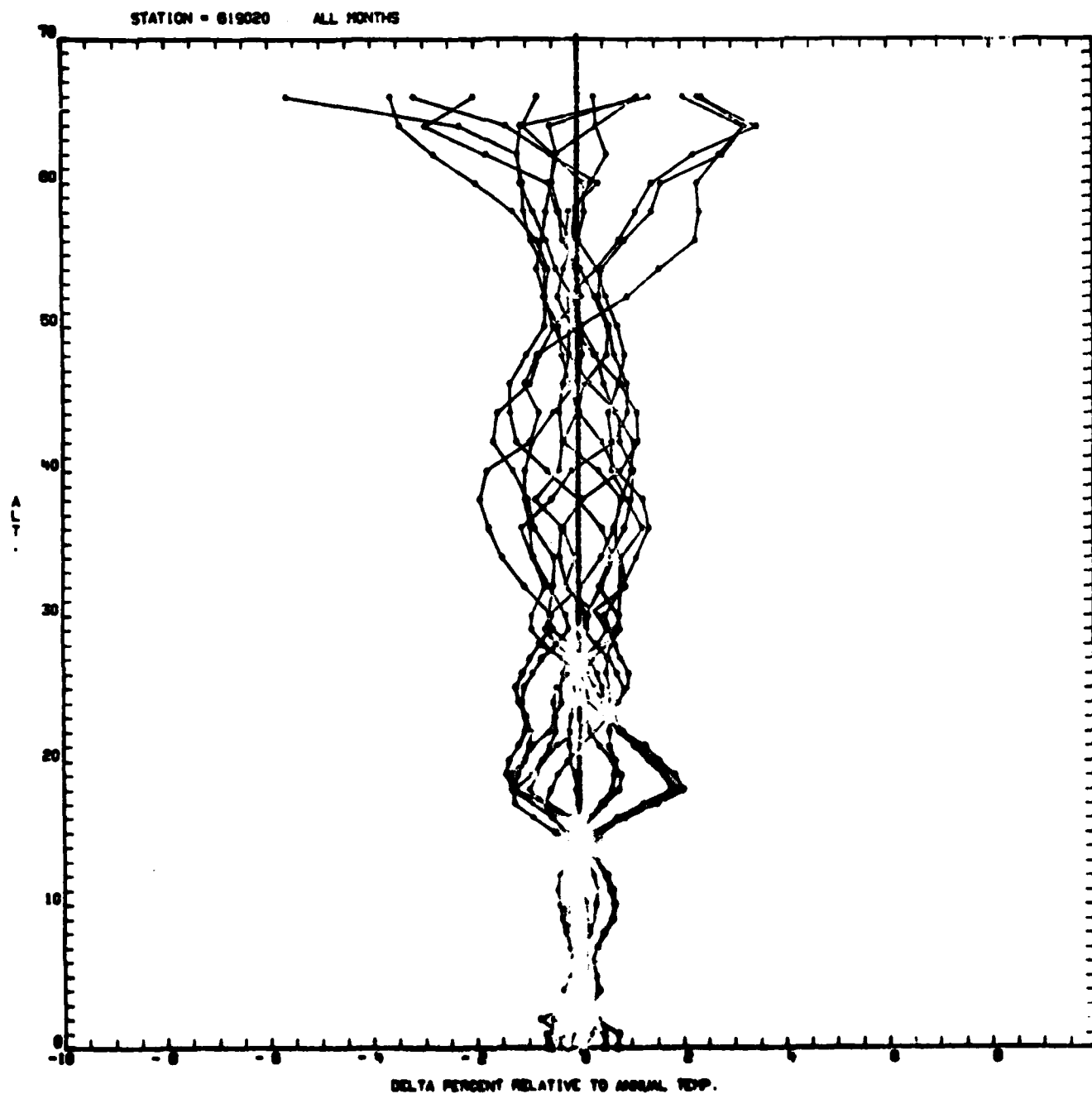


Figure B-11.

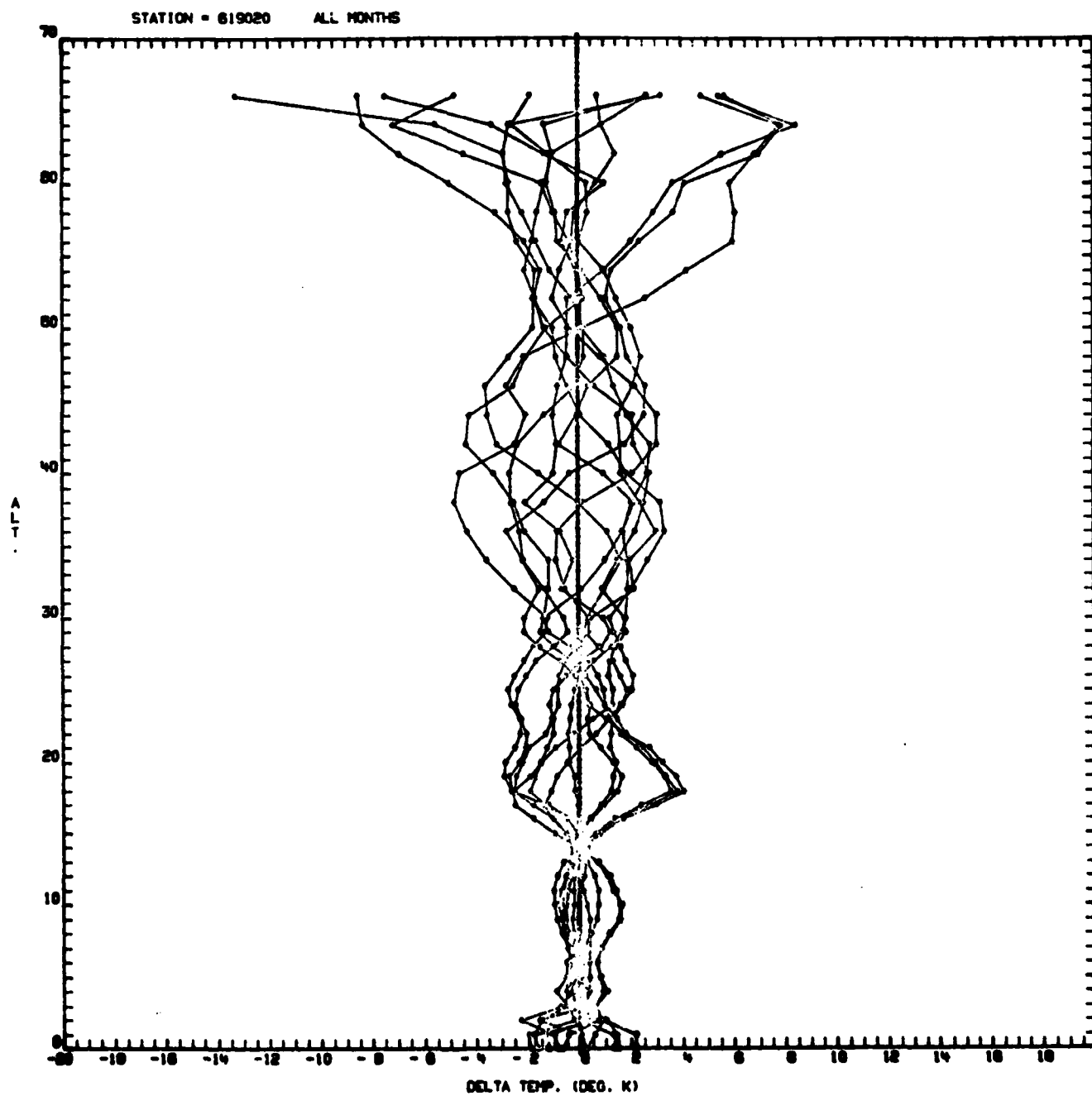


Figure B-12.

Table B-4.

STATION 618020 LEVEL	MONTH CVP	I CVD	CVT	R(P,T)	R(P,D)	R(T,D)	DCVP	DCVD	DCVT
.000	.0015	.0054	.0046	-.3471	.9881	-.9833	-.0085	-.0008	-.0023
.020	.0015	.0052	.0045	-.3374	.9809	-.9623	-.0083	-.0008	-.0022
1.000	.0015	.0047	.0045	.0379	.2848	-.9471	-.0076	-.0013	-.0017
2.000	.0016	.0059	.0059	.1006	.1682	-.9638	-.0102	-.0015	-.0016
3.000	.0018	.0041	.0044	.3343	.0711	-.9163	-.0068	-.0020	-.0015
4.000	.0020	.0045	.0046	.2622	.1735	-.9037	-.0071	-.0021	-.0019
5.000	.0021	.0055	.0053	.1210	.2650	-.9251	-.0087	-.0019	-.0023
6.000	.0023	.0052	.0054	.2848	.1456	-.9059	-.0083	-.0024	-.0021
7.000	.0026	.0051	.0056	.4148	.0475	-.6891	-.0082	-.0031	-.0021
8.000	.0029	.0051	.0058	.4773	.0308	-.8636	-.0080	-.0037	-.0022
9.000	.0034	.0058	.0065	.4716	.0459	-.8592	-.0090	-.0041	-.0026
10.000	.0040	.0062	.0071	.4821	.0902	-.8291	-.0093	-.0048	-.0031
11.000	.0045	.0047	.0063	.6723	.0867	-.6938	-.0064	-.0061	-.0029
12.000	.0050	.0047	.0059	.6400	.2834	-.5535	-.0054	-.0062	-.0039
13.000	.0057	.0060	.0062	.4923	.4384	-.5583	-.0065	-.0059	-.0055
14.000	.0061	.0078	.0076	.3652	.4267	-.6861	-.0093	-.0059	-.0063
15.000	.0065	.0094	.0093	.3402	.3573	-.7567	-.0122	-.0065	-.0068
16.000	.0070	.0105	.0102	.2820	.3038	-.7743	-.0138	-.0066	-.0074
17.000	.0074	.0123	.0105	.0824	.5316	-.8003	-.0154	-.0056	-.0093
18.000	.0077	.0150	.0132	.0419	.4750	-.8593	-.0206	-.0059	-.0095
19.000	.0081	.0142	.0133	.1803	.3978	-.8307	-.0195	-.0071	-.0090
20.000	.0087	.0124	.0125	.3523	.3350	-.7502	-.0162	-.0068	-.0096
21.000	.0094	.0106	.0116	.5083	.3351	-.6411	-.0128	-.0104	-.0085
22.000	.0106	.0104	.0107	.5216	.4756	-.5024	-.0108	-.0109	-.0102
23.000	.0112	.0104	.0097	.5118	.6039	-.3756	-.0089	-.0105	-.0120
24.000	.0120	.0132	.0109	.3356	.6326	-.5172	-.0121	-.0097	-.0143
25.000	.0128	.0148	.0116	.8477	.6948	-.5703	-.0138	-.0093	-.0158
26.000	.0130	.0156	.0118	.2178	.6727	-.5759	-.0143	-.0093	-.0168
27.000	.0134	.0156	.0117	.2288	.6837	-.5542	-.0140	-.0094	-.0173
28.000	.0139	.0162	.0113	.1847	.7292	-.5378	-.0136	-.0090	-.0188
29.000	.0143	.0168	.0115	.1710	.7357	-.5404	-.0140	-.0091	-.0136
30.000	.0148	.0164	.0112	.2261	.7474	-.4782	-.0128	-.0096	-.0200
32.000	.0148	.0157	.0138	.3993	.5912	-.5034	-.0147	-.0129	-.0167
34.000	.0163	.0156	.0154	.5301	.5805	-.4160	-.0143	-.0165	-.0170
36.000	.0182	.0178	.0174	.8420	.5533	-.4002	-.0158	-.0190	-.0193
38.000	.0224	.0185	.0204	.6294	.5179	-.3388	-.0165	-.0243	-.0206
40.000	.0258	.0214	.0224	.8121	.5845	-.3072	-.0180	-.0267	-.0248
42.000	.0291	.0233	.0202	.6083	.7255	-.1049	-.0143	-.0260	-.0322
44.000	.0322	.0254	.0178	.6193	.8381	.0906	-.0108	-.0244	-.0399
46.000	.0351	.0280	.0182	.6094	.8578	.1152	-.0111	-.0252	-.0449
48.000	.0383	.0324	.0187	.5332	.8730	.0528	-.0129	-.0246	-.0520
50.000	.0400	.0349	.0229	.4939	.8218	-.0895	-.0178	-.0279	-.0520
52.000	.0427	.0402	.0228	.3744	.8495	-.1711	-.0203	-.0254	-.0600
54.000	.0449	.0416	.0224	.3901	.8682	-.1183	-.0182	-.0257	-.0641
56.000	.0483	.0434	.0245	.4413	.8618	-.0748	-.0197	-.0294	-.0671
58.000	.0527	.0450	.0271	.5188	.8578	.0084	-.0194	-.0348	-.0708
60.000	.0506	.0427	.0320	.5442	.7773	-.1049	-.0241	-.0399	-.0613
62.000	.0534	.0408	.0315	.6492	.8091	.0783	-.0188	-.0442	-.0627
64.000	.0585	.0443	.0336	.6581	.8203	.1093	-.0195	-.0478	-.0691
66.000	.0548	.0408	.0421	.8779	.8484	-.1228	-.0279	-.0583	-.0533



Table B-5.

STATION 618020 LEVEL	MONTH CVP	7 CVO	CVT	R(P,T)	R(P,D)	R(T,D)	DCVP	DCVO	DCVT
.000	.0014	.0039	.0035	-.1434	.4783	-.9373	-.0050	-.0009	-.0018
.020	.0014	.0038	.0034	-.1495	.4806	-.9350	-.0059	-.0009	-.0018
1.000	.0015	.0039	.0039	.1221	.2611	-.9262	-.0062	-.0014	-.0016
2.000	.0016	.0082	.0082	.1022	.0921	-.9311	-.0148	-.0016	-.0016
3.000	.0018	.0056	.0058	.1505	.1728	-.9478	-.0094	-.0018	-.0018
4.000	.0020	.0056	.0056	.1951	.1611	-.9365	-.0092	-.0020	-.0020
5.000	.0022	.0053	.0054	.2701	.1341	-.9179	-.0085	-.0023	-.0020
6.000	.0025	.0053	.0055	.3088	.1523	-.8930	-.0082	-.0027	-.0023
7.000	.0027	.0057	.0059	.2998	.1661	-.8910	-.0088	-.0029	-.0025
8.000	.0031	.0062	.0056	.3733	.0982	-.8865	-.0097	-.0035	-.0026
9.000	.0035	.0064	.0072	.4521	.0369	-.8747	-.0101	-.0042	-.0027
10.000	.0040	.0063	.0073	.5134	.0437	-.8321	-.0095	-.0051	-.0030
11.000	.0046	.0045	.0062	.6814	.0933	-.6652	-.0061	-.0062	-.0030
12.000	.0052	.0045	.0057	.6703	.3013	-.5056	-.0050	-.0065	-.0039
13.000	.0058	.0053	.0064	.6273	.3358	-.5221	-.0059	-.0070	-.0047
14.000	.0064	.0069	.0068	.4559	.4783	-.5636	-.0073	-.0063	-.0065
15.000	.0069	.0080	.0074	.3751	.6154	-.6010	-.0086	-.0063	-.0075
16.000	.0073	.0091	.0073	.2187	.6207	-.6294	-.0092	-.0095	-.0090
17.000	.0075	.0127	.0094	-.1053	.6733	-.8062	-.0146	-.0043	-.0108
18.000	.0078	.0145	.0117	-.0726	.5950	-.8448	-.0184	-.0050	-.0106
19.000	.0079	.0145	.0115	-.0787	.6077	-.8396	-.0181	-.0050	-.0108
20.000	.0077	.0132	.0106	-.0261	.6022	-.8138	-.0181	-.0050	-.0104
21.000	.0077	.0126	.0102	.0272	.5879	-.7927	-.0152	-.0053	-.0101
22.000	.0081	.0127	.0107	.1071	.5480	-.7723	-.0153	-.0061	-.0101
23.000	.0083	.0114	.0103	.2587	.4824	-.7134	-.0134	-.0071	-.0094
24.000	.0088	.0117	.0109	.3068	.4675	-.6981	-.0138	-.0080	-.0097
25.000	.0087	.0115	.0105	.2911	.4828	-.6991	-.0133	-.0077	-.0098
26.000	.0092	.0115	.0102	.3027	.5314	-.6405	-.0125	-.0079	-.0105
27.000	.0097	.0110	.0101	.3758	.5323	-.5845	-.0115	-.0087	-.0106
28.000	.0101	.0069	.0083	.4702	.5738	-.4442	-.0091	-.0095	-.0108
29.000	.0104	.0110	.0094	.3928	.6101	-.4809	-.0100	-.0089	-.0118
30.000	.0110	.0122	.0102	.3288	.6216	-.5354	-.0115	-.0089	-.0130
32.000	.0150	.0176	.0208	.5568	.1963	-.7094	-.0234	-.0182	-.0118
34.000	.0190	.0169	.0224	.6781	.2262	-.5625	-.0202	-.0245	-.0135
36.000	.0228	.0150	.0174	.7513	.8440	-.0211	-.0097	-.0252	-.0204
38.000	.0261	.0197	.0173	.6581	.7506	-.0021	-.0108	-.0238	-.0285
40.000	.0293	.0219	.0194	.6634	.7489	.0009	-.0120	-.0268	-.0318
42.000	.0325	.0258	.0174	.6084	.8453	.0914	-.0108	-.0240	-.0408
44.000	.0345	.0335	.0183	.3207	.8948	-.2177	-.0173	-.0194	-.0498
46.000	.0358	.0358	.0202	.2853	.8403	-.2800	-.0202	-.0203	-.0514
48.000	.0377	.0363	.0222	.3566	.8214	-.2389	-.0207	-.0238	-.0518
50.000	.0418	.0381	.0208	.4195	.8889	-.0849	-.0170	-.0245	-.0591
52.000	.0437	.0401	.0191	.3989	.8998	-.0411	-.0155	-.0227	-.0648
54.000	.0456	.0432	.0199	.3353	.9016	-.1051	-.0174	-.0223	-.0690
56.000	.0474	.0448	.0204	.3390	.9035	-.0971	-.0178	-.0230	-.0717
58.000	.0514	.0449	.0265	.4695	.8570	-.0288	-.0200	-.0331	-.0698
60.000	.0582	.0525	.0320	.4447	.8377	-.1186	-.0263	-.0377	-.0787
62.000	.0673	.0589	.0320	.4846	.8800	.0110	-.0235	-.0404	-.0942
64.000	.0778	.0687	.0412	.4727	.8480	-.0644	-.0321	-.0503	-.1094
66.000	.1097	.0997	.0640	.4414	.8171	-.1588	-.0540	-.0741	-.1454

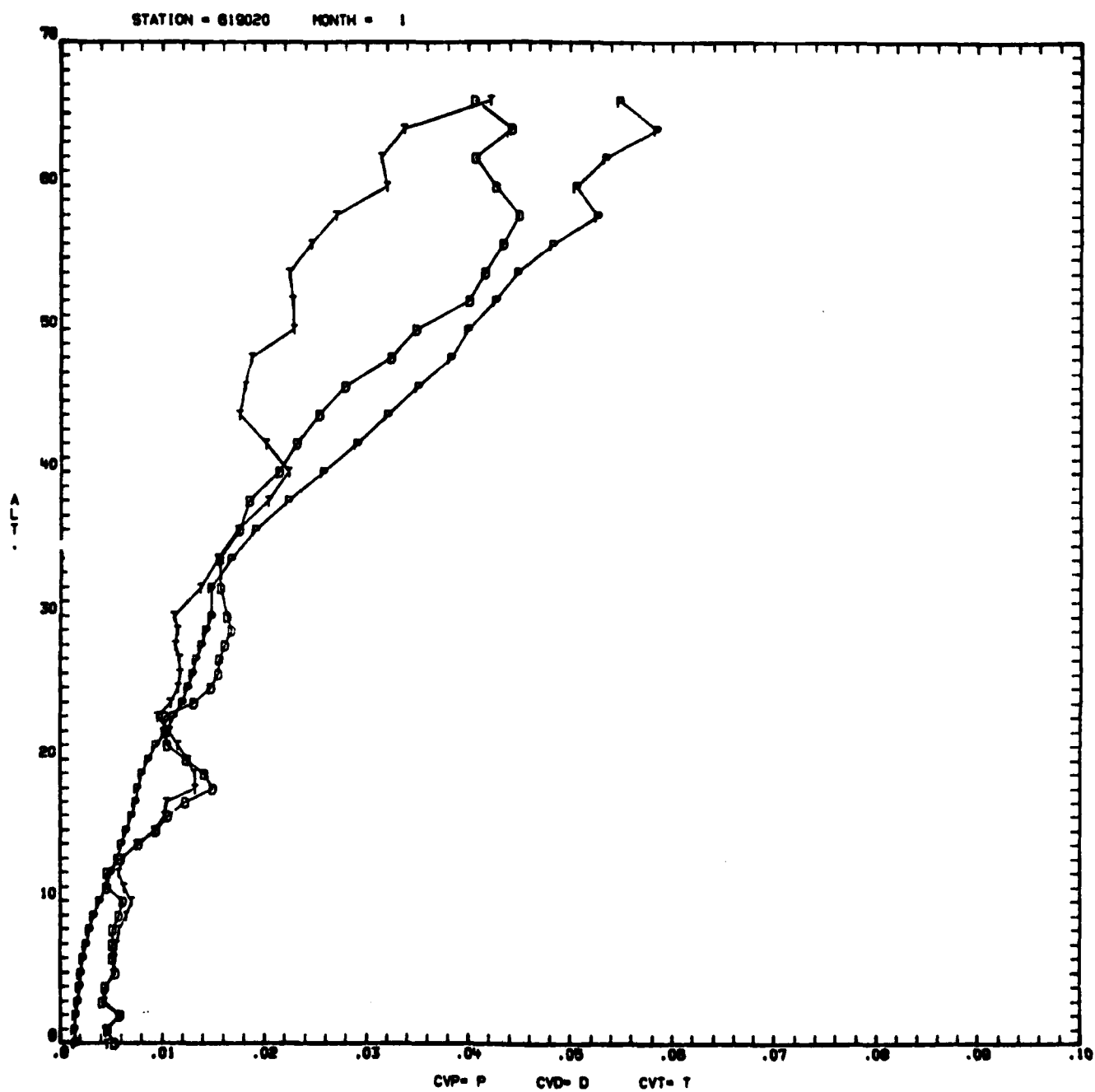


Figure B-13.

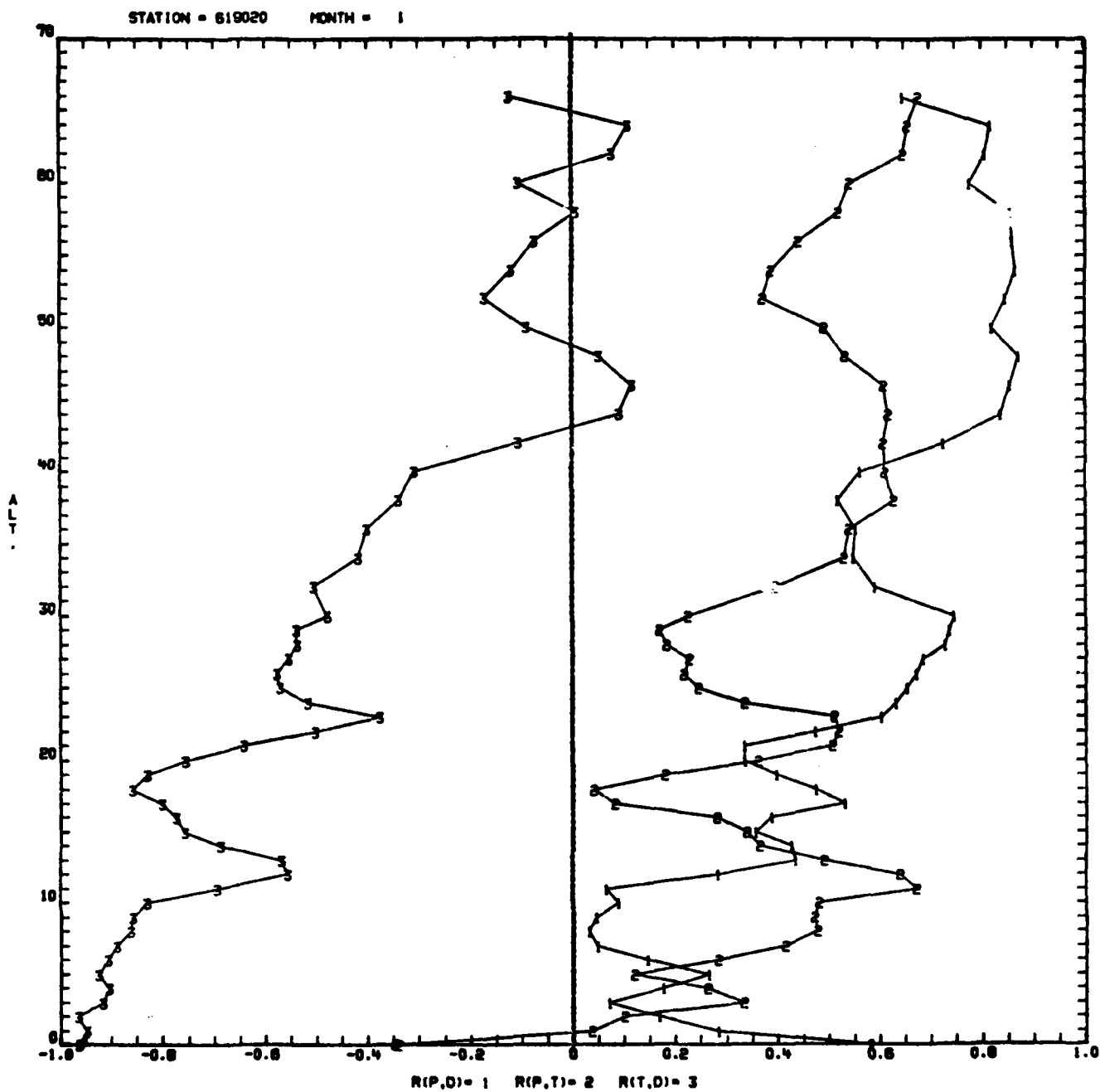


Figure B-14.

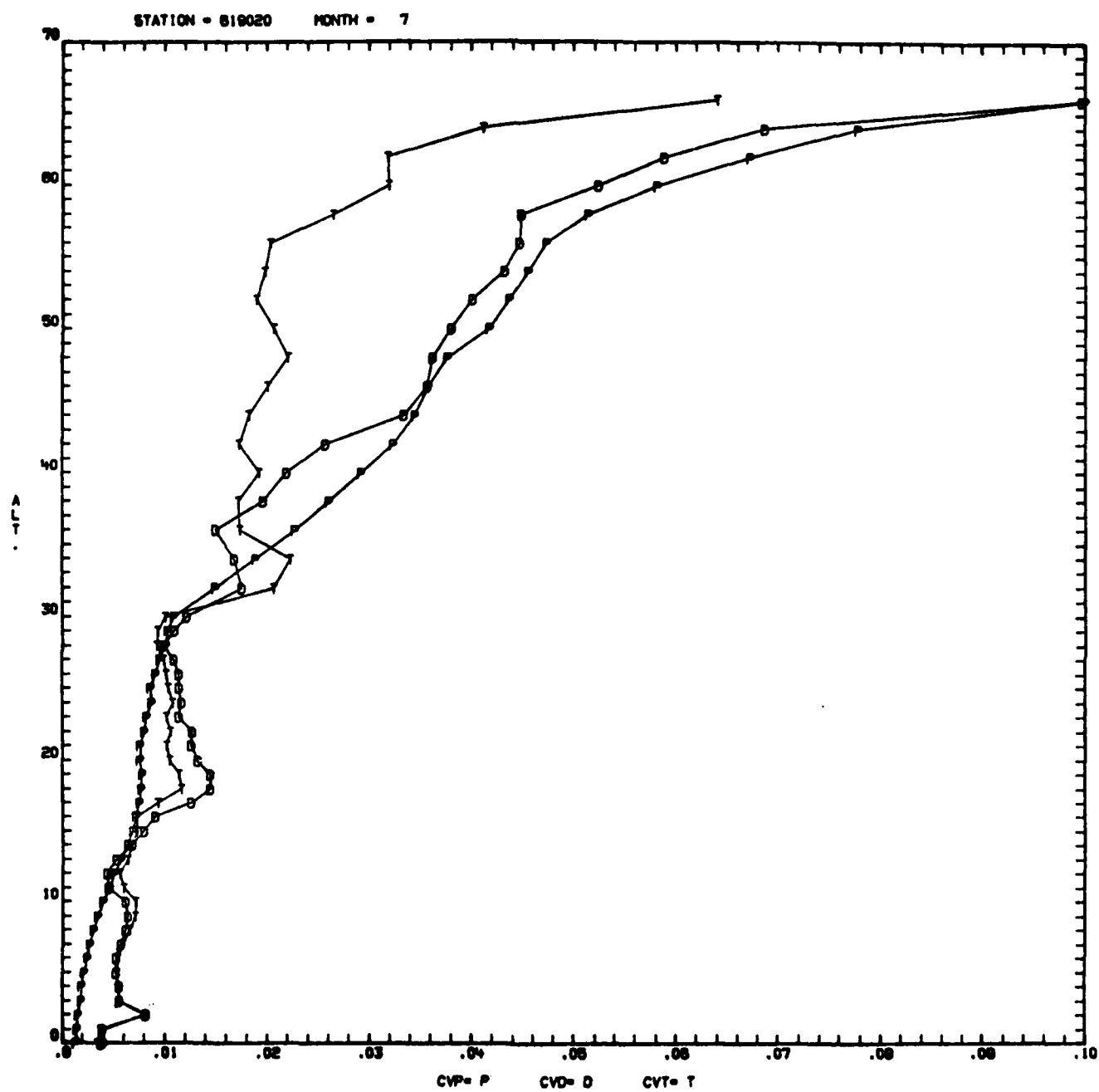


Figure B-15.

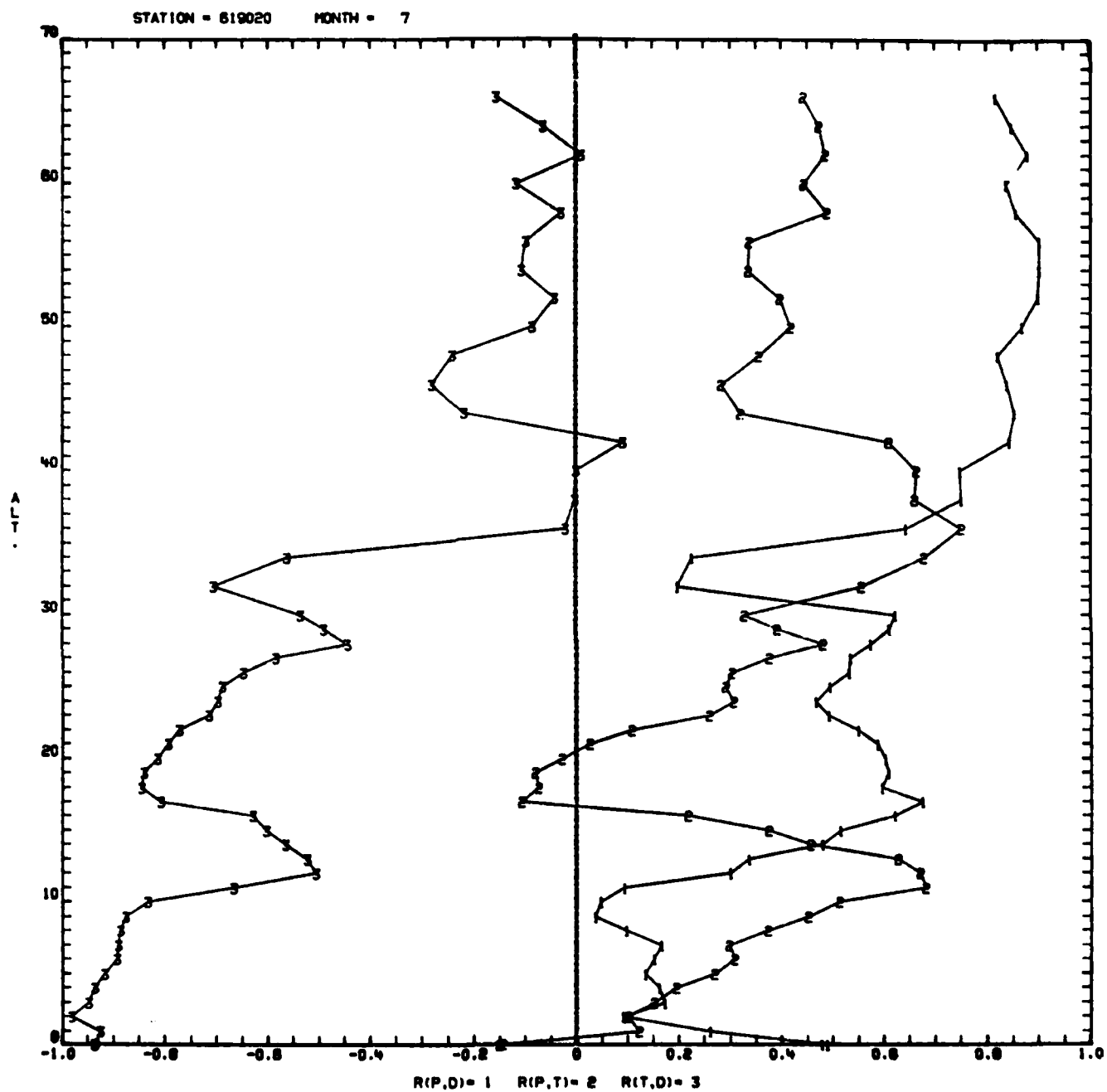


Figure B-16.

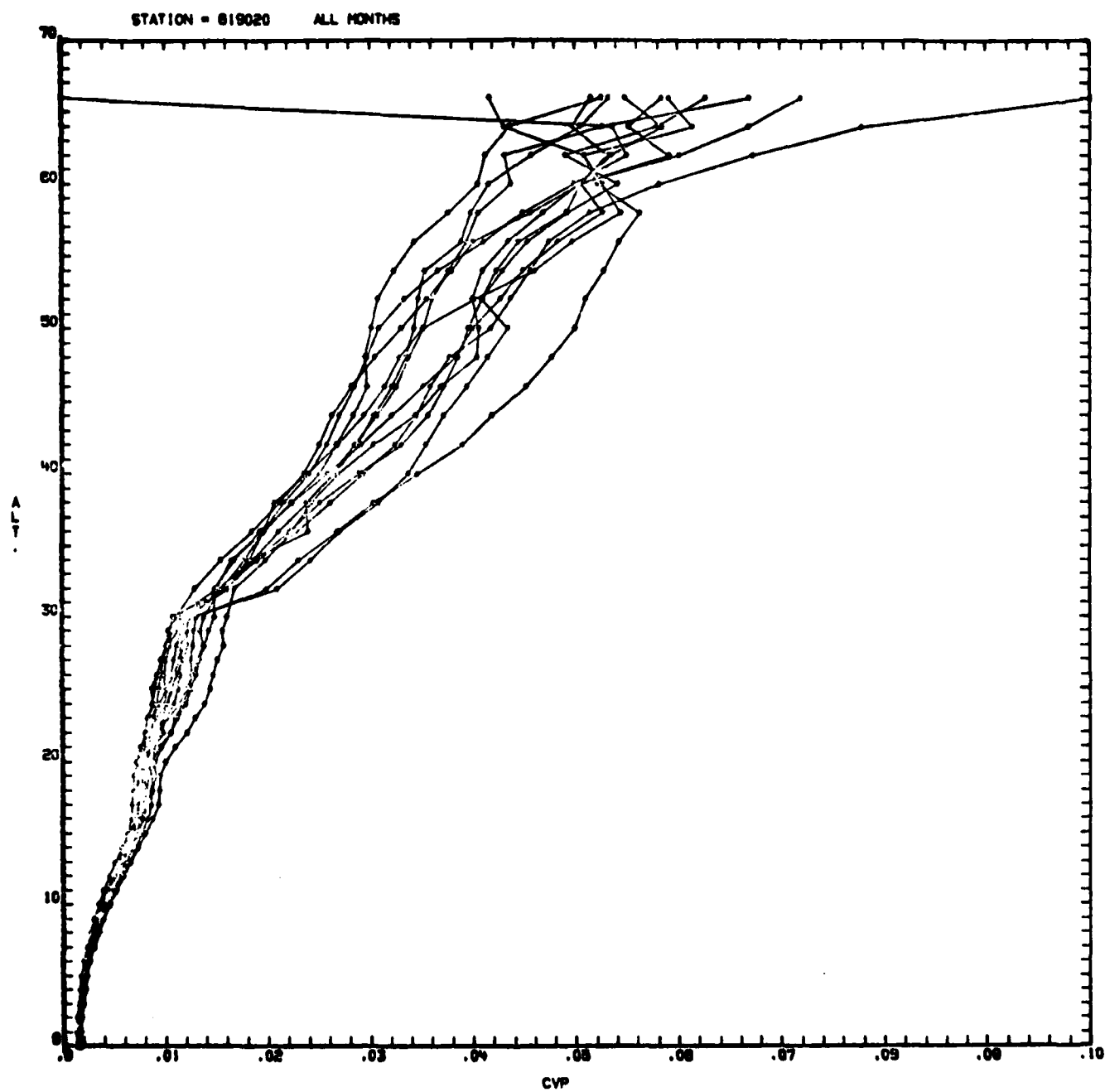


Figure B-17.

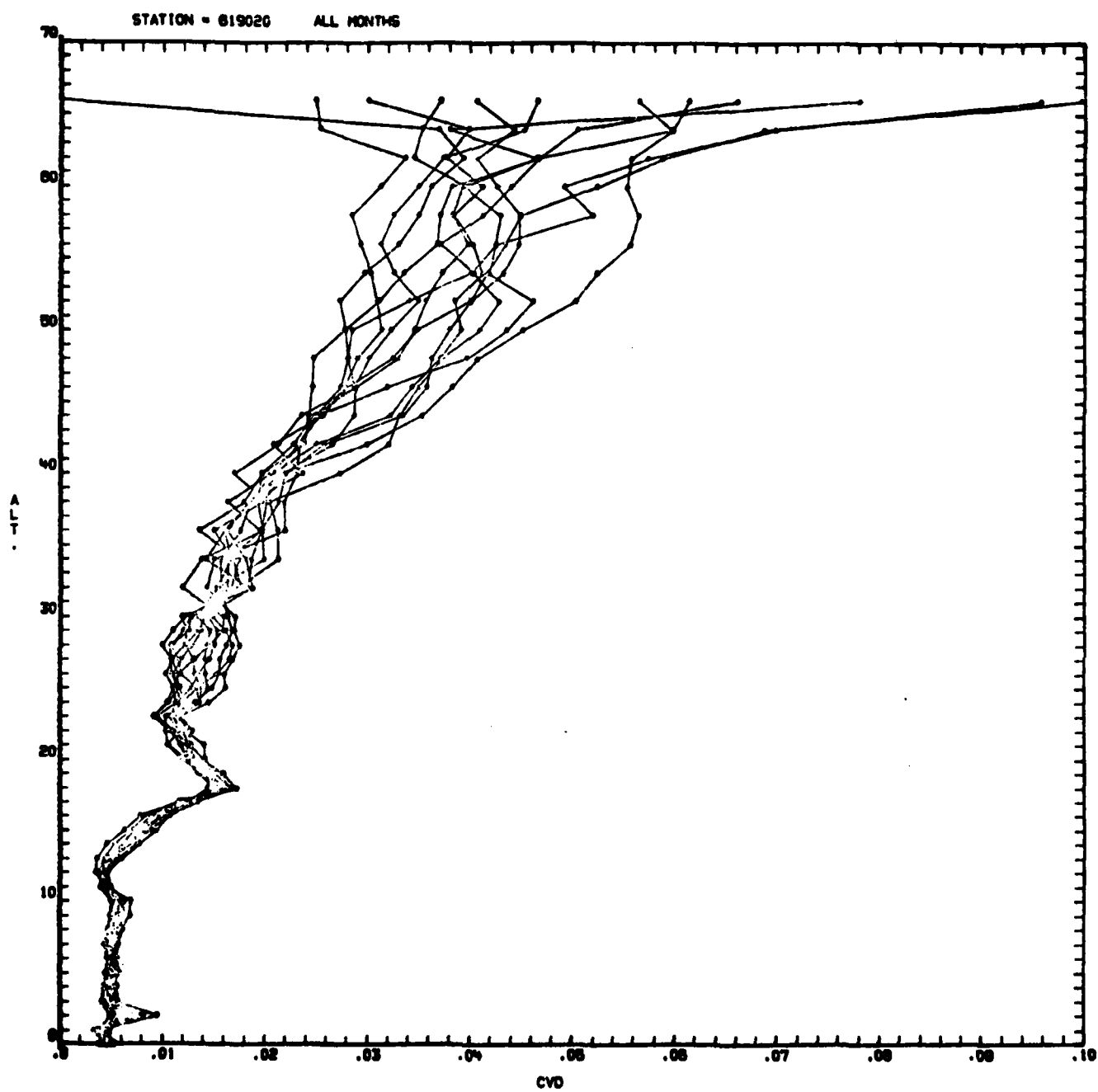


Figure B-18.

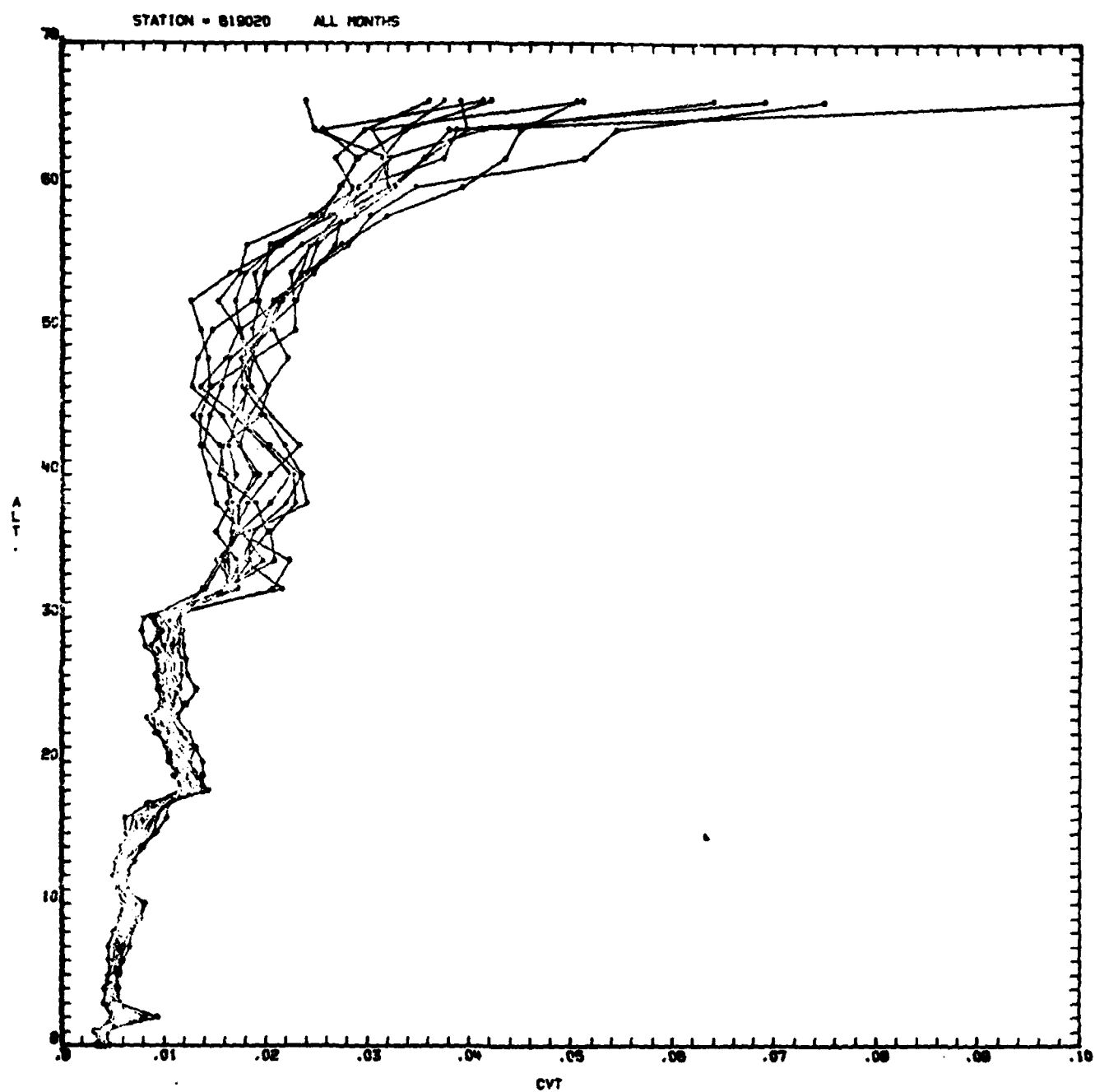


Figure B-19.



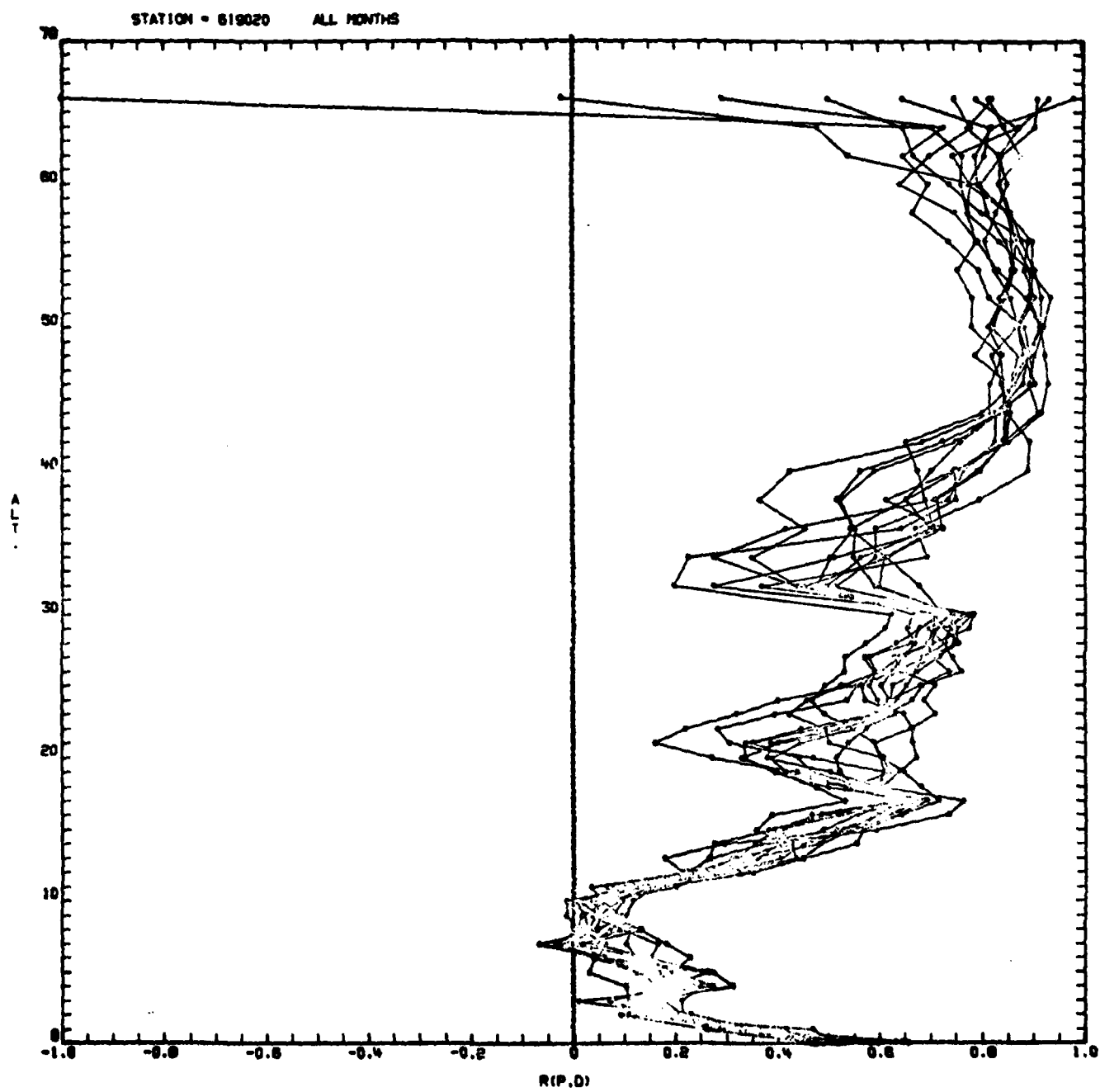


Figure B-20.

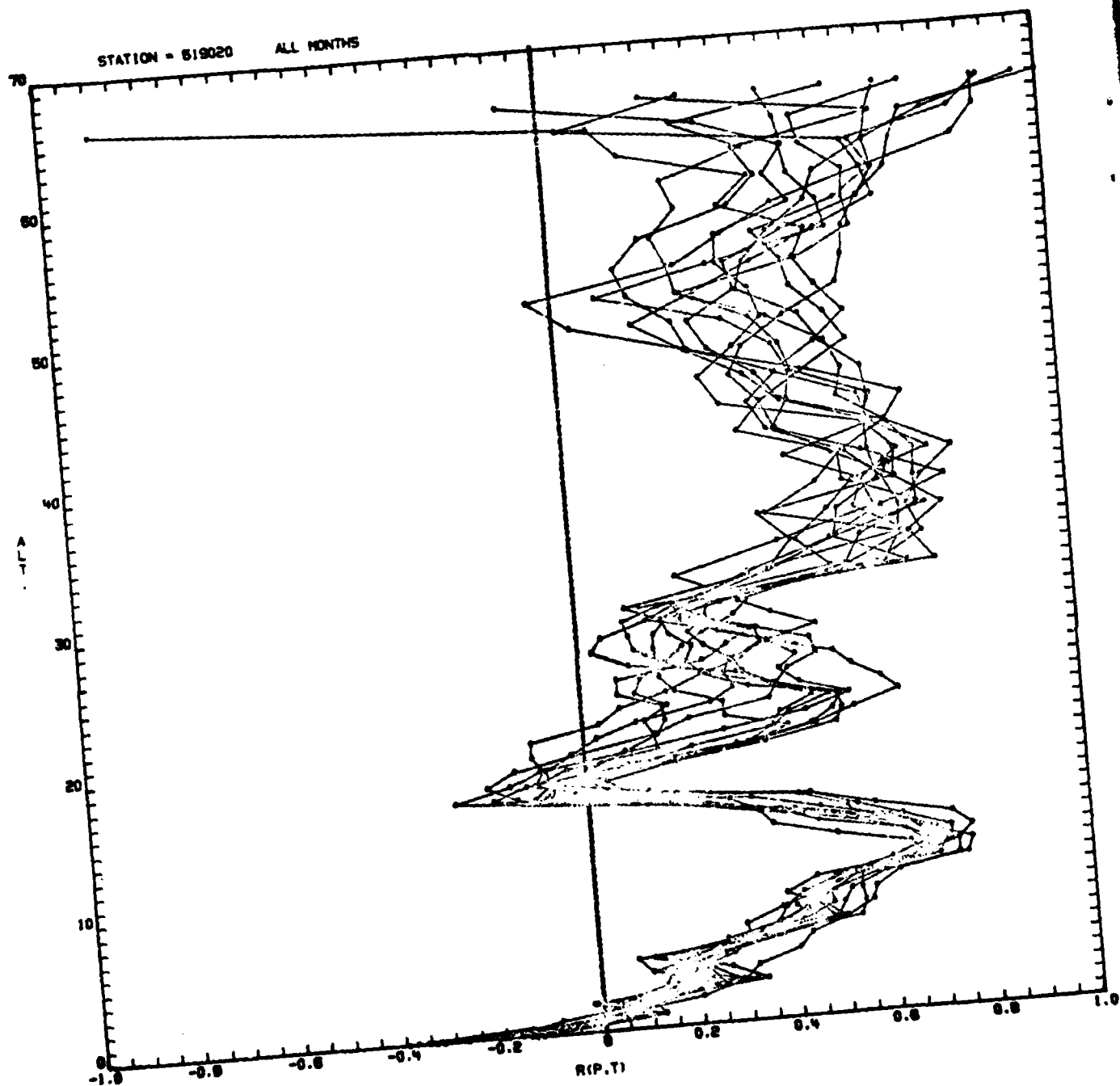


Figure B-21.

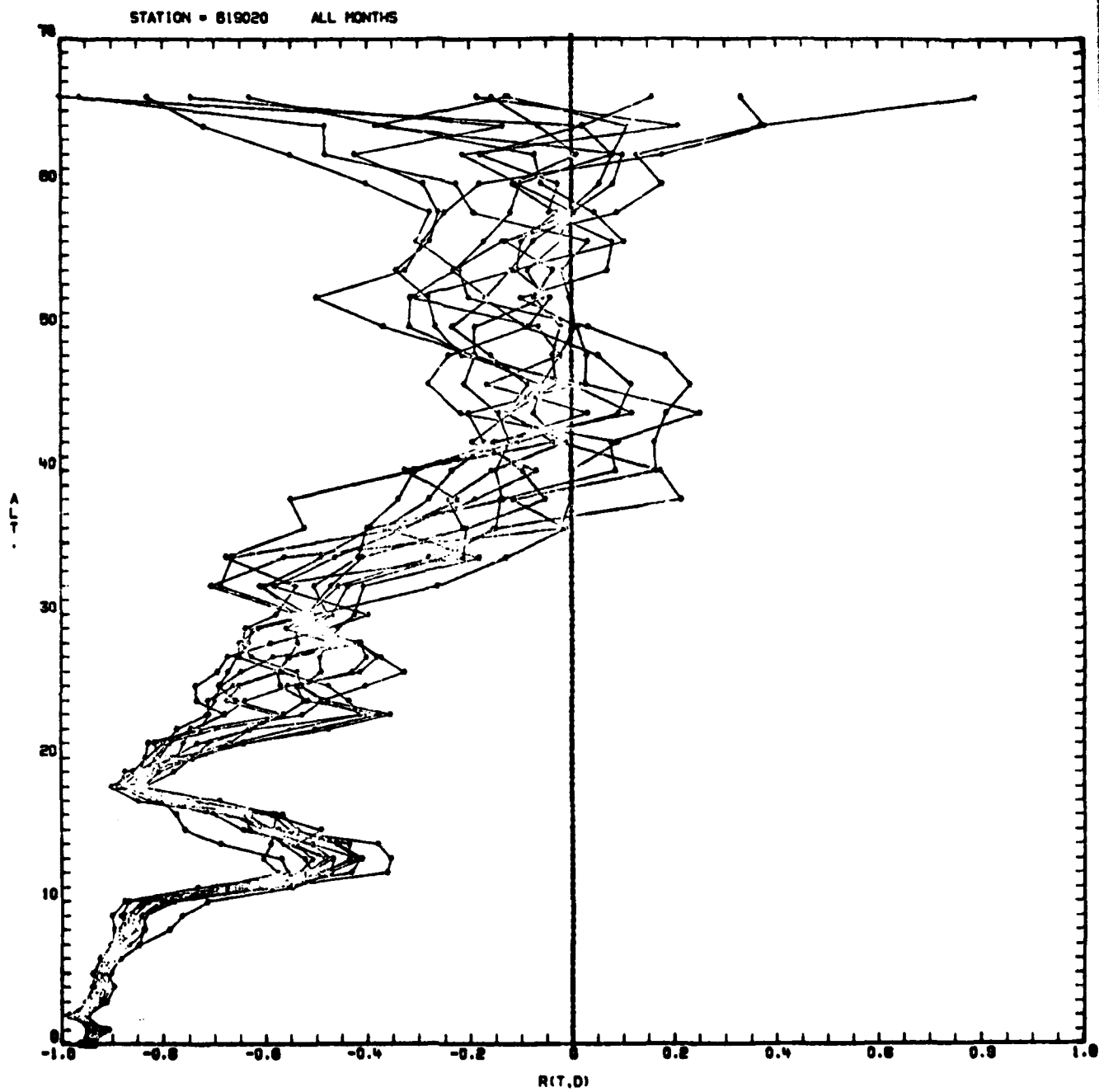


Figure B-22.